## I Selection Guide to NSK Linear Guides

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## Characteristics of NSK Linear Rolling Guides

The following describes comparative characteristics of rolling and slide guide way, which are the most commonly used.

Comparative characteristics of rolling and sliding guide way

| Function | Rolling guide | Sliding guide |
| :---: | :---: | :---: |
| Friction | - Friction coefficient: 0.01 and lower <br> - Difference between static and dynamic friction is small. <br> -Change by speed is slight. | - Friction is great <br> - Static and dynamic friction vary greatly. |
| Positioning accuracy | - Lost motion is slight. <br> - Stick-slip is slight. <br> - Easy to sub-micron positioning | - Lost motion is great. <br> - Stick-slip at low speed is great. <br> - Difficult to achieve sub-micron positioning |
| Life | - Easy to estimate life | - Difficult to estimate life |
| Static rigidity | - Generally high <br> - No play because of preload <br> - Easy-to estimate rigidity | - Rigidity is great against load from a single direction. <br> -There is mechanical play. <br> - Difficult to estimate rigidity |
| Speed | -Wide range of use from low to high speed. | - Unsuitable for extremely low and high speed |
| Maintenance, reliability | - Long life through simple maintenance | - Precision is lost greatly by deteriorated guide surface. |

In response to the demand for guide with highspeed, high-precision, high-quality, as well as to the demand for easy maintenance, rolling guides which have above features are becoming prevalent.
Utilizing the technology we sharpened in anti-friction rotating bearings, NSK makes various types of linear guides which are highly accurate and reliable.

## Characteristics of the NSK linear rolling guides are:

## - Designs are simple and void of waste. This contributes to high precision and low cost.

- Ultra-high purity of materials and superb processing technology assure reliability.
- Prompt delivery thanks to interchangeable components and abundant stock.
-The user can select the most suitable guide from a wide choice.


## Types of NSK Linear Rolling Guides A <br> Rigidity; @ :Superb 〇 :Fare 0 :Low

| Product | Appearance | Rolling element, etc. | Rigidity | Major applications |
| :---: | :---: | :---: | :---: | :---: |
|  | LH Series <br> Page A38 | Balls <br> Infinite stroke <br> Guided by rail | $0$ | - Industrial robots <br> - Materials handling <br> - Electric discharge machines <br> - Woodworking machines <br> - Laser processing machines <br> - Semiconductor manufacturing equipment <br> - Precision measuring equipment <br> - Packaging/packing machines <br> - Food processing machines <br> - Medical equipment <br> - Tool grinders <br> - Flat surface grinders |
|  | LS Series <br> Page A52 |  | $0$ | - Industrial robots <br> - Materials handling <br> - Electric discharge machines <br> -Woodworking machines <br> - Laser processing machines <br> - Semiconductor manufacturing equipment <br> - Precision measuring equipment <br> - Packaging/packing machines <br> - Food processing machines <br> -Medical equipment <br> - Pneumatic components |
|  | LA Series |  |  | - Machining centers <br> - NC lathes <br> - Heavy cutting machine tools <br> - Grinders <br> - Gear cutting machines <br> - Press <br> - Electric discharge machines |
|  | LY Series |  | (0) | - Machining centers <br> - NC lathes <br> - Heavy cutting machine tools <br> - Grinders <br> - Gear cutters |
|  | Page A76 |  |  |  |

Rigidity; @ :Superb 0 :Fare $\mathbf{0}$ :Low

| Product |  | Rolling <br> element, etc. | Rigidity | Major applications |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

$\square$

Rigidity; @ :Superb
0 :Far
Fare 0
:Low

| Product | Appearance | $\begin{gathered} \text { Rolling } \\ \text { element, etc. } \end{gathered}$ | Rigidity | Major applications |
| :---: | :---: | :---: | :---: | :---: |
| Linear rolling bushing | Page A185 | Balls <br> Infinite <br> stroke <br> Round guide shaft | 0 | - Materials handling <br> - Packaging machines <br> - Medical equipment <br> - Pneumatic equipment <br> - Office equipment <br> - Assembling machines |
| Crossed roller guide | Page A196 | Roller <br> Limited <br> stroke <br> Rail guide | $0$ | - Precision stage <br> - Measuring equipment <br> -Test equipment <br> - Printed circuit board assembly |
| Roller pack |  |  | (@) | - Large machine tools <br> - Conveyor system for heavy objects (guide for heavy load ) |
| Linear roller bearing |  | Roller Infinite stroke Flat surface guide | (Q) |  |
| Cam- <br> follower/ <br> roller- <br> follower |  |  | 0 | - Conveyor systems <br> - Packaging machines <br> - Pallet changers <br> - Office equipment |

## A- I Selection Guide to NSK Linear Guides

## A-I -1 Structure of NSK Linear Guides

By avoiding structural complexity, and by reducing the number of components, we not only enhanced the precision of linear guides, but also are able to keep costs low. We have added NSK's patented unique structural feature to the original invention (Fig. I-1-1). This contributes to higher precision and lower prices.
NSK linear guide is comprised of a rail and ball slide (Fig. I-1.2). The balls roll on the grooves on the rail and the ball slide, and scooped up by the end carp attached to the end of the ball slide. Then, the balls go through the opening made in the ball slide, and circulate back to the other end.

## A-I -2 Characteristics of NSK Linear Guides

The use of a unique offset gothic arch groove (Fig. I-1•3) allows the NSK linear guides to satisfy groove designs required for specific purposes.
The precise measurement of the ball groove leads to stable production of highly accurate linear guides and interchangeable linear guides.
(Fig. I-1•4).
Such technologies bestow the NSK linear guide with the characteristics outlined below.

## (1) Abundant in type for any purpose

* Various series are available, and their ball slide models and size categories are standardized to satisfy any requirement. Our technology, polished by abundant experience in the use of special materials and surface treatments, meets the customer's most demanding expectations.


## (2) High precision and quality

* High precision and quality come from our superb production and measuring technologies, strengthened by extensive experience in antifriction rotary bearings and ball screw production. Our quality assurance extends to the smallest components.


## (3) High reliability and durability

* Logical simplicity in shape, along with stable processing, maintain high precision and reliability.
* Super-clean materials and our advanced heat treatment and processing technologies increase product durability.


## (4) Component compatibility shortens delivery time

* The adoption of the gothic arch groove, which makes measuring easy, and a new reliable quality control method have made random-matching of the rails and the ball slides possible. This has led to our interchangeable assemblies. Our interchangeable assemblies are stocked as standard products, thereby reducing delivery time.


## (5) Patented static load carrying capacity (shock-resistance)

* When a super-high load (shock-load) is imposed, our gothic-arch groove spreads the load to surfaces which usually do not come into contact. This increases shock resistance (Fig. I-1-5).


Fig. I-1•1• French Patent in 1932.

- Inventor : Gretsh (German)

NSK added its patented technology to the invention in Fig. 1, and improved the linear guide structure and realized low cost design.


Fig. I-1e3 Offset gothic-arch groove


Fig. I-15 Shock-resistance


LH•LS Series


Fig. I-102 Structure of NSK linear guides


Fig. I-14 Processing and measuring a groove Measuring grooves is easy, and you can obtain highly accurate results for all types of NSK series. This is why you can purchase rail and ball slide separately (interchangeability ).

## A-I-2.1 Types and Characteristics of NSK

 Linear GuidesWe have abundant types of linear guide for any purpose to accommodate the most special needs of the users.

## (1) Types of series and classification by

 feature- There are two types of NSK linear guide:

1. Rigidity and load carrying capacity against the vertical direction are greater than the rigidity and load carrying capacity against the load from the lateral direction (high vertical load carrying capacity type);
2. Load is equally distributed to four directions four-directional iso-load carrying capacity type)

- There are three types of NSK linear guide by the length of the ball slide

1. Standard length ball slide with high-load
carrying capacity;
2. Long ball slide with super-high load carrying capacity;
3. Short ball slide for mid-level load carrying capacity.

- Four-row ball grooves linear guide has two types:

1. Self-aligning capability- which absorbs certain amount of installation error
2. High moment carrying type with great moment rigidity.

- Two-row ball grooves linear guide has mid-level moment rigidity
- Interchangeable assemblies: Thanks to the ease in measuring gothic-arch groove, you can separately purchase rail and ball slide in some series.
- Stainless steel is also available as standard material for some series.

Table I-2.1 Classification of NSK linear guides


| Characteristics | Applications | Page |
| :---: | :---: | :---: |
| - High load capacity type. <br> - The contact angle between the ball and ball raceway is set at 50 degrees. The load carrying capacity against the vertical directions, which is prevalent in most operations, increases by this design. <br> - The DF contact structure greatly absorbs the error in the perpendicular direction to rail at the time of installation. <br> - Balls make contacts at two points thanks to the offset gothic-arch groove. This keeps friction to a minimum. <br> - Structural resistance against shock load. <br> - Gothic-arch groove renders measuring of ball grooves accurate and easy. <br> - Standardized interchangeable assemblies allows separate purchase of rails and ball slides. <br> - Stainless steel type is also available for small sizes ( - \#30). | - Cartesian type robots <br> - Robots that remove plastic molds from injection machine <br> - Material hardling <br> - Food processing machines <br> - Packaging/packing machines <br> - Printing machines <br> - Woodworking machines <br> - Paper machines <br> - Measuring equipment <br> - Inspecting equipment <br> - Semiconductor manufacturing equipment <br> - Liquid crystal display manufacturing equipment <br> - Medical equipment <br> - Electric discharge machines <br> - Laser processing machines <br> - Press <br> - Tool grinders <br> - Flat surface grinders <br> - NC lathes <br> - Machining centers <br> - ATC | A38 |



| Characteristics | Applications | Page |
| :---: | :---: | :---: |
| - Compact, low in height <br> - The contact angle between the ball and the raceway is set at 50 degrees. The load carrying capacity against vertical directions, which is prevalent in most operations, increases by this design. <br> - The DF contact structure greatly absorbs the error in the perpendicular direction of rail at time of installation. <br> - Thanks to the offset gothic arch groove, balls make contacts at two points. This keeps friction small. <br> - Great resistance against shock load. <br> - Gothic arch groove renders measuring groove accurate and easy. <br> - Standardized interchangeablility allows separate purchase of rails and ball slide. <br> - Some are standardized stainless steel type. <br> - Low-noise type | - Cartesian type robots <br> - Robots that remove plastic molds from injection machine <br> - Material handling <br> - Food processing machines <br> - Packaging/packing machines <br> - Printing machines <br> - Woodworking machines <br> - Paper machines <br> - Measuring equipment <br> - Inspection equipment <br> - Semiconductor manufacturing equipment <br> - Liquid crystal display manufacturing equipment <br> - Medical equipment <br> - Electric discharge machines <br> - Laser processing machines <br> - Press | A52 |
| - The contact angle between the ball and the raceway is set at 45 degrees. This makes load carrying capacity and rigidity equal in vertical and lateral directions. <br> - Six-row ball grooves support load from vertical and lateral directions, enhancing rigidity and increasing load carrying capacity. <br> - Appropriate friction <br> - Best for machine tools. | - Machining centers <br> - NC lathes <br> - Heavy cutting machine tools <br> - Gear cutters <br> - Electric discharge machines <br> - Press <br> - Grinders | A66 |



| Characteristics |
| :--- |
| - The contact angle between the ball and the raceway is |

- 45 de between the ball and the raceway is se are equal in vertical and lateral directions
- Balls contact at four points during high preload. The fourrow ball groove supports the load from vertical and lateral directions. This makes the linear guide highly rigid.
- Rigidity against moment load is great due to the DB contact (at time of light preload) or the four-point contact (at time of high preload)
- Sliding resistance slightly increases, absorbing vibration to the rail longitudinal direction due to the four-point contact at time of high preload.
- Ideal for heavy cutting machine tools.
- Strong against shock load
- Low-noise type
- The contact angle between the ball and the raceway is set at 50 degrees. The load carrying capacity against vertical
 with this design
- The rail is wide. This contributes to a high rolling moment carrying capacity and to great moment rigidity when only single linear guide is in use
- Balls contact at two points in the offset gothic arch groove, keeping friction small.
- High resistance against shock load
- Standardized interchangeable assemblies allows separate purchase of rails and ball slides.
- Extremely thin, and wide in shape. This is ideal in use of only single linear guide.
- Available in standardized stainless stee
- Standardized series with ball retainer
- Standardizedinterchangeablity allows separate purchase of rails and ball slide.
- Super-small size
- Stainless steel is standard as the material.
- Series with a ball retainer is standardized.
- Interchangeability is standardized, allowing separate purchase of rails and ball slide.


## - Light-weight and compact

- Stainless steel as standard material is available.

| Applications | Page |
| :---: | :---: |

- Machining centers
- NC lathes
- Heavy cutting machine tools
- Gear cutters
- Semiconductor manufacturing
equipment
- Liquid crystal display
manufacturing equipment
- Conveyor systems
- Inspection equipment
- Punch press
- Semiconductor manufacturing
equipment
- Liquid crystal display
manufacturing equipment
- Medical equipment
- Optical stage
- Microscope XY stage
- Conveying optical fiber
- Small robots
- Computer peripheral equipment
- Pneumatic equipment
- Knitting machines
- Hard disk carriage damper
$\qquad$


## A-I-2.2 Model Number and Shape Code of Ball Slide

- "Model number" refers to a combination of the series name, size number, and code of shape and height of ball slide.


## Example of a model number:



Note: Height code R of LE and LU series refers to low type eith ball retainer.
-The combination of ball shape shape and height are shown in table I- $2 \cdot 2$
Table I-2.2 Shape and height of Ball slide

| Series | Height | Ball slide length | Square type | Flanged type |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Mounting tap | Mounting tap | Mounting bolt hole |
| LH | High | Standard | LH-AN |  |  |
|  |  | Long | LH-BN |  |  |
|  | Low | Standard |  | LH-EL | LH-FL |
|  |  | Long |  | LH-GL | LH-HL |
| LS | Low | Standard | LS-AL | LS-EL | LS-FL |
|  |  | Short | LS-CL | LS-J L | LS-KL |
| LA | High | Standard | LA-AN |  |  |
|  |  | Long | LA-BN |  |  |
|  | Low | Standard | LA-AL | LA-EL | LA-FL |
|  |  | Long | LA-BL | LA-GL | LA-HL |
| LY | High | Standard | LY-AN |  |  |
|  |  | Long | LY-BN |  |  |
|  | Low | Standard | LY-AL | LY-EL | LY-FL |
|  |  | Long | LY-BL | LY-GL | LY-HL |
| LW | Low | Standard |  | LW-EL |  |
| LE | Low | Standard | LE-AL, TL, AR, TR |  |  |
|  |  | Long | LE-BL, UL |  |  |
|  |  | Short | LE-CL, SL |  |  |
| LU | Low | Standard | LU-AL, TL, AR, TR |  |  |
|  |  | Long | LU-BL, UL |  |  |
| LL | Low | Standard | LL-PL |  |  |

## A-I-3 Procedures for Selecting Linear Guide

## A-I-3.1 Flow Chart for Selection

The flow chart below indicates general steps for selection.


## A-I-3.2 Selection of Linear Guide Size

To select a linear guide of satisfactory durability; it is a standard practice to calculate its expected life. Prior to calculating the linear guide's life expectancy, select an appropriate size of the linear guide.
Below is an easy selection method. After selecting the size by this method, check the life by using the

## "A-II-3.2: Calculation of Life Expectancy."

## (1) Select the size based on the space to be used

Select a linear guide which matches the space in which it is used. Select directly from the "A-I-5:

## Model Number and Dimension Table."

## (2) Select the size based on the ball screw size

Always select a linear guide which matches the size of the screw shaft diameter, or the size closest to it, e.g., when the ball screw shaft diameter is 32 the select linear guide type should be LH30, or LH35.

## (3) Select the size based on the estimated load on one ball slider

Most linear guides are table-shaped and have two rails and four ball slides for an axis.
Assuming the linear guide is this type, calculate a rough load per ball slide using the formula below:

$$
\begin{equation*}
P=\sum \frac{F}{4}+\sum \frac{K_{\mathrm{p}} \cdot F}{2} \tag{3.1}
\end{equation*}
$$

$P$ : Load per ball slide
$K_{\mathrm{p}}$ : Load position coefficient
$F$ :Load
Load position coefficient $K_{\mathrm{p}}$ should be found for each load by the proportion of the distance between ball slide span and load point, and the distance between rail span and load point.
(A) When load is vertical
(Fig. I-31)

$$
K_{\mathrm{p}}=\left|\frac{X_{0}}{L_{\mathrm{b}}}\right|+\left|\frac{Y_{0}}{L_{\mathrm{r}}}\right|
$$

(B) When the load is in the axial direction
(Fig. I-302)

$$
K_{\mathrm{p}}=\left|\frac{Z_{1}}{L_{\mathrm{b}}}\right|+\left|\frac{Y_{1}}{L_{\mathrm{b}}}\right|
$$

## (C) When the load is lateral to the rail

(Fig. I-3•3)

$$
K_{\mathrm{p}}=\left|\frac{X_{0}}{L_{\mathrm{b}}}\right|+\left|\frac{Z_{0}}{L_{\mathrm{r}}}\right|
$$

The load position is normally the coordinate position. Disregard +or - symbols, and use absolute values.

Upon obtaining the load value $P$ per ball slide by using the above position coefficient $K_{\mathrm{p}}$ in (3.1), select the matching size (model number) from Fig. I-3•4. Because the above calculation formula is a simple one, the load obtained by the above formula may be larger than the actual case if the value of $K_{\mathrm{p}}$ is over 1, or in the case three patterns (A), (B), and (C) are combined. In such case, the size to be selected ( model number) should be larger; however, the life will be longer.


Fig. I-31 Load from vertical direction


Fig. I-302 Load to the axis direction


Fig. I-33 Load from the lateral direction of rail


Fig.I-34 Selection based on the load
(4) Selection based on the moment load per ball slide

- In cases shown in Fig.I-3•5 to $\bullet 6, \bullet 7$, it is necessary to consider the moment load applied to the ball slide.
- Moment directions that have to be taken into account are only those shown by the arrow in the Figures.
- When the load is applied from more than one
direction, select the value of the direction which applies to the largest moment load.
- Select the size (model number) based on the moment load per ball slide referring to either Fig.I$3 \cdot 8$ or Fig.I-309.
- Consult NSK when: moment load and vertical load are applied at the same time; or moment load and horizontal load are applied at the same time.


Fig.I-35 Pitching direction


Fig.I-36 Rolling direction


Fig.I-307 Pitching, rolling and yawing directions


Fig.I-38 Selection based on the moment load, rolling direction


Fig.I-3-9 Selection based on the moment load, pitching or yawing direction

- Loads applied to the types recommended in Fig.I-3•4, I-3•8, and I-3•9 are equivalent to $10 \%$ of the basic dynamic load rating of the linear guide. This contributes to select a size numfer with a longer life.


## A-I-3.3 Example of Linear Guide Selection (Model number)

The selection below used "A-I-3.2 (3) Selection based on load per ball slide."
In this example, let us select a linear guide for a single axis table as illustrated below.
Use LH-AN type in LH Series which is selected based on "A-I-2.1 Types and Characteristics of NSK Linear Guides"


## Weight and coordinates of Table W :

$$
\text { 500N, }(0,0,-)
$$

Weight and coordinates of Weight $F_{1}$ :
2500N, ( 100,120, - )

Weight and coordinates of Weight $F_{2}$ :
1000N, ( 0,180, - )
Since the above is all vertical load, we do not consider $Z$ axis coordinates.
Therefore, the formula "(A) When vertical load is applied" is.:

$$
K_{\mathrm{p} 0}=\left|\frac{X_{0}}{L_{\mathrm{b}}}\right|+\left|\frac{Y_{0}}{L_{\mathrm{r}}}\right|=\frac{0}{300}+\frac{0}{300}=0
$$

(1) Also

$$
\begin{aligned}
& K_{\mathrm{p} 1}=\frac{100}{300}+\frac{120}{300}=0.73 \\
& K_{\mathrm{p} 2}=\frac{0}{300}+\frac{180}{300}=0.6
\end{aligned}
$$

obtain the load per ball slide $P$ using formula (5.1.) as follows.

$$
\begin{aligned}
P & =\sum \frac{F}{4}+\sum \frac{K_{\mathrm{p}} \cdot F}{2} \\
& =\frac{W+F_{1}+F_{2}}{4}+\frac{K_{\mathrm{p} 0} \cdot W+K_{\mathrm{p} 1} \cdot F_{1}+K_{\mathrm{p} 2} \cdot F_{2}}{2} \\
& =\frac{500+2500+1000}{4} \\
& +\frac{0 \times 500+0.73 \times 2500+0.6 \times 1000}{2} \\
& =2212.5(\mathrm{~N})
\end{aligned}
$$

The appropriate size is around 30 for $\mathrm{LH}, \mathrm{LS}$, and LY types according to Fig. I-3.4. Confirm the size (Model number) in " A-I -5 Model Number and Dimension Table." The correct linear guide size is LH30AN. Calculate the life expectancy using "A-II-3.2 Calculation of Life Expectancy." In this case, the expected life is 47560 km .

## A-I-3.4 Accuracy and Preload

## (1) Accuracy grades and types of preload

## (1) Accuracy grades

- The accuracy grade which matches the characteristic of each series is set for NSK linear guides.
- Table I-3•1 shows accuracy grade set for each series.
- See Page A115 for accuracy specifications of each
series.
- Refer to "(2) Application examples of accuracy grades and preload" which shows cases of appropriate accuracy grade and preload type for specific purpose.

Table I-31 Accuracy grades and applicable series

|  | Preloaded assembly (non-interchangeable) |  |  |  |  | Interchangeable assembly |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ultra precision | Super precision | High precision | Precision | Normal grade | Normal grade |
| Series | P3 | P4 | P5 | P6 | PN | PC |
| LH | 0 | 0 | 0 | 0 | 0 | 0 |
| LS | 0 | 0 | 0 | 0 | 0 | 0 |
| LA | 0 | 0 | 0 | 0 |  |  |
| LY | 0 | 0 | 0 | 0 |  |  |
| LW |  |  | 0 | 0 | 0 | 0 |
| LE |  |  | 0 | 0 | 0 | 0 |
| LU |  | 0 | 0 | 0 | 0 | 0 |
| LL |  |  |  |  | 0 |  |

Preload

- Several types of preload that match the characteristic of each series are set for NSK linear guides.
- Types of preload for each series are shown in Table I-3•2.
- Radial clearance, preload, and rigidity of each series are shown in Page A119
- "(2) Application examples of accuracy grade and preload" show cases of appropriate preload and accuracy grades for specific purposes.

Table I-3.2 Classification of preload

|  | Preloaded assembly (non-interchangeable) |  |  |  |  | Interchangeable assembly |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Heavy preload | Medium preload | Light preload | Slight preload | Fine clearance | Slight preload | Fine clearance |
| Series | Z4 | Z3 | Z2 | Z1 | Z0 | ZZ | ZT(Z0) |
| LH |  | 0 |  | 0 | 0 | 0 | 0 |
| LS |  | 0 |  | 0 | 0 | 0 | 0 |
| LA | 0 | 0 |  |  |  |  |  |
| LY | 0 | 0 | 0 | 0 | 0 |  |  |
| LW |  | $(0)$ |  | 0 | 0 |  | 0 |
| LE |  |  |  | 0 | 0 |  | 0 |
| LU |  |  |  | 0 | 0 |  | 0 |
| LL |  |  |  |  | 0 |  |  |

Note: •Z3 preload types for LW Series are LW35, 50 only.

- "Z" is omitted from the specification number (See A-I-4.1).
(3) Combinations of accuracy grade and preload
- Combinations of accuracy grade and preload are shown in Table I-3•3.

Table I-3॰3 Combinations of accuracy grade and preload type

| Preloaded assembly | Accuracy grade | Preload |
| :---: | :---: | :---: |
|  | P3~P6 | Z4~Z0 |
| Interchangeable assembly | PN | Z1, Z0 |

## （2）Application examples of accuracy grade and preload

Table I－3．4 shows examples of accuracy grade and preload＂of NSK linear guides for specific purposes．

Refer to this table when selecting accuracy grade and preload type for your application．

Tabl I－3e4 Examples of accuracy grade and preload for specific purpose

|  | Application | Accuracy grade |  |  |  |  | Preload |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{array}{\|c\|} \hline \text { Ultra } \\ \text { precision } \end{array}$ P3 | $\begin{gathered} \text { Super } \\ \text { n precision } \end{gathered}$ P4 | High <br> precision <br> P5 | Precision P6 | Normal grade PN，PC | Heavy preload Z4 | Medium preload Z3 | Light 72 | Slight preload Z1，ZZ | Fine clearance Z0 |
|  | －Machining centers |  | 0 | 0 | 0 |  | 0 | 0 |  |  |  |
|  | －Grinders | 0 | 0 | 0 |  |  | 0 | 0 | 0 |  |  |
| $\stackrel{\sim}{0}$ | －Lathes |  | 0 | 0 | 0 |  | 0 | 0 |  |  |  |
| O | －Milling machines |  | 0 | 0 | 0 |  | 0 | 0 |  |  |  |
| $\stackrel{\square}{0}$ | －Drilling machines |  |  | 0 | 0 |  | 0 | 0 |  |  |  |
| ． | －Boring machines |  | 0 | 0 | 0 |  | 0 | 0 |  |  |  |
| Ч | －Gear cutters |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |
| $\sum^{0}$ | －Diesinking machine |  | 0 | 0 | 0 |  |  | 0 | 0 | 0 |  |
|  | －Laser processing machine |  | 0 | 0 | 0 |  |  | 0 | 0 | 0 |  |
|  | －Electric discharge machine | 0 | 0 | 0 |  |  | 0 | 0 |  |  |  |
|  | －Punch press |  |  | 0 | 0 |  |  | 0 | 0 | 0 |  |
| ¢ | －Press machine |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| 등 | －Welding machine |  |  |  | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 言 | －Painting machine |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| 힝 | －Textile machine |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| $\bigcirc$ | －Coil winder |  |  |  | 0 | 0 |  | 0 | 0 | 0 |  |
| 0 | －Woodworking machine |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| $\stackrel{\mathscr{O}}{.}$ | －Glass processing machine |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| 弟 | －Stone cutting machine |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| ¢ | －Tire forming machine |  |  |  |  | 0 |  |  |  | 0 | 0 |
|  | －ATC |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| － | －Industrial robot |  |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 5 | －Materials handling |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| 은 | －Packing machine |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
|  | －Construction machine |  |  |  |  | 0 |  |  |  |  | 0 |
|  | －Prober | 0 |  |  |  |  |  | 0 |  | 0 |  |
| $\frac{\text { 兰 }}{\bar{O}}$ | －Wire bonder |  | 0 | 0 |  |  |  | 0 | 0 | 0 |  |
| － | －PCB driller |  |  | 0 | 0 |  |  | 0 | 0 | 0 |  |
| － | －Slicer | 0 | 0 |  |  |  |  | 0 |  |  |  |
| ¢ | －Dicer | 0 | 0 |  |  |  |  | 0 |  |  |  |
| 믇 | －Chip mounter |  |  | 0 | 0 |  |  | 0 | 0 | 0 |  |
| ． | －IC handler |  |  | 0 | 0 |  |  |  |  | 0 |  |
| हो | －Scanner |  |  | 0 | 0 |  |  |  |  | 0 |  |
| $\cdots$ | －Lithographic machine | 0 | 0 |  |  |  |  | 0 | 0 | 0 |  |
|  | －Measuring／inspection equipment | 0 | 0 | 0 | 0 |  |  |  |  | 0 |  |
|  | －Threedimensional measuring equipment | 0 | 0 | 0 | 0 |  |  | 0 | 0 | 0 |  |
|  | －Medical equipment |  | 0 | 0 | 0 |  |  |  |  | 0 | 0 |
| $\stackrel{\text { ¢ }}{ }$ | －OA equipment |  |  |  | 0 | 0 |  |  |  | 0 | 0 |
| $\bigcirc$ | －Railway cars |  |  |  |  | 0 |  |  |  | 0 | 0 |
|  | －Stage systems |  |  |  |  | 0 |  |  |  |  | 0 |
|  | －Pneumatic equipment |  |  |  | 0 | 0 |  |  |  | 0 | 0 |

Only＂slight preload（Z1，ZZ）＂and＂fine clearance（Z0，ZT）＂are available for normal grade（PN and PC）．
For interchangeable type，only accuracy grade＂PC，＂and preload（ZZ）and（ZT）are available．
Refer to Page A115 for the explanation of accuracy grade and preload．

## A-I-3.5 Available Length of Rail (single rail)

- Table I-3.5 and Table I-36 show the limitations of rail length (maximum length). However, the limitations vary by accuracy grade.

Table-I -35 Limitations of rail length (single rail)
Unit: mm

| Series |  | 05 | 07 | 09 | 12 | 15 | 20 | 25 | 30 | 35 | 45 | 55 | 65 | 85 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LH | Special high carbon steel |  |  |  |  |  | 3960 | 3960 | 4000 | 4000 | 3990 | 3960 | 3900 | 2520 |
|  | Stainless steel |  |  |  |  |  | 3500 | 3500 | 3500 |  |  |  |  |  |
| LS | Special high carbon steel |  |  |  |  | 2000 | 3960 | 3960 | 4000 | 4000 |  |  |  |  |
|  | Stainless steel |  |  |  |  | 1700 | 3500 | 3500 | 3500 | 3500 |  |  |  |  |
| LA | Special high carbon steel |  |  |  |  |  |  |  | 4000 | 4000 | 3990 | 3960 | 3900 |  |
| LY | Special high carbon steel |  |  |  |  | 2000 | 2000 | 2200 | 3000 | 3000 | 3000 | 3000 | 3000 |  |
| LE | Stainless steel | 150 | 600 | 800 | 1000 | 1200 |  |  |  |  |  |  |  |  |
| LU | Special high carbon steel |  |  | 1200 | 1800 | 2000 |  |  |  |  |  |  |  |  |
|  | Stainless steel | 210 | 375 | 600 | 800 | 1000 |  |  |  |  |  |  |  |  |

Table-I -36 Length limitations of LW Series rails
Unit: mm

| Series | Size <br> Material | 17 | 21 | 27 | 35 | 50 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LW | Special high carbon steel | 1000 | 1600 | 2000 | 2400 | 3000 |

- Rails can be butted if user requirement exceeds the rail length shown in the Table. Please consult NSK.
- Exclusive butting rails are standardized and stocked for interchangeable type in LH and LS Series.
Rail designation code of LH butting rail specification : L1H304000-01Z
(Non-butting rail specification: L1H304000Z)
Rail designation code of LS butting rail specification
: L1S304000J Z
(Non-butting rail specification: L1S304000Z)
$\square$


## A-I -4 When Placing Orders

## A-I-4.1 Specification Number and Reference Number

Specification number : Use a number for inquiry prior to finalize specifications. A code indicates a general specification of the item. Codes are a great help when you need an estimate or when you desire to discuss specifications with us.

## (1) Preloaded assembly

(A) Specification number

Reference number: Alpha-numeric codes are assigned to identify each linear guide assembly after all specifications are finalized.
A reference number appears in the specification drawing for user reference. Use this number when placing an order.

(B) Reference number (Series: LH, LA, LY, LW, LE, LU)


Table I-4•1 Material/surface treatment code

| Code | Description |
| :---: | :---: |
| C | Special high carbon steel (NSK standard) |
| K | Stainless steel |
| D | Special high carbon steel with <br> surface treatment |
| H | Stainess steel with surface treatment |
| $\mathbf{Z}$ | Other, special |

## (2) Interchangeable type

(A) Rails and ball slides as a single item

| Component | Preload | Butting or non-butting rail | Material | Reference number (example) |
| :---: | :---: | :---: | :---: | :---: |
| Rail | Slight preload | Regular rail | Special high carbon steel | L1H301240-Z |
|  |  |  | Stainless steel | L1H301240-SZ |
|  |  | Butting rail | Special high carbon steel | L1H304000-01Z |
|  | Fine clearance | Regular rail | Special high carbon steel | L1H301240 |
|  |  |  | Stainless steel | L1H301240S |
|  |  | Butting rail | Special high carbon steel | L1H304000-01 |
| Ball slide | Slight preload | - | Special high carbon steel | LAH30ELZ |
|  |  |  | Stainless steel | LAH30ELSZ |
|  | Fine clearance | - | Special high carbon steel | LAH30EL |
|  |  |  | Stainless steel | LAH30ELS |

(B) Assembled item with rail and ball slide (specification number)

| LH301200 ANC2-PC Z - 2 - I |  |
| :---: | :---: |
| $\begin{aligned} & \text { Series } \\ & \text { (See Table I-2•2) } \end{aligned}$ | $-\quad$II refers to a set of two <br> rails; no code refers to one |
| Size | Slight preload ZZ, fine clearance Z (See Table I-302) |
| Rail length (mm) | Accuracy grade: normal grade PC (See Table I-3•1) |
| Ball slide shape/height (See Table I-2•3) | Number of ball slides per rail |
|  | Material/surface treatment (See Table I-4•1) |

(C) Assembled item with rail andball slide (reference number)


Note:Interchangeable assemblies are available only to the normal grade (PC).

## A-I-4.2 Reference Number of the Standardized Linear Guide in Stock

- NSK keeps a stock of standardized linear guides. Refer to Tables I-4•2 to I-4•15 for their reference numbers.
- For easy ordering, use the reference number of the standardized linear guide in stock.

Table I-4•2 Standardized LH Series in stock (Interchangeable part)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rail G* dimension |  |  |
| LH2O | Special high carbon steel | Interchangeable with fine clearance | L1H200220 <br> L1H200280 <br> L1H200340 <br> L1H200460 <br> L1H200640 <br> L1H200820 <br> L1H201000 <br> L1H201240 | 20 | LAH2OAN <br> LAH20EL <br> LAH2OFL | LAH20BN <br> LAH20GL <br> LAH20HL |
|  |  | Interchangeable with preload | L1H200220Z <br> L1H200280Z <br> L1H200340Z <br> L1H200460Z <br> L1H200640Z <br> L1H200820Z <br> L1H201000Z <br> L1H201240Z |  | LAH2OANZ <br> LAH20ELZ <br> LAH20FLZ | LAH2OBNZ <br> LAH20GLZ <br> LAH20HLZ |
|  | Stainless steel | Interchangeable with fine clearance | L1H200220S <br> L1H200280S <br> L1H200340S <br> L1H200460S <br> L1H200640S <br> L1H200820S <br> L1H201000S <br> L1H201240S |  | LAH2OANS <br> LAH20ELS <br> LAH20FLS | LAH20BNS <br> LAH20GLS <br> LAH2OHLS |
|  |  | Interchangeable with preload | L1H200220SZ <br> L1H200280SZ <br> L1H200340SZ <br> L1H200460SZ <br> L1H200640SZ <br> L1H200820SZ <br> L1H201000SZ <br> L1H201240SZ |  | $\begin{aligned} & \text { LAH2OANSZ } \\ & \text { LAH20ELSZ } \\ & \text { LAH20FLSZ } \end{aligned}$ | LAH20BNSZ <br> LAH20GLSZ <br> LAH2OHLSZ |

* Refer to the dimension tables for the rail dimension $\mathbf{G}$.

Table I-4•3 Standardized LH Series in stock (Interchangeable part)

| Model | Material | Interchangeabletype | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \text { Rail G* } \\ \text { dimension } \\ \hline \hline \end{gathered}$ |  |  |
| LH25 | Special high carbon steel | Interchangeable with fine clearance | L1H250220 <br> L1H250280 <br> L1H250340 <br> L1H250460 <br> L1H250640 <br> L1H250820 <br> L1H251000 <br> L1H251240 | 20 | LAH25AN <br> LAH25EL <br> LAH25FL | LAH25BN <br> LAH25GL <br> LAH25HL |
|  |  | Interchangeable with preload | L1H250220Z <br> L1H250280Z <br> L1H250340Z <br> L1H250460Z <br> L1H250640Z <br> L1H250820Z <br> L1H251000Z <br> L1H251240Z |  | $\begin{aligned} & \text { LAH25ANZ } \\ & \text { LAH25ELZ } \\ & \text { LAH25FLZ } \end{aligned}$ | LAH25BNZ <br> LAH25GLZ <br> LAH25HLZ |
|  | Stainless steel | Interchangeable with fine clearance | L1H250220S <br> L1H250280S <br> L1H250340S <br> L1H250460S <br> L1H250640S <br> L1H250820S <br> L1H251000S <br> L1H251240S |  | LAH25ANS <br> LAH25ELS <br> LAH25FLS | LAH25BNS <br> LAH25GLS <br> LAH25HLS |
|  |  | Interchangeable with preload | L1H250220SZ <br> L1H250280SZ <br> L1H250340SZ <br> L1H250460SZ <br> L1H250640SZ <br> L1H250820SZ <br> L1H251000SZ <br> L1H251240SZ |  | LAH25ANSZ <br> LAH25ELSZ <br> LAH25FLSZ | LAH25BNSZ <br> LAH25GLSZ <br> LAH25HLSZ |

[^0]Table I-44 Standardized LH Series in stock (Interchangeable part)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rail G* dimension |  |  |
| LH30 | Special high carbon steel | $\begin{aligned} & \text { Interchangeable } \\ & \text { with } \\ & \text { fine clearance } \end{aligned}$ | L1H300280 <br> L1H300440 <br> L1H300600 <br> L1H300760 <br> L1H301000 <br> L1H301240 | 20 | LAH30AN <br> LAH30EL <br> LAH3OFL | LAH30BN <br> LAH30GL <br> LAH30HL |
|  |  | Interchangeable with preload | $\begin{aligned} & \text { L1H300280Z } \\ & \text { L1H300440Z } \\ & \text { L1H300600Z } \\ & \text { L1H300760Z } \\ & \text { L1H301000Z } \\ & \text { L1H301240Z } \end{aligned}$ |  | LAH30ANZ <br> LAH30ELZ <br> LAH30FLZ | LAH30BNZ <br> LAH30GLZ <br> LAH3OHLZ |
|  | Stainless steel | $\begin{aligned} & \text { Interchangeable } \\ & \text { with } \\ & \text { fine clearance } \end{aligned}$ | L1H300280S <br> L1H300440S <br> L1H300600S <br> L1H300760S <br> L1H301000S <br> L1H301240S |  | LAH3OANS <br> LAH30ELS <br> LAH30FLS | LAH3OBNS <br> LAH30GLS <br> LAH3OHLS |
|  |  | Interchangeable with preload | L1H300280SZ <br> L1H300440SZ <br> L1H300600SZ <br> L1H300760SZ <br> L1H301000SZ <br> L1H301240SZ |  | LAH30ANSZ <br> LAH30ELSZ <br> LAH30FLSZ | LAH30BNSZ <br> LAH30GLSZ <br> LAH30HLSZ |
| LH35 | Special high carbon steel | $\begin{gathered} \text { Interchangeable } \\ \text { with } \\ \text { fine clearance } \end{gathered}$ | L1H350280 <br> L1H350440 <br> L1H350600 <br> L1H350760 <br> L1H351000 <br> L1H351240 | 20 | LAH35AN <br> LAH35EL <br> LAH35FL | LAH35BN <br> LAH35GL <br> LAH35HL |
|  |  | Interchangeable with preload | L1H350280Z <br> L1H350440Z <br> L1H350600Z <br> L1H350760Z <br> L1H351000Z <br> L1H351240Z |  | LAH35ANZ <br> LAH35ELZ <br> LAH35FLZ | LAH35BNZ <br> LAH35GLZ <br> LAH35HLZ |

* Refer to the dimension tables for the rail dimension $\mathbf{G}$.

Table I-4.5 Standardized LH Series in stock (Interchangeable part)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \text { Rail G } \\ \text { dimension } \end{gathered}$ |  |  |
| LH45 | Special high carbon steel | Interchangeable with fine clearance | - | - | LAH45AN LAH45EL LAH45FL | LAH45BN <br> LAH45GL <br> LAH45HL |
|  |  | Interchangeable with preload | - |  | LAH45ANZ <br> LAH45ELZ <br> LAH45FLZ | LAH45BNZ <br> LAH45GLZ <br> LAH45HLZ |
| LH55 | Special high carbon steel | Interchangeable with fine clearance | - | - | LAH55AN LAH55EL LAH55FL | LAH55BN LAH55GL LAH55HL |
|  |  | Interchangeable with preload | - |  | LAH55ANZ <br> LAH55ELZ <br> LAH55FLZ | LAH55BNZ <br> LAH55GLZ <br> LAH55HLZ |
| LH65 | Special high carbon steel | Interchangeable with fine clearance | - | - | LAH65AN <br> LAH65EL <br> LAH65FL | LAH65BN LAH65GL LAH65HL |
|  |  | Interchangeable with preload | - |  | LAH65ANZ <br> LAH65ELZ <br> LAH65FLZ | LAH65BNZ <br> LAH65GLZ <br> LAH65HLZ |

Rails of LH45 and larger are not standardized stock.

Table I-4.6 Standardized LS Series in stock (Interchangeable part)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rail G* dimension |  |  |
| LS15 | Special high carbon steel | Interchangeable with fine clearance | L1S150160(T)** L1S150220(T)** L1S150280(T)** L1S150340(T)** L1S150460(T)** L1S150640(T)** L1S150820(T)** L1S151000(T)** | 20 | LAS15AL <br> LAS15EL <br> LAS15FL | $\begin{aligned} & \text { LAS15CL } \\ & \text { LAS15KL } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S150160TZ L1S150220TZ L1S150280TZ L1S150340TZ L1S150460TZ L1S150640TZ L1S150820TZ L1S151000TZ |  | $\begin{aligned} & \text { LAS15ALZ } \\ & \text { LAS15ELZ } \\ & \text { LAS15FLZ } \end{aligned}$ | LAS15CLZ <br> LAS15KLZ |
|  | Stainless steel | Interchangeable with fine clearance | L1S150160TS L1S150220TS L1S150280TS L1S150340TS L1S150460TS L1S150640TS L1S150820TS L1S151000TS |  | LAS15ALS <br> LAS15ELS <br> LAS15FLS | LAS15CLS LAS15KLS |
|  |  | Interchangeable with preload | L1S150160STZ L1S150220STZ L1S150280STZ L1S150340STZ L1S150460STZ L1S150640STZ L1S150820STZ L1S151000STZ |  | LAS15ALSZ LAS15ELSZ LAS15FLSZ | LAS15CLSZ LAS15KLSZ |

[^1]Table I-4•7 Standardized LS Series in stock (Interchangeable part)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rail G* dimension |  |  |
| LS20 | Special high carbon steel | Interchangeable with fine clearance | L1S200220 L1S200280 L1S200340 L1S200460 L1S200640 L1S200820 L1S201000 L1S201240 | 20 | $\begin{aligned} & \text { LAS20AL } \\ & \text { LAS20EL } \\ & \text { LAS20FL } \end{aligned}$ | $\begin{aligned} & \text { LAS20CL } \\ & \text { LAS20KL } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S200220Z L1S200280Z L1S200340Z L1S200460Z L1S200640Z L1S200820Z L1S201000Z L1S201240Z |  | $\begin{aligned} & \text { LAS20ALZ } \\ & \text { LAS20ELZ } \\ & \text { LAS20FLZ } \end{aligned}$ | $\begin{aligned} & \text { LAS20CLZ } \\ & \text { LAS20KLZ } \end{aligned}$ |
|  | Stainless steel | Interchangeable with fine clearance | L1S200220S <br> L1S200280S <br> L1S200340S <br> L1S200460S <br> L1S200640S <br> L1S200820S <br> L1S201000S <br> L1S201240S |  | LAS20ALS <br> LAS20ELS <br> LAS20FLS | LAS20CLS LAS20KLS |
|  |  | Interchangeable with preload | L1S200220SZ L1S200280SZ L1S200340SZ L1S200460SZ L1S200640SZ L1S200820SZ L1S201000SZ L1S201240SZ |  | $\begin{aligned} & \text { LAS20ALSZ } \\ & \text { LAS20ELSZ } \\ & \text { LAS20FLSZ } \end{aligned}$ | LAS20CLSZ LAS20KLSZ |

[^2]Table I-48 Standardized LS Series in stock (randomly-matching items)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rail G* dimension |  |  |
| LS25 | Special high carbon steel | $\begin{aligned} & \text { Interchangeable } \\ & \text { with } \\ & \text { fine clearance } \end{aligned}$ | L1S250220 L1S250280 L1S250340 L1S250460 L1S250640 L1S250820 L1S251000 L1S251240 | 20 | LAS25AL <br> LAS25EL <br> LAS25FL | $\begin{aligned} & \text { LAS25CL } \\ & \text { LAS25KL } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S250220Z <br> L1S250280Z <br> L1S250340Z <br> L1S250460Z <br> L1S250640Z <br> L1S250820Z <br> L1S251000Z <br> L1S251240Z |  | LAS25ALZ <br> LAS25ELZ <br> LAS25FLZ | $\begin{aligned} & \text { LAS25CLZ } \\ & \text { LAS25KLZ } \end{aligned}$ |
|  | Stainless steel | Interchangeable with fine clearance | L1S250220S <br> L1S250280S <br> L1S250340S <br> L1S250460S <br> L1S250640S <br> L1S250820S <br> L1S251000S <br> L1S251240S |  | LAS25ALS <br> LAS25ELS <br> LAS25FLS | $\begin{aligned} & \text { LAS25CLS } \\ & \text { LAS25KLS } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S250220SZ L1S250280SZ L1S250340SZ L1S250460SZ L1S250640SZ L1S250820SZ L1S251000SZ L1S251240SZ |  | LAS25ALSZ LAS25ELSZ LAS25FLSZ | $\begin{aligned} & \text { LAS25CLSZ } \\ & \text { LAS25KLSZ } \end{aligned}$ |

[^3]Table I-4.9 Standardized LS Series in stock (Interchangeable part)

| Model | Material | Interchangeable type | Rail reference number |  | Ball slide reference number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Rail G* dimension |  |  |
| LS30 | Special high carbon steel | $\begin{gathered} \text { Interchangeable } \\ \text { with } \\ \text { fine clearance } \end{gathered}$ | $\begin{aligned} & \text { L1S300280 } \\ & \text { L1S300440 } \\ & \text { L1S300600 } \\ & \text { L1S300760 } \\ & \text { L1S } 301000 \\ & \text { L1S301240 } \end{aligned}$ | 20 | LAS30AL <br> LAS30EL <br> LAS30FL | $\begin{aligned} & \text { LAS30CL } \\ & \text { LAS30KL } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S300280Z <br> L1S300440Z <br> L1S300600Z <br> L1S300760Z <br> L1S301000Z <br> L1S301240Z |  | LAS30ALZ <br> LAS30ELZ <br> LAS30FLZ | $\begin{aligned} & \text { LAS30CLZ } \\ & \text { LAS30KLZ } \end{aligned}$ |
|  | Stainless steel | $\begin{gathered} \text { Interchangeable } \\ \text { with } \\ \text { fine clearance } \end{gathered}$ | L1S300280S <br> L1S300440S <br> L1S300600S <br> L1S300760S <br> L1S301000S <br> L1S301240S |  | LAS30ALS <br> LAS30ELS <br> LAS30FLS | $\begin{aligned} & \text { LAS30CLS } \\ & \text { LAS30KLS } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S300280SZ <br> L1S300440SZ <br> L1S300600SZ <br> L1S300760SZ <br> L1S301000SZ <br> L1S301240SZ |  | $\begin{aligned} & \text { LAS30ALSZ } \\ & \text { LAS30ELSZ } \\ & \text { LAS30FLSZ } \end{aligned}$ | $\begin{aligned} & \text { LAS30CLSZ } \\ & \text { LAS30KLSZ } \end{aligned}$ |
| LS35 | Special high carbon steel | $\begin{gathered} \text { Interchangeable } \\ \text { with } \\ \text { fine clearance } \end{gathered}$ | L1S350280 L1S350440 L1S350600 L1S350760 L1S351000 L1S351240 | 20 | LAS35AL <br> LAS35EL <br> LAS35FL | $\begin{aligned} & \text { LAS35CL } \\ & \text { LAS35KL } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S350280Z L1S350440Z L1S350600Z L1S350760Z L1S351000Z L1S351240Z |  | LAS35ALZ <br> LAS35ELZ <br> LAS35FLZ | $\begin{aligned} & \text { LAS35CLZ } \\ & \text { LAS35KLZ } \end{aligned}$ |
|  | Stainless steel | $\begin{gathered} \text { Interchangeable } \\ \text { with } \\ \text { fine clearance } \end{gathered}$ | L1S350280S <br> L1S350440S <br> L1S350600S <br> L1S350760S <br> L1S351000S <br> L1S351240S |  | LAS35ALS <br> LAS35ELS <br> LAS35FLS | $\begin{aligned} & \text { LAS35CLS } \\ & \text { LAS35KLS } \end{aligned}$ |
|  |  | Interchangeable with preload | L1S350280SZ <br> L1S350440SZ <br> L1S350600SZ <br> L1S350760SZ <br> L1S351000SZ <br> L1S351240SZ |  | LAS35ALSZ <br> LAS35ELSZ <br> LAS35FLSZ | $\begin{aligned} & \text { LAS35CLSZ } \\ & \text { LAS35KLSZ } \end{aligned}$ |

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Table I -4-10 Standardized LW Series in stock (Preloaded assembly)

| Model | Material | Reference number |  | Rail dimension (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Z0 preload | Z1 preload | Rail length | G* dimension |
| LW17EL | Special high carbon steel | LW170510EL2A01PNZO LW170750EL2A01PNZO LW170990EL2A01PNZO | LW170510EL2A02PNZ1 LW170750EL2A02PNZ1 LW170990EL2A02PNZ1 | $\begin{aligned} & 510 \\ & 750 \\ & 990 \end{aligned}$ | 15 |
| LW21EL | Special high carbon steel | LW210530EL2A01PNZ0 LW211030EL2A01PNZ0 LW211530EL2A01PNZ0 | LW210530EL2A02PNZ1 LW211030EL2A02PNZ1 LW211530EL2A02PNZ1 | $\begin{gathered} 530 \\ 1030 \\ 1530 \end{gathered}$ | 15 |
| LW27EL | Special high carbon steel | LW270520EL2A01PNZ0 LW271000EL2A01PNZ0 LW271540EL2A01PNZO | LW270520EL2A02PNZ1 LW271000EL2A02PNZ1 LW271540EL2A02PNZ1 | $\begin{gathered} 520 \\ 1000 \\ 1540 \end{gathered}$ | 20 |
| LW35EL | Special high carbon steel | LW351000EL2A01PNZ0 LW351560EL2A01PNZ0 LW352040EL2A01PNZ0 | LW351000EL2A01PNZ1 LW351560EL2A01PNZ1 LW352040EL2A01PNZ1 | $\begin{aligned} & 1000 \\ & 1560 \\ & 2040 \end{aligned}$ | 20 |
| LW50EL | Special high carbon steel | LW501000EL2A01PNZ0 LW501560EL2A01PNZ0 LW502040EL2A01PNZO | LW501000EL2A01PNZ1 LW501560EL2A01PNZ1 LW502040EL2A01PNZ1 | $\begin{aligned} & 1000 \\ & 1560 \\ & 2040 \end{aligned}$ | 20 |

* Refer to the dimension tables for the rail dimension $\mathbf{G}$.

Table I-4•11 Standardized LW Series in stock (Interchangeable part)

|  |  | Interchangeable | Rail reference number |  | Ball slide reference number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Model | Material | type |  | Rail G* dimension |  |
| LW17 | Special high carbon steel | Interchangeable with fine clearance | L1W170430 <br> L1W170670 <br> L1W170990 | 15 | LAW17EL |
| LW21 | Special high carbon steel | Interchangeable with fine clearance | L1W210430 <br> L1W210680 <br> L1W210980 | 15 | LAW21EL |
| LW27 | Special high carbon steel | Interchangeable with fine clearance | L1W270460 <br> L1W270640 <br> L1W270820 <br> L1W271000 | 20 | LAW27EL |
| LW35 | Special high carbon steel | Interchangeable with fine clearance | L1W350440 <br> L1W350600 <br> L1W350760 <br> L1W351000 <br> L1W351240 | 20 | LAW35EL |
| LW50 | Special high carbon steel | Interchangeable with fine clearance | L1W500440 <br> L1W500600 <br> L1W500760 <br> L1W501000 <br> L1W501240 | 20 | LAW50EL |

[^5]Table I-4•12 Standardized LE Series in stock (Preloaded assembly)

| Model | M aterial | Reference number |  | Rail dimension (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Z0 preload | Z1 preload | Rail length | $\mathrm{G}^{*}$ dimension |
| LE07AL | Stainless steel | LE070110AL2AS7PNZ0 | LE070110AL2AS8P6Z1 | 110 | 10 |
|  |  | LE070200AL2AS7PNZ0 | LE070200AL2AS8P6Z1 | 200 |  |
|  |  | LE070290AL2AS7PNZ0 | LE070290AL2AS8P6Z1 | 290 |  |
| LE09AL | Stainless steel | LE090110AL2A70PNZ0 | LE090110AL2A61P6Z1 | 110 | 10 |
|  |  | LE090200AL2A 70PNZ0 | LE090200AL2A61P6Z1 | 200 |  |
|  |  | LE090290AL2A70PNZ0 | LE090290AL2A61P6Z1 | 290 |  |
| LE09TL | Stainless steel | LE090110TL2AS7PNZ0 | LE090110TL2AS8P6Z1 | 110 | 10 |
|  |  | LE090200TL2AS7PNZ0 | LE090200TL2AS8P6Z1 | 200 |  |
|  |  | LE090290TL2AS7PNZ0 | LE090290TL2AS8P6Z1 | 290 |  |
| LE12AL | Stainless steel | LE120150AL2AS7PNZ0 | LE120150AL2AS8P6Z1 | 150 | 15 |
|  |  | LE120310AL2AS7PNZ0 | LE120310AL2AS8P6Z1 | 310 |  |
|  |  | LE120470AL2AS7PNZ0 | LE120470AL2AS8P6Z1 | 470 |  |
| LE15AL | Stainless steel | LE150230AL2AS7PNZ0 | LE150230AL2AS8P6Z1 | 230 | 15 |
|  |  | LE150430AL2AS7PNZO | LE150430AL2AS8P6Z1 | 430 |  |
|  |  | LE150670AL2AS7PNZ0 | LE150670AL2AS8P6Z1 | 670 |  |

* Refer to the dimension tables for the rail dimension $\mathbf{G}$.

Table I-4•13 Standardized LE Series in stock (Interchangeable part)

|  |  | Interchangeable | Rail reference number |  | Ball slide reference number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mo | M | type |  | Rail G* dimension |  |
| LE09 | Stainless steel | Interchangeable with fine clearance | L1E090110S <br> L1E090200S <br> L1E090290S <br> L1E090380S | 10 | LAE09AR LAE09TR |
| LE12 | Stainless steel | Interchangeable with fine clearance | L1E120150S <br> L1E120310S <br> L1E120470S <br> L1E120790S | 15 | LAE12AR |
| LE15 | Stainless steel | Interchangeable with fine clearance | L1E150230S <br> L1E150430S <br> L1E150670S <br> L1E150990S | 15 | LAE15AR |

* Refer to the dimension tables for the rail dimension G.

Table I-4•14 Standardized LU Series in stock (Preloaded assembly)

| Model | Material | Reference number |  | Rail dimension (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Z0 preload | Z1 preload | Rail length | G* dimension |
| LU07AL | Special high carbon steel | LU070085AL2AS7PNZ0 LU070145AL2AS7PNZ0 LU070235AL2AS7PNZ0 | LU070085AL2AS8P6Z1 LU070145AL2AS8P6Z1 LU070235AL2AS8P6Z1 | $\begin{gathered} \hline 85 \\ 145 \\ 235 \\ \hline \end{gathered}$ | 5 |
| LU09AL | Special high carbon steel | LU090115AL2A70PNZ0 LU090195AL2A70PNZ0 LU090275AL2A70PNZ0 | $\begin{aligned} & \text { LU090115AL2A61P6Z1 } \\ & \text { LU090195AL2A61P6Z1 } \\ & \text { LU090275AL2A61P6Z1 } \end{aligned}$ | $\begin{aligned} & 115 \\ & 195 \\ & 275 \end{aligned}$ | 7.5 |
|  | Stainless steel | LU090115AL2AS7PNZ0 LU090195AL2AS7PNZ0 LU090275AL2AS7PNZ0 | LU090115AL2AS8P6Z1 LU090195AL2AS8P6Z1 LU090275AL2AS8P6Z1 | $\begin{aligned} & 115 \\ & 195 \\ & 275 \\ & \hline \end{aligned}$ | 7.5 |
| LU09TL | Stainless steel | LU090115TL2AS7PNZ0 LU090195TL2AS7PNZ0 LU090275TL2AS7PNZ0 | LU090115TL2AS8P6Z1 LU090195TL2AS8P6Z1 LU090275TL2AS8P6Z1 | $\begin{aligned} & \hline 115 \\ & 195 \\ & 275 \\ & \hline \end{aligned}$ | 7.5 |
| LU12AL | Special high carbon steel | LU120170AL2A70PNZ0 LU120270AL2A70PNZ0 LU120470AL2A70PNZ0 | LU120170AL2A61P6Z1 LU120270AL2A61P6Z1 LU120470AL2A61P6Z1 | $\begin{aligned} & \hline 170 \\ & 270 \\ & 470 \\ & \hline \end{aligned}$ | 10 |
|  | Stainless steel | LU120170AL2AS7PNZ0 LU120270AL2AS7PNZ0 LU120470AL2AS7PNZ0 | LU120170AL2AS8P6Z1 LU120270AL2AS8P6Z1 LU120470AL2AS8P6Z1 | $\begin{aligned} & 170 \\ & 270 \\ & 470 \\ & \hline \end{aligned}$ | 10 |
| LU12TL | Special high carbon steel | LU120170TL2A70PNZ0 LU120270TL2A70PNZ0 LU120470TL2A70PNZ0 | LU120170TL2A61P6Z1 LU120270TL2A61P6Z1 LU120470TL2A61P6Z1 | $\begin{aligned} & 170 \\ & 270 \\ & 470 \\ & \hline \end{aligned}$ | 10 |
|  | Stainless steel | LU120170TL2AS7PNZ0 LU120270TL2AS7PNZO LU120470TL2AS7PNZ0 | LU120170TL2AS8P6Z1 LU120270TL2AS8P6Z1 LU120470TL2AS8P6Z1 | $\begin{aligned} & \hline 170 \\ & 270 \\ & 470 \\ & \hline \end{aligned}$ | 10 |
| LU15AL | Special high carbon steel | LU150230AL2A70PNZ0 LU150430AL2A 70PNZ0 LU150670AL2A70PNZ0 | LU150230AL2A61P6Z1 LU150430AL2A61P6Z1 LU150670AL2A61P6Z1 | $\begin{aligned} & 230 \\ & 430 \\ & 670 \\ & \hline \end{aligned}$ | 15 |
|  | Stainless steel | LU150230AL2AS7PNZ0 LU150430AL2AS7PNZ0 LU150670AL2AS7PNZ0 | LU150230AL2AS8P6Z1 LU150430AL2AS8P6Z1 LU150670AL2AS8P6Z1 | $\begin{aligned} & \hline 230 \\ & 430 \\ & 670 \\ & \hline \end{aligned}$ | 15 |

[^6]Table I-4•15 Standardized LU Series in stock (Interchangeable part)

|  |  | Interchangeable | Rail reference number |  | Ball slide reference number |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | type |  | Rail G* dimension |  |
| LU09 | Stainless steel | Interchangeable with fine clearance | L1U090115S <br> L1U090195S <br> L1U090275S <br> LIU090115TS <br> L1U090195TS <br> L1U090275TS | 7.5 | LAU09ARS LAU09TRS |
| LU12 | Stainless steel | Interchangeable with fine clearance | LIU120170S <br> L1U120270S <br> L1U120470S <br> LIU120170TS <br> LIU120270TS <br> LIU120470TS | 10 | LAU12ARS LAU12TRS |
| LU15 | Special high carbon steel/ Stainless steel | Interchangeable with fine clearance | LIU150230 <br> LIU150430 <br> L1U150670 <br> L1U150990 <br> LIU150230S <br> L1U150430S <br> L1U150670S <br> L1U150990S | 15 | LAU15AL LAU15ALS |

[^7]
## A-I -5 Model Number and Dimension Table of NSK Linear Guides

## A-I-5.1 LH Series



## (1) High self-aligning capability (rolling direction)

Same as the DF combination in angular contact bearings, self-aligning capability is high because the cross point of the contact lines of balls and grooves comes inside, reducing moment rigidity.
This increases the capacity to absorb the error of installation.

## (2) High load carrying capacity to vertical direction

The contact angle is set at 50 degrees, increasing load carrying capacity as well as rigidity in vertical direction.

## (3) High resistance against shock load

The bottom ball groove is formed in gothic-arch and the center of the top and bottom grooves are offset as shown in Fig.I-5.2. The vertical load is generally carried by the top rows, at where balls are contacting at two points. Because of this design, the bottom rows will carry load when a large impact load is applied vertically as shown in Fig. I-5•3. This assures high resistance to the shock load.

## (4) Highly accurate As shown in Fig.

I-5.4, fixing the master rollers is easy thanks to the gothic-arch groove. This makes easy and accurate measuring of ball grooves.

## (5) Interchangeable rail and ball slide (prompt delivery)

Randomly matching rails and ball slides are stocked as standardized interchangeable items. This reduces delivery time.

## (6) Easy to handle, and designed with safety in mind.

Balls are retained in the retainer, therefore they do not fall out when theball slider is withdrawn from the rail.

## (7) Abundant models and sizes

Each series has various models of ball slides, rendering the linear guide available for numerous uses.


Fig. I-5.1 LH Series


Fig. I-5.2 Enlarged illustration of the offset gothic-arch


Fig. I-5.3 When load is applied


Fig. I-5.4 Rail grinding and measuring

## Dimensions of LH Series (Preloaded assembly)

LH-AN (High load type)

## LH-BN (Super high load type)

- Specification number of preloaded assembly
(Custom made assembly)
LH35 0840 AN C $2-$ PN Z O-II II refers to a set of 2

Model
Rail length (mm
Ball slide shape
Material/surface treatment
(See Page A24)

- C: Standard material
- K: Stainless steel
(only for LH2O-30)
Number of ball slides per rail


> Accuracy grade -PN normal grade -P6 precision grade -P5 high precision grade -P4 super precision grade -P3 ultra precision grade

Table. I-5॰1

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width$w$ | Length <br> L | M ounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
|  | 30 | 5 | 12 | 44 | $\begin{aligned} & 69.8 \\ & 91.8 \end{aligned}$ | 32 | 36 <br> 50 | M 5 x $0.8 \times 6$ | 6 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | $\begin{array}{\|c} 7 \\ 11 \end{array}$ | 25 | 12 | M 6×0.75 | 5 | 11 |
|  | 40 | 7 | 12.5 | 48 | $\begin{gathered} 79 \\ 107 \end{gathered}$ | 35 | $\begin{aligned} & 35 \\ & 50 \end{aligned}$ | M $6 \times 1 \times 9$ | 6.5 | $\begin{aligned} & 58 \\ & 86 \end{aligned}$ | $\left.\begin{array}{\|l\|} 11.5 \\ 18 \end{array} \right\rvert\,$ | 33 | 12 | M 6×0.75 | 10 | 11 |
|  | 45 | 9 | 16 | 60 | $\begin{gathered} 85.6 \\ 124.6 \end{gathered}$ | 40 | $\begin{aligned} & 40 \\ & 60 \end{aligned}$ | $\mathrm{M} 8 \times 1.25 \times 10$ | 10 | $\begin{aligned} & 59 \\ & 98 \end{aligned}$ | $\left.\begin{gathered} 9.5 \\ 19 \end{gathered} \right\rvert\,$ | 36 | 14 | M 6×0.75 | 10 | 11 |
|  | 55 | 9.5 | 18 | 70 | $\begin{aligned} & 109 \\ & 143 \end{aligned}$ | 50 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{array}{\|c\|} \hline 80 \\ 114 \\ \hline \end{array}$ | $15$ $21$ | 45.5 | 15 | M 6×0.75 | 15 | 11 |
|  | 70 | 14 | 20.5 | 86 | $139$ <br> 171 | 60 | 60 <br> 60 <br> 80 | M $10 \times 1.5 \times 17$ | 13 | $\left\lvert\, \begin{aligned} & 105 \\ & 137 \end{aligned}\right.$ | $\begin{aligned} & 22.5 \\ & 28.5 \\ & \hline \end{aligned}$ | 56 | 17 | PT1/8 | 20 | 13 |
|  | 80 | 15 | 23.5 | 100 | $\begin{aligned} & 163 \\ & 201 \end{aligned}$ | 75 | $75$ <br> 95 | M $12 \times 1.75 \times 18$ | 12.5 | $\begin{aligned} & 126 \\ & 164 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} 25.5 \\ 34.5 \\ \hline \end{array}$ | 65 | 18 | PT1/8 | 21 | 13 |
|  | 90 | 16 | 31.5 | 126 | $\begin{aligned} & 193 \\ & 253 \end{aligned}$ | 76 | $\begin{aligned} & 70 \\ & 120 \end{aligned}$ | M 16×2×20 | 25 | $\left\lvert\, \begin{aligned} & 147 \\ & 207 \end{aligned}\right.$ | $\left\|\begin{array}{l} 38.5 \\ 48.5 \end{array}\right\|$ | 74 | 23 | PT1/8 | 19 | 13 |

## Preload code <br> - ZO fine clearance <br> - Z1 slight preload

.73 medium pread


Unit: mm

| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width <br> $W_{1}$ | Height <br> $H_{1}$ | Pitch <br> F | Mounting bolt hole$d \times D \times h$ | $B_{3}$ | $\begin{gathered} \mathrm{G} \\ \left.\begin{array}{c} \text { (recomm } \\ \text { ended) } \end{array} \right\rvert\, \end{gathered}$ | Max. length Lomax. stánless | Dynamic Static <br> $C$ $C_{0}$ <br> $(N[k g f])$  |  | Static moment |  |  | $D_{\text {w }}$ | Ball slide (kg) |  |
|  |  |  |  |  |  |  |  |  | $\begin{aligned} & M_{\mathrm{RO}} \\ & (\mathrm{~N} \end{aligned}$ | $\begin{gathered} M_{\mathrm{Po}} \\ \mathrm{~m}[\mathrm{kgf} . \end{gathered}$ | $\begin{gathered} M_{\mathrm{Yo}} \\ \mathrm{~m}]) \end{gathered}$ |  |  |  |
| 20 | 18 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & \hline 14200 \\ & {[1450]} \\ & 18200 \\ & {[1860]} \\ & \hline \end{aligned}$ | 25100 $[2560]$ 39500 $[4020]$ | $\begin{aligned} & 216 \\ & {[22]} \\ & 305 \\ & {[31]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 345 \\ & {[35]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 345 \\ & {[35]} \end{aligned}$ | 3.968 | $\begin{aligned} & 0.33 \\ & 0.48 \end{aligned}$ | 2.6 |
| 23 | 22 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & \hline 21000 \\ & {[2140]} \\ & 26900 \\ & {[2740]} \\ & \hline \end{aligned}$ | 39000 $[4000]$ 52500 $[5340]$ | 355 $[36]$ 470 $[48]$ | $\begin{aligned} & 315 \\ & {[32]} \\ & 530 \\ & {[54]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 305 \\ & {[31]} \\ & 520 \\ & {[53]} \\ & \hline \end{aligned}$ | 4.762 | $\begin{aligned} & 0.55 \\ & 0.82 \end{aligned}$ | 3.6 |
| 28 | 26 | 80 | $9 \times 14 \times 12$ | 14 | 20 | $\begin{gathered} 4000 \\ (3500) \end{gathered}$ | $\begin{aligned} & \hline 25700 \\ & {[2620]} \\ & 37500 \\ & {[3800]} \\ & \hline \end{aligned}$ | 45000 $[4570]$ 71500 $[7310]$ | $\begin{aligned} & 490 \\ & {[50]} \\ & 785 \\ & {[80]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & 845 \\ & {[86]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 355 \\ & {[36]} \\ & 835 \\ & {[85]} \\ & \hline \end{aligned}$ | 5.556 | $\begin{aligned} & 0.77 \\ & 1.3 \end{aligned}$ | 5.2 |
| 34 | 29 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 4000 | 39000 $[3960]$ 49500 $[5060]$ | 68500 $[7010]$ 97500 $[9930]$ | $\begin{gathered} 940 \\ {[96]} \\ 1330 \\ {[136]} \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline 735 \\ {[75]} \\ 1410 \\ {[144]} \\ \hline \end{array}$ | $\begin{gathered} \hline 715 \\ {[73]} \\ 1380 \\ {[141]} \end{gathered}$ | 6.350 | $\begin{aligned} & 1.5 \\ & 2.1 \end{aligned}$ | 7.2 |
| 45 | 38 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3990 | $\begin{aligned} & \hline 66000 \\ & {[6740]} \\ & 79500 \\ & {[8130]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 119000 \\ & {[12100]} \\ & 146000 \\ & {[14900]} \end{aligned}$ | $\begin{aligned} & 2120 \\ & {[216]} \\ & 2590 \\ & {[264]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1670 \\ & {[170]} \\ & 2460 \\ & {[251]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1650 \\ & {[168]} \\ & 2430 \\ & {[248]} \\ & \hline \end{aligned}$ | 7.937 | 3 $3.9$ | 12.3 |
| 53 | 44 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3960 | $\begin{aligned} & 97500 \\ & {[9940]} \\ & 118000 \\ & {[12000]} \\ & \hline \end{aligned}$ | $\left[\begin{array}{l}168000 \\ {[17100]} \\ 207000 \\ {[21100]}\end{array}\right]$ | $\begin{aligned} & 3600 \\ & {[367]} \\ & 4400 \\ & {[449]} \end{aligned}$ | $\begin{aligned} & 2870 \\ & {[293]} \\ & 4250 \\ & {[435]} \end{aligned}$ | $\begin{aligned} & 2820 \\ & {[288]} \\ & 4150 \\ & {[426]} \\ & \hline \end{aligned}$ | 9.525 | $\begin{aligned} & 4.7 \\ & 6.1 \end{aligned}$ | 16.9 |
| 63 | 53 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3900 | 150000 $[15100]$ 189000 $[19300]$ | $\left[\begin{array}{l}240000 \\ {[24500]} \\ 320000 \\ {[32700]}\end{array}\right.$ | $\begin{aligned} & \hline 6150 \\ & {[629]} \\ & 8150 \\ & {[834]} \end{aligned}$ | $\begin{aligned} & 4850 \\ & {[495]} \\ & 8350 \\ & {[850]} \end{aligned}$ | $\begin{aligned} & \hline 4750 \\ & {[484]} \\ & 8150 \\ & {[830]} \end{aligned}$ | 11.906 | $\begin{gathered} 7.7 \\ 10.8 \end{gathered}$ | 24.3 |

## LH-EL (High load type)

## LH-GL (Super high load type)

- Specification number of preloaded assembly
(Custom made assembly)

LH35 0840 EL C 2 -PN ZO-II II refers to a set of 2
Modelel
number
Rail length (mm)
Ball slide shape
Material/surface treatment
(See Page A24)

- C: Standard material
- K: Stainless steel
(only for LH2O-30)


## Accuracy grade <br> ${ }^{-}$PN normal grade <br> - P5 high precision grade <br> - P4 super precision grade

Table. I -5•2

| M odel No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Height } \\ H \end{gathered}$ | E | $W_{2}$ | $\begin{array}{c\|} \hline \text { Width } \\ w \\ \hline \end{array}$ | Length$L$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LH20EL <br> LH20GL | 30 | 5 | 21.5 | 63 | $\begin{aligned} & 69.8 \\ & 91.8 \end{aligned}$ | 53 | 40 | M $6 \times 1 \times 10$ | 5 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | $\begin{array}{r} 5 \\ 16 \end{array}$ | 25 | 10 | M 6×0.75 | 5 | 11 |
| LH25EL LH25GL | 36 | 7 | 23.5 | 70 | $\begin{array}{r} 79 \\ 107 \end{array}$ | 57 | 45 | M $8 \times 1.25 \times 16$ | 6.5 | $\begin{aligned} & 58 \\ & 86 \end{aligned}$ | $\begin{array}{r} 6.5 \\ 20.5 \end{array}$ | 29 | 11 | M 6×0.75 | 6 | 11 |
| LH30EL <br> LH30GL | 42 | 9 | 31 | 90 | $\begin{gathered} 98.6 \\ 124.6 \end{gathered}$ | 72 | 52 | M 10×1.5×18 | 9 | $\begin{aligned} & 72 \\ & 98 \end{aligned}$ | $\begin{aligned} & 10 \\ & 23 \end{aligned}$ | 33 | 11 | M 6×0.75 | 7 | 11 |
| LH35EL LH35GL | 48 | 9.5 | 33 | 100 | $\begin{aligned} & 109 \\ & 143 \end{aligned}$ | 82 | 62 | M 10×1.5×20 | 9 | $\left.\begin{gathered} 80 \\ 114 \end{gathered} \right\rvert\,$ | $\begin{array}{r} 9 \\ 26 \end{array}$ | 38.5 | 12 | M 6×0.75 | 8 | 11 |
| LH45EL LH45GL | 60 | 14 | 37.5 | 120 | $\begin{aligned} & 139 \\ & 171 \end{aligned}$ | 100 | 80 | M $12 \times 1.75 \times 24$ | 10 | $\left\|\begin{array}{c} 105 \\ 137 \end{array}\right\|$ | $\begin{aligned} & 12.5 \\ & 28.5 \end{aligned}$ | 46 | 13 | PT1/8 | 10 | 13 |
| LH55EL LH55GL | 70 | 15 | 43.5 | 140 | $\begin{aligned} & 163 \\ & 201 \end{aligned}$ | 116 | 95 | M $14 \times 2 \times 28$ | 12 | $\begin{array}{\|l\|} \hline 126 \\ 164 \\ \hline \end{array}$ | $\begin{aligned} & 15.5 \\ & 34.5 \end{aligned}$ | 55 | 15 | PT1/8 | 11 | 13 |
| LH65EL LH65GL | 90 | 16 | 53.5 | 170 | $\begin{aligned} & 193 \\ & 253 \end{aligned}$ | 142 | 110 | M 16×2×24 | 14 | $\begin{aligned} & 147 \\ & 207 \end{aligned}$ | $\begin{aligned} & 18.5 \\ & 48.5 \end{aligned}$ | 74 | 23 | PT1/8 | 19 | 13 |
| LH85GL | 110 | 18 | 65 | 215 | 303 | 185 | 140 | M $20 \times 2.5 \times 30$ | 15 | 243 | 51.5 | 92 | 30 | PT1/8 | 23 | 13 | LH85 is the item on order

 - P3 ultra precision grade


A41

## LH-FL (High load type)

LH-HL (Super high load type)

- Specification number of preloaded assembly
(Custom made assembly)
Model LH3 0840 FL C $\mathbf{2}$ - PN ZO-II $\begin{aligned} & \text { Iin refers to a set of } 2\end{aligned}$

Rail length (mm)
Ball slide shape
Material/surface treatment
(See Page A24)

- C: Standard material
- K: Stainless steel
(only for LH2O-30)


## Preload code <br> - ZO fine clearance <br> - Z1 slight preload

## Accuracy grade

- PN normal grade
- P5 precision grade
- P4 super precision grade
-P3 ultra precision grade

Table. I-53

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{\|c\|} \hline \text { Height } \\ H \\ \hline \end{array}$ | $E$ | $W_{2}$ | Width <br> w | Length$L$ | M ounting hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $Q \times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LH20FL <br> LH2OHL | 30 | 5 | 21.5 | 63 | $\begin{aligned} & 69.8 \\ & 91.8 \end{aligned}$ | 53 | 40 | $6 \times 10$ | 5 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | $\begin{array}{r} 5 \\ 16 \end{array}$ | 25 | 10 | M 6×0.75 | 5 | 11 |
| LH25FL <br> LH25HL | 36 | 7 | 23.5 | 70 | $\begin{array}{r} 79 \\ 107 \end{array}$ | 57 | 45 | $7 \times 10$ | 6.5 | $\begin{aligned} & 58 \\ & 86 \end{aligned}$ | $\begin{array}{r} 6.5 \\ 20.5 \end{array}$ | 29 | 11 | M 6×0.75 | 6 | 11 |
| LH30FL LH30HL | 42 | 9 | 31 | 90 | $\begin{gathered} 98.6 \\ 124.6 \end{gathered}$ | 72 | 52 | $9 \times 12$ | 9 | $\begin{aligned} & 72 \\ & 98 \end{aligned}$ | $\begin{aligned} & 10 \\ & 23 \end{aligned}$ | 33 | 11 | M 6×0.75 | 7 | 11 |
| LH35FL <br> LH35HL | 48 | 9.5 | 33 | 100 | $\begin{aligned} & 109 \\ & 143 \end{aligned}$ | 82 | 62 | $9 \times 13$ | 9 | $\left.\begin{aligned} & 80 \\ & 114 \end{aligned} \right\rvert\,$ | $\begin{array}{r} 9 \\ 26 \end{array}$ | 38.5 | 12 | M 6×0.75 | 8 | 11 |
| LH45FL <br> LH45HL | 60 | 14 | 37.5 | 120 | $\begin{aligned} & 139 \\ & 171 \end{aligned}$ | 100 | 80 | $11 \times 15$ | 10 | $\left\|\begin{array}{l} 105 \\ 137 \end{array}\right\|$ | $\begin{aligned} & 12.5 \\ & 28.5 \end{aligned}$ | 46 | 13 | PT1/8 | 10 | 13 |
| $\begin{aligned} & \text { LH55FL } \\ & \text { LH55HL } \end{aligned}$ | 70 | 15 | 43.5 | 140 | $\begin{aligned} & 163 \\ & 201 \end{aligned}$ | 116 | 95 | $14 \times 18$ | 12 | $\left\|\begin{array}{c} 126 \\ 164 \end{array}\right\|$ | $\begin{aligned} & 15.5 \\ & 34.5 \end{aligned}$ | 55 | 15 | PT1/8 | 11 | 13 |
| LH65FL <br> LH65HL | 90 | 16 | 53.5 | 170 | $\begin{aligned} & 193 \\ & 253 \end{aligned}$ | 142 | 110 | 16×24 | 14 | $\left\|\begin{array}{l} 147 \\ 207 \end{array}\right\|$ | $\begin{aligned} & 18.5 \\ & 48.5 \end{aligned}$ | 74 | 23 | PT1/8 | 19 | 13 |
| LH85HL | 110 | 18 | 65 | 215 | 303 | 185 | 140 | $18 \times 30$ | 15 | 243 | 51.5 | 92 | 30 | PT1/8 | 23 | 13 |

LH85 is the item on order


| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width | Height | Pitch | Mounting |  | G |  | Dynamic | Static |  | tic mom |  |  |  | Rai |
| $W_{1}$ | $H_{1}$ | $F$ | bolt hole $d \times D \times h$ | $B_{3}$ |  |  | $\begin{aligned} & \hline C \\ & (N[k \end{aligned}$ | ${ }_{\text {kgf]) }} C_{0}$ | $\begin{gathered} M_{\mathrm{RO}} \\ (\mathrm{~N} \end{gathered}$ | $\begin{array}{\|c\|} \hline \\ \cdot M_{\mathrm{PO}} \\ \cdot \mathrm{~m}[\mathrm{kgf} . \end{array}$ | $\begin{aligned} & M_{Y 0} \\ & \cdot \mathrm{~m}]) \end{aligned}$ | $D_{\text {w }}$ | slide <br> (kg) | (kg/m) |
| 20 | 18 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{array}{\|l\|} \hline 14200 \\ {[1450]} \\ 18200 \\ {[1860]} \\ \hline \end{array}$ | $\left\|\begin{array}{l}25100 \\ {[2560]} \\ 39500 \\ {[4020]}\end{array}\right\|$ | $\begin{aligned} & 216 \\ & {[22]} \\ & 305 \\ & {[31]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 345 \\ & {[35]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 345 \\ & {[35]} \\ & \hline \end{aligned}$ | 3.968 | $\begin{aligned} & 0.45 \\ & 0.65 \end{aligned}$ | 2.6 |
| 23 | 22 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & \hline 21000 \\ & {[2140]} \\ & 26900 \\ & {[2740]} \end{aligned}$ | 39000 $[4000]$ 52500 $[5340]$ | $\begin{aligned} & \hline 355 \\ & {[36]} \\ & 470 \\ & {[48]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 315 \\ & {[32]} \\ & 530 \\ & {[54]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 305 \\ & {[31]} \\ & 520 \\ & {[53]} \\ & \hline \end{aligned}$ | 4.762 | $\begin{aligned} & 0.63 \\ & 0.93 \end{aligned}$ | 3.6 |
| 28 | 26 | 80 | $9 \times 14 \times 12$ | 14 | 20 | $\begin{gathered} 4000 \\ (3500) \end{gathered}$ | $\begin{aligned} & 29200 \\ & {[2980]} \\ & 37500 \\ & {[3800]} \\ & \hline \end{aligned}$ | 54000 $[5490]$ 71500 $[7310]$ | $\begin{aligned} & 590 \\ & {[60]} \\ & 785 \\ & {[80]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 490 \\ & {[50]} \\ & 845 \\ & {[86]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 480 \\ & {[49]} \\ & 835 \\ & {[85]} \\ & \hline \end{aligned}$ | 5.556 | $6 \begin{aligned} & 1.2 \\ & 1.6 \end{aligned}$ | 5.2 |
| 34 | 29 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 4000 | $\left.\begin{array}{l}39000 \\ {[3960]} \\ 49500 \\ {[5060]}\end{array}\right]$ | 68500 $[7010]$ 97500 $[9930]$ | $\begin{aligned} & \hline 940 \\ & {[96]} \\ & 1330 \\ & {[136]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 735 \\ & {[75]} \\ & 1410 \\ & {[144]} \\ & \hline \end{aligned}$ | 715 $[73]$ 1380 $[141]$ | 6.350 | $0 \left\lvert\, \begin{aligned} & 1.7 \\ & 2.4 \end{aligned}\right.$ | 7.2 |
| 45 | 38 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3990 | $\begin{array}{\|l\|} \hline 66000 \\ {[6740]} \\ 79500 \\ {[8130]} \\ \hline \end{array}$ | $\left[\begin{array}{l} 119000 \\ {[12100]} \\ 146000 \\ {[14900]} \end{array}\right]$ | $\begin{aligned} & 2120 \\ & {[216]} \\ & 2590 \\ & {[264]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1670 \\ & {[170]} \\ & 2460 \\ & {[251]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1650 \\ & {[168]} \\ & 2430 \\ & {[248]} \\ & \hline \end{aligned}$ | 7.937 | $\begin{aligned} & 3 \\ & 3.9 \end{aligned}$ | 12.3 |
| 53 | 44 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3960 | $\begin{array}{l\|} \hline 97500 \\ {[9940]} \\ 118000 \\ {[12000]} \end{array}$ | $\left[\begin{array}{l} 168000 \\ {[17100]} \\ 207000 \\ {[21100]} \end{array}\right.$ | $\begin{array}{\|l\|} \hline 3600 \\ {[367]} \\ 4400 \\ {[449]} \\ \hline \end{array}$ | $\begin{aligned} & \hline 2870 \\ & {[293]} \\ & 4250 \\ & {[435]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2820 \\ & {[288]} \\ & 4150 \\ & {[426]} \\ & \hline \end{aligned}$ | 9.525 | $\begin{aligned} & 5 \\ & 6.5 \end{aligned}$ | 16.9 |
| 63 | 53 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3900 | $\begin{aligned} & 150000 \\ & {[15100]} \\ & 189000 \\ & {[19300]} \end{aligned}$ | $0 \begin{aligned} & 240000 \\ & \hline 24500] \\ & 320000 \\ & {[32700]} \end{aligned}$ | $\begin{array}{\|c\|} \hline 6150 \\ {[629]} \\ 8150 \\ {[834]} \end{array}$ | $\begin{aligned} & \hline 4850 \\ & {[495]} \\ & 8350 \\ & {[850]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4750 \\ & {[484]} \\ & 8150 \\ & {[830]} \\ & \hline \end{aligned}$ | 11.906 | $6 \begin{aligned} & 10 \\ & 14.1 \end{aligned}$ | 24.3 |
| 85 | 65 | 180 | $24 \times 35 \times 28$ | 42.5 | 45 | 2520 | $\left[\begin{array}{l} 279000 \\ {[28500]} \end{array}\right]$ | [494000] | $\begin{aligned} & 17000 \\ & {[1730]} \end{aligned}$ | $\begin{aligned} & 16100 \\ & {[1640]} \end{aligned}$ | $\begin{aligned} & \hline 15700 \\ & {[1600]} \end{aligned}$ | 14.287 | 24.5 | 38.3 |

## Dimensions of LH Series (Interchangeable ball slide)

## LAH-AN (High load type)

## LAH-BN (Super high load type)

- See "A-I -4.2. Reference Number of the Standardized Linear Guide in Stock" in Page A26 for reference number of each interchangeable part.


Table. I -5^4

| Model No. | Assembly |  |  | Width <br> w | Length <br> $L$ |  |  |  |  | Ball | slide |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | W。 |  |  | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  |
| LAH20AN <br> LAH2OBN | 30 | 5 | 12 | 44 | $\begin{aligned} & 69.8 \\ & 91.8 \end{aligned}$ | 32 | $\begin{aligned} & 36 \\ & 50 \end{aligned}$ | M 5 ¢ $0.8 \times 6$ | 6 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | $\begin{array}{r} 7 \\ 11 \end{array}$ | 25 | 12 |
| LAH25AN <br> LAH25BN | 40 | 7 | 12.5 | 48 | $\begin{array}{r} 79 \\ 107 \end{array}$ | 35 | $\begin{aligned} & 35 \\ & 50 \end{aligned}$ | M $6 \times 1 \times 9$ | 6.5 | $\begin{aligned} & 58 \\ & 86 \end{aligned}$ | $\begin{aligned} & 11.5 \\ & 18 \end{aligned}$ | 33 | 12 |
| LAH30AN <br> LAH30BN | 45 | 9 | 16 | 60 | $\begin{array}{r} 85.6 \\ 124.6 \end{array}$ | 40 | $\begin{aligned} & 40 \\ & 60 \end{aligned}$ | M $8 \times 1.25 \times 10$ | 10 | $\begin{aligned} & 59 \\ & 98 \end{aligned}$ | $\begin{aligned} & 9.5 \\ & 19 \end{aligned}$ | 36 | 14 |
| LAH35AN <br> LAH35BN | 55 | 9.5 | 18 | 70 | $\begin{aligned} & 109 \\ & 143 \end{aligned}$ | 50 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{gathered} 80 \\ 114 \end{gathered}$ | $\begin{aligned} & 15 \\ & 21 \end{aligned}$ | 45.5 | 15 |
| LAH45AN <br> LAH45BN | 70 | 14 | 20.5 | 86 | $\begin{aligned} & 139 \\ & 171 \end{aligned}$ | 60 | $\begin{aligned} & 60 \\ & 80 \end{aligned}$ | M $10 \times 1.5 \times 17$ | 13 | $\begin{aligned} & 105 \\ & 137 \end{aligned}$ | $\begin{aligned} & 22.5 \\ & 28.5 \end{aligned}$ | 56 | 17 |
| LAH55AN <br> LAH55BN | 80 | 15 | 23.5 | 100 | $\begin{aligned} & 163 \\ & 201 \end{aligned}$ | 75 | $\begin{aligned} & 75 \\ & 95 \end{aligned}$ | M $12 \times 1.75 \times 18$ | 12.5 | $\begin{aligned} & 126 \\ & 164 \end{aligned}$ | $\begin{aligned} & 25.5 \\ & 34.5 \end{aligned}$ | 65 | 18 |
| LAH65AN <br> LAH65BN | 90 | 16 | 31.5 | 126 | $\begin{aligned} & 193 \\ & 253 \end{aligned}$ | 76 | $\begin{gathered} 70 \\ 120 \end{gathered}$ | M 16x2×20 | 25 | $\begin{aligned} & 147 \\ & 207 \end{aligned}$ | $\begin{aligned} & 38.5 \\ & 48.5 \end{aligned}$ | 74 | 23 |




## LAH-EL (High load type)

## LAH-GL (Super high load type)

- See "A-I -4.2. Reference Number of the Standardized Linear Guide in Stock" in Page A26 for reference number of each interchangeable part.


Table. I -5 5

| Model No. | Assembly |  |  | Width <br> w | Length <br> L |  |  |  |  |  | slide |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W_{2}$ |  |  | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |
| LAH20EL <br> LAH20GL | 30 | 5 | 21.5 | 63 | $\begin{aligned} & 69.8 \\ & 91.8 \end{aligned}$ | 53 | 40 | M $6 \times 1 \times 10$ | 5 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | $\begin{array}{r} 5 \\ 16 \end{array}$ | 25 | 10 |
| LAH25EL <br> LAH25GL | 36 | 7 | 23.5 | 70 | $\begin{array}{r} 79 \\ 107 \end{array}$ | 57 | 45 | M 8×1.25×16 | 6.5 | $\begin{aligned} & 58 \\ & 86 \end{aligned}$ | $\begin{array}{r} 6.5 \\ 20.5 \end{array}$ | 29 | 11 |
| LAH30EL LAH30GL | 42 | 9 | 31 | 90 | $\begin{array}{r} 98.6 \\ 124.6 \end{array}$ | 72 | 52 | M 10×1.5×18 | 9 | $\begin{aligned} & 72 \\ & 98 \end{aligned}$ | $\begin{aligned} & 10 \\ & 23 \end{aligned}$ | 33 | 11 |
| LAH35EL <br> LAH35GL | 48 | 9.5 | 33 | 100 | $\begin{aligned} & 109 \\ & 143 \end{aligned}$ | 82 | 62 | M 10×1.5×20 | 9 | $\begin{gathered} 80 \\ 114 \end{gathered}$ | $\begin{array}{r} 9 \\ 26 \end{array}$ | 38.5 | 12 |
| LAH45EL LAH45GL | 60 | 14 | 37.5 | 120 | $\begin{aligned} & 139 \\ & 171 \end{aligned}$ | 100 | 80 | M $12 \times 1.75 \times 24$ | 10 | $\begin{aligned} & 105 \\ & 137 \end{aligned}$ | $\begin{aligned} & 12.5 \\ & 28.5 \end{aligned}$ | 46 | 13 |
| LAH55EL LAH55GL | 70 | 15 | 43.5 | 140 | $\begin{aligned} & 163 \\ & 201 \end{aligned}$ | 116 | 95 | M $14 \times 2 \times 28$ | 12 | $\begin{aligned} & 126 \\ & 164 \end{aligned}$ | $\begin{aligned} & 15.5 \\ & 34.5 \end{aligned}$ | 55 | 15 |
| LAH65EL LAH65GL | 90 | 16 | 53.5 | 170 | $\begin{aligned} & 193 \\ & 253 \end{aligned}$ | 142 | 110 | M 16×2×24 | 14 | $\begin{aligned} & 147 \\ & 207 \end{aligned}$ | $\begin{aligned} & 18.5 \\ & 48.5 \end{aligned}$ | 74 | 23 |



GL type


## LAH-FL (High load type)

## LAH-HL (Super high load type)

- See "A-I -4.2. Reference Number of the Standardized Linear Guide in Stock" in Page A26 for reference number of each interchangeable part


Table. I-56

| Model No. | Assembly |  |  | Width Length <br> $W$ $L$ |  | Mounting hole |  |  | Ball slide |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height$H$ | $E$ | $W_{2}$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  | B | $J$ | $Q \times \ell$ | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ |
| LAH20FL <br> LAH20HL | 30 | 5 | 21.5 | 63 | $\begin{aligned} & 69.8 \\ & 91.8 \end{aligned}$ |  |  |  | 53 | 40 | $6 \times 10$ | 5 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | $\begin{array}{r} 5 \\ 16 \end{array}$ | 25 | 10 |
| LAH25FL LAH25HL | 36 | 7 | 23.5 | 70 | $\begin{array}{r} 79 \\ 107 \end{array}$ | 57 | 45 | $7 \times 10$ | 6.5 | $\begin{aligned} & 58 \\ & 86 \end{aligned}$ | $\begin{array}{r} 6.5 \\ 20.5 \end{array}$ | 29 | 11 |
| LAH30FL LAH3OHL | 42 | 9 | 31 | 90 | $\begin{array}{r} 98.6 \\ 124.6 \end{array}$ | 72 | 52 | $9 \times 12$ | 9 | $\begin{aligned} & 72 \\ & 98 \end{aligned}$ | $\begin{aligned} & 10 \\ & 23 \end{aligned}$ | 33 | 11 |
| LAH35FL LAH35HL | 48 | 9.5 | 33 | 100 | $\begin{aligned} & 109 \\ & 143 \end{aligned}$ | 82 | 62 | $9 \times 13$ | 9 | $\begin{gathered} 80 \\ 114 \end{gathered}$ | $\begin{array}{r} 9 \\ 26 \end{array}$ | 38.5 | 12 |
| LAH45FL LAH45HL | 60 | 14 | 37.5 | 120 | $\begin{aligned} & 139 \\ & 171 \end{aligned}$ | 100 | 80 | $11 \times 15$ | 10 | $\begin{aligned} & 105 \\ & 137 \end{aligned}$ | $\begin{aligned} & 12.5 \\ & 28.5 \end{aligned}$ | 46 | 13 |
| LAH55FL LAH55HL | 70 | 15 | 43.5 | 140 | $\begin{aligned} & 163 \\ & 201 \end{aligned}$ | 116 | 95 | $14 \times 18$ | 12 | $\begin{aligned} & 126 \\ & 164 \end{aligned}$ | $\begin{aligned} & 15.5 \\ & 34.5 \end{aligned}$ | 55 | 15 |
| LAH65FL LAH65HL | 90 | 16 | 53.5 | 170 | $\begin{aligned} & 193 \\ & 253 \end{aligned}$ | 142 | 110 | $16 \times 24$ | 14 | $\begin{aligned} & 147 \\ & 207 \end{aligned}$ | $\begin{aligned} & 18.5 \\ & 48.5 \end{aligned}$ | 74 | 23 |




|  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grease fitting |  |  | Dynamic | Static | Static moment |  |  |  | Ball slide |
| Hole size | $T_{1}$ | $N$ | ( $\mathrm{N}[\mathrm{kgf}]$ ) |  |  | $\begin{gathered} M_{\mathrm{Po}} \\ \mathrm{~m}[\mathrm{kgff} . \end{gathered}$ | $M_{y o}$ | $D_{\text {w }}$ | (kg) |
| M 6×0.75 | 5 | 11 | $\begin{aligned} & \hline 14200 \\ & {[1450]} \\ & 18200 \\ & {[1860]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 25100 \\ & {[2560]} \\ & 39500 \\ & {[4020]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 216 \\ & {[22]} \\ & 305 \\ & {[31]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 345 \\ & {[35]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 177 \\ & {[18]} \\ & 345 \\ & {[35]} \\ & \hline \end{aligned}$ | 3.968 | $\begin{aligned} & 0.45 \\ & 0.65 \end{aligned}$ |
| M 6×0.75 | 6 | 11 | $\begin{aligned} & \hline 21000 \\ & {[2140]} \\ & 26900 \\ & {[2740]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 39000 \\ & {[4000]} \\ & 52500 \\ & {[5340]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 355 \\ & {[36]} \\ & 470 \\ & {[48]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 315 \\ & {[32]} \\ & 530 \\ & {[54]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 305 \\ & {[31]} \\ & 520 \\ & {[53]} \\ & \hline \end{aligned}$ | 4.762 | $\begin{aligned} & 0.63 \\ & 0.93 \end{aligned}$ |
| M 6×0.75 | 7 | 11 | $\begin{aligned} & 29200 \\ & {[2980]} \\ & 37500 \\ & {[3800]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 54000 \\ & {[5490]} \\ & 71500 \\ & {[7310]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 590 \\ & {[60]} \\ & 785 \\ & {[80]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 490 \\ & {[50]} \\ & 845 \\ & {[86]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 480 \\ & {[49]} \\ & 835 \\ & {[85]} \\ & \hline \end{aligned}$ | 5.556 | $\begin{aligned} & 1.2 \\ & 1.6 \end{aligned}$ |
| M 6×0.75 | 8 | 11 | $\begin{aligned} & \hline 39000 \\ & {[3960]} \\ & 49500 \\ & {[5060]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 68500 \\ & {[7010]} \\ & 97500 \\ & {[9930]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 940 \\ & {[96]} \\ & 1330 \\ & {[136]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 735 \\ & {[75]} \\ & 1410 \\ & {[144]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 715 \\ & {[73]} \\ & 1380 \\ & {[141]} \\ & \hline \end{aligned}$ | 6.350 | $\begin{aligned} & 1.7 \\ & 2.4 \end{aligned}$ |
| PT1/8 | 10 | 13 | $\begin{aligned} & \hline 66000 \\ & {[6740]} \\ & 79500 \\ & {[8130]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 119000 \\ & {[12100]} \\ & 146000 \\ & {[14900]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 2120 \\ & {[216]} \\ & 2590 \\ & {[264]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1670 \\ & {[170]} \\ & 2460 \\ & {[251]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1650 \\ & {[168]} \\ & 2430 \\ & {[248]} \end{aligned}$ | 7.937 | $\begin{aligned} & 3 \\ & 3.9 \end{aligned}$ |
| PT1/8 | 11 | 13 | $\begin{aligned} & \hline 97500 \\ & {[9940]} \\ & 118000 \\ & {[12000]} \end{aligned}$ | $\begin{aligned} & 168000 \\ & {[17100]} \\ & 207000 \\ & {[21100]} \end{aligned}$ | $\begin{aligned} & 3600 \\ & {[367]} \\ & 4400 \\ & {[449]} \end{aligned}$ | $\begin{aligned} & 2870 \\ & {[293]} \\ & 4250 \\ & {[435]} \end{aligned}$ | $\begin{aligned} & 2820 \\ & {[288]} \\ & 4150 \\ & {[426]} \end{aligned}$ | 9.525 | $\begin{aligned} & 5 \\ & 6.5 \end{aligned}$ |
| PT1/8 | 19 | 13 | $\begin{aligned} & 150000 \\ & {[15100]} \\ & 189000 \\ & {[19300]} \end{aligned}$ | $\begin{aligned} & 240000 \\ & {[24500]} \\ & 320000 \\ & {[32700]} \end{aligned}$ | $\begin{aligned} & 6150 \\ & {[629]} \\ & 8150 \\ & {[834]} \end{aligned}$ | $\begin{aligned} & 4850 \\ & {[495]} \\ & 8350 \\ & {[850]} \end{aligned}$ | $\begin{aligned} & \hline 4750 \\ & {[484]} \\ & 8150 \\ & {[830]} \end{aligned}$ | 11.906 | $\begin{aligned} & 10 \\ & 14.1 \end{aligned}$ |

## LH Series (Interchangeable part)

## Dimensions of LH Series (Interchangeable rail)

## Dimensions of LH Series (Interchangeable rail) <br> Regular rails <br> Butting rails <br> L1H (Fine clearance ) LIH-01 (Fine clearance) L1H-Z (Slight preload) L1H-01Z (Slight preload)

- See " A-I -4•2 Reference Number of the Standardized Linear Guide in Stock" on Page A26 for reference number of each interchangeable part.


Table I-5•7
Unit: mm

| Model No. | Rail |  |  |  |  |  |  | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Width <br> $W_{1}$ | Height <br> $H_{1}$ | Pitch <br> $F$ | Mounting bolt hole <br> $d \times D \times h$ | $B_{3}$ | $G$ <br> Recommended | Max. length <br> $L_{\text {omax }}$ | Rail <br> $(\mathrm{Kg} / \mathrm{m})$ |
| L1H20 | 20 | 18 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | 3960 | 2.6 |
| L1H25 | 23 | 22 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | 3960 | 3.6 |
| L1H30 | 28 | 26 | 80 | $9 \times 14 \times 12$ | 14 | 20 | 4000 | 5.2 |
| L1H35 | 34 | 29 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 4000 | 7.2 |
| L1H45 | 45 | 38 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3990 | 12.3 |
| L1H55 | 53 | 44 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3960 | 16.9 |
| L1H65 | 63 | 53 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3900 | 24.3 |

G dimension is $1 / 2 F^{0.5}$ for butting rail.

## A-I-5.2 LS Series



## (1) High self aligning capability (rolling direction)

Same as the DF combination in angular contact bearings, self-aligning capability is high because the cross point of the contact lines of balls and grooves comes inside, reducing moment rigidity. This increases the capacity to absorb the error of installation.

## (2) High load carrying capacity to vertical direction

The contact angle is set at 50 degrees, increasing load carrying capacity as well as rigidity against the load in vertical direction.

## (3) High resistance against shock load

The bottom ball groove is formed in gothic-arch and the center of the top and bottom grooves are offset as shown in Fig. I-5॰6. The vertical load is usually carried by top 2 rows at where balls are contacting at two points. Because of this design, the bottom rows will carry the load when a large impact load is applied as shown in Fig. I-5•7. This assures high resistance to the shock load.

## (4) Highly accurate

As shown in Fig. I-5•8, fixing the measuring rollers is simple thanks to the gothic-arch groove. This makes easy and accurate measuring of ball- grooves.

## (5) Interchangeable rail and ball slide (short delivery time)

Randomly matching rails and ball slides are stocked as standardized interchangeable items. This reduces delivery time.

## (6) Easy to handle, and designed with safety in mind.

Balls are retained in the retainer and do not fall out when the ball slide is withdrawn from the rail.

## (7) Abundant models and sizes come in series.

Each series have several ball slide models, rendering the linear guide available for numerous uses. The LS Series also has standardized long stainless- steel rail (maximum: 3500 mm ).


Fig. I-5٪ LS Series


Fig. I-5®6 Enlarged illustration: Offset gothicarch


Fig. I-5•7 When load is applied


Fig. I-5\&8 Rail-grinding and measuring

## Dimensions of LS Series (Preloaded assembly)

## LS-CL (Medium load type) <br> LS-AL (High load type)

- Specification number of preloaded assembly
(Custom made assembly)
LH35 0840 AL C $2-\mathrm{PN}$ ZO-II II refers to a set of 2
Model

Rail length (mm
Ball slide shape

Material/surface treatment (See Page A24)

- C: Standard material
- K: Stainless steel

Number of ball slides per rail

```
Accuracy grade
    - PN normal grade
    - P6 precision grade 
    - P4 super precision grade
    - P3 ultra precision grade
```

Table. I-58

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width <br> w | Length <br> $L$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LS15CL <br> LS15AL | 24 | 4.6 | 9.5 | 34 | $\begin{aligned} & 40.4 \\ & 56.8 \end{aligned}$ | 26 | $\begin{aligned} & - \\ & 26 \end{aligned}$ | M 4×0.7×6 | 4 | $\begin{array}{\|l\|} 23.6 \\ 40 \end{array}$ | $\begin{array}{\|c} 11.8 \\ 7 \end{array}$ | 19.4 | 10 | ¢ 3 | 6 | 3 |
| LS20CL <br> LS20AL | 28 | 6 | 11 | 42 | $\begin{aligned} & 47.2 \\ & 65.2 \end{aligned}$ | 32 | $\begin{aligned} & - \\ & 32 \end{aligned}$ | M 5 x 0.8×7 | 5 | $\begin{aligned} & 30 \\ & 48 \end{aligned}$ | $\begin{gathered} 15 \\ 8 \end{gathered}$ | 22 | 12 | M 6×0.75 | 5.5 | 11 |
| $\begin{aligned} & \text { LS25CL } \\ & \text { LS25AL } \end{aligned}$ | 33 | 7 | 12.5 | 48 | $\begin{aligned} & 59.6 \\ & 81.6 \end{aligned}$ | 35 | $35$ | M $6 \times 1 \times 9$ | 6.5 | $\begin{aligned} & 38 \\ & 60 \end{aligned}$ | $\begin{aligned} & 19 \\ & 12.5 \end{aligned}$ | 26 | 12 | M 6×0.75 | 7 | 11 |
| $\begin{aligned} & \text { LS30CL } \\ & \text { LS30AL } \end{aligned}$ | 42 | 9 | 16 | 60 | $\begin{aligned} & 67.4 \\ & 96.4 \end{aligned}$ | 40 | $\begin{aligned} & - \\ & 40 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{aligned} & 42 \\ & 71 \end{aligned}$ | $\begin{array}{\|l} 21 \\ 15.5 \end{array}$ | 33 | 13 | M 6×0.75 | 8 | 11 |
| $\begin{aligned} & \text { LS35CL } \\ & \text { LS35AL } \end{aligned}$ | 48 | 10.5 | 18 | 70 | $\begin{gathered} 77 \\ 108 \end{gathered}$ | 50 | $\begin{aligned} & - \\ & 50 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{aligned} & 49 \\ & 80 \end{aligned}$ | $\begin{aligned} & 24.5 \\ & 15 \end{aligned}$ | 37.5 | 14 | M 6×0.75 | 8.5 | 11 |

*Either M3 (3.5x6x4.5) or M4 (4.5×7.5×5.3) is available for mounting LS15 rail. "T" is added to the end of length code in the reference number of interchangeable rail with M4 mounting hole.


AL type


| Unit: mm |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| Width | Height | Pitch | Mounting bolt hole$d \times D \times h$ | $B_{3}$ | G <br> (recomm ended) | Maxlength () for | Dynamic | Static | Static moment |  |  | $D_{\text {w }}$ | Ball slide (kg) | $\begin{aligned} & \hline \text { Rail } \\ & (\mathrm{kg} / \mathrm{m}) \\ & \hline \end{aligned}$ |
| $W_{1}$ | $\mathrm{H}_{1}$ |  |  |  |  |  | C <br> ( $\mathrm{N}[\mathrm{k} \mathrm{g}$ | ${ }_{\text {kgf]) }} C_{0}$ | $\begin{aligned} & M_{\text {RO }} \\ & (N) \end{aligned}$ | $\begin{gathered} M_{\mathrm{Po}} \\ \mathrm{~m}[\mathrm{kgf} \end{gathered}$ | $\begin{gathered} M_{\mathrm{Yo}} \\ \mathrm{~m}]) \end{gathered}$ |  |  |  |
| 15 | 12.5 | 60 | $\begin{gathered} * \\ 3.5 \times 6 \times 4.5 \\ 4.5 \times 7.5 \times 5.3 \end{gathered}$ | 7.5 | 20 | $\left.\begin{gathered} 2000 \\ (1700) \end{gathered} \right\rvert\,$ | $\begin{aligned} & 4550 \\ & {[465]} \\ & 6700 \\ & {[685]} \end{aligned}$ | $\begin{array}{\|c\|} \hline 8300 \\ {[845]} \\ 12500 \\ {[1270]} \end{array}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 69 \\ & {[7]} \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \end{aligned}$ | 2.778 | $\begin{aligned} & 0.14 \\ & 0.20 \end{aligned}$ | 1.4 |
| 20 | 15.5 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | $\left\|\begin{array}{c} 3960 \\ (3500) \end{array}\right\|$ | $\begin{aligned} & \hline 6550 \\ & {[670]} \\ & 8900 \\ & {[910]} \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 12200 \\ {[1240]} \\ 17500 \\ {[1780]} \end{array}$ | 88 $[9]$ 127 $[13]$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | 3.175 | $\begin{aligned} & 0.19 \\ & 0.28 \end{aligned}$ | 2.3 |
| 23 | 18 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | $\left.\begin{gathered} 3960 \\ (3500) \end{gathered} \right\rvert\,$ | 10600 $[1080]$ 14400 $[1470]$ | $\begin{array}{\|l\|} \hline 18600 \\ {[1900]} \\ 29100 \\ {[2970]} \end{array}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 245 \\ & {[25]} \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & 206 \\ & {[21]} \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & 196 \\ & {[20]} \end{aligned}$ | 3.968 | $\begin{array}{\|l} 0.34 \\ 0.51 \end{array}$ | 3.1 |
| 28 | 23 | 80 | $7 \times 11 \times 9$ | 14 | 20 | $\left\|\begin{array}{c} 4000 \\ (3500) \end{array}\right\|$ | 15900 $[1620]$ 23400 $[2390]$ | 26500 $[2700]$ 43000 $[4400]$ | $\begin{aligned} & \hline 245 \\ & {[25]} \\ & 470 \\ & {[48]} \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | 4.762 | $\begin{array}{\|l\|} 0.58 \\ 0.85 \end{array}$ | 4.8 |
| 34 | 27.5 | 80 | $9 \times 14 \times 12$ | 17 | 20 | $\left\|\begin{array}{c} 4000 \\ (3500) \end{array}\right\|$ | 22100 $[2250]$ 32500 $[3320]$ | 36000 $[3650]$ 58500 $[5940]$ | $\begin{aligned} & \hline 410 \\ & {[42]} \\ & 775 \\ & {[79]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 560 \\ & {[57]} \end{aligned}$ | 5.556 | $\begin{array}{\|l\|} 0.86 \\ 1.3 \end{array}$ | 7.0 |

## LS-EL (High load type)

- Specification number of preloaded assembly
(Custom made assembly)
LH35 0840 EL C 2 -PN ZO-II II refers to a set of 2

Model
number
Rail length ( mm )
Ball slide shape

Material/surface treatment (See Page A24)
-C: Standard materia

- K: Stainless steel

Number of ball slides per rail


> Accuracy grade •PN normal grade •P6 precision grade •P5 high precision grade •P4 super precision grade •P3 ultra precision grade

Table. I -5^9

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | $\begin{gathered} \hline \text { Width } \\ w \\ \hline \end{gathered}$ |  | M ounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| $\begin{gathered} \text { LS15J L } \\ \text { LS15EL } \end{gathered}$ | 24 | 4.6 | 18.5 | 52 | $\begin{aligned} & 40.4 \\ & 56.8 \end{aligned}$ | 41 | $26$ | M $5 \times 0.8 \times 8$ | 5.5 | $\begin{array}{\|l\|} 23.6 \\ 40 \end{array}$ | $\begin{gathered} 11.8 \\ 7 \end{gathered}$ | 19.4 | 8 | ¢ 3 | 6 | 3 |
| $\begin{gathered} \text { LS20J L } \\ \text { LS20EL } \end{gathered}$ | 28 | 6 | 19.5 | 59 | $\begin{aligned} & 47.2 \\ & 65.2 \end{aligned}$ | 49 | $32$ | M $6 \times 1 \times 10$ | 5 | $\begin{aligned} & 30 \\ & 48 \end{aligned}$ | $\begin{array}{r} 15 \\ 8 \end{array}$ | 22 | 10 | M 6×0.75 | 5.5 | 11 |
| $\begin{gathered} \text { LS25J L } \\ \text { LS25EL } \end{gathered}$ | 33 | 7 | 25 | 73 | $\begin{aligned} & 59.6 \\ & 81.6 \end{aligned}$ | 60 | $35$ | M $8 \times 1.25 \times 12$ | 6.5 | $\begin{aligned} & 38 \\ & 60 \end{aligned}$ | $\left\|\begin{array}{l} 19 \\ 12.5 \end{array}\right\|$ | 26 | 11 | M 6×0.75 | 7 | 11 |
| $\begin{aligned} & \text { LS30J L } \\ & \text { LS30EL } \end{aligned}$ | 42 | 9 | 31 | 90 | $\begin{aligned} & 67.4 \\ & 96.4 \end{aligned}$ | 72 | $\begin{aligned} & - \\ & 40 \end{aligned}$ | M 10×1.5×18 | 9 | $\begin{aligned} & 42 \\ & 71 \end{aligned}$ | $\left\|\begin{array}{l} 21 \\ 15.5 \end{array}\right\|$ | 33 | 11 | M 6×0.75 | 8 | 11 |
| $\begin{aligned} & \text { LS35J L } \\ & \text { LS35EL } \end{aligned}$ | 48 | 10.5 | 33 | 100 | $\begin{gathered} 77 \\ 108 \end{gathered}$ | 82 | $50$ | M 10×1.5×20 | 9 | $\begin{aligned} & 49 \\ & 80 \end{aligned}$ | $\left\lvert\, \begin{aligned} & 24.5 \\ & 15 \end{aligned}\right.$ | 37.5 | 12 | M 6×0.75 | 8.5 | 11 |

*Either M3 (3.5x6x4.5) or M4 (4.5×7.5×5.3) is available for mounting LS15 rail. "T" is added to the end of length code in the reference number of interchangeable rail with M4 mounting hole


| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width <br> $W_{1}$ | Height <br> $\mathrm{H}_{1}$ | Pitch <br> F | Mounting bolt hole $d \times D \times h$ | $B_{3}$ | G <br> recom <br> endea) | Max <br> ( ) for | Dynamic Static <br> $C$ $C_{0}$ <br> $(\mathrm{~N}[\mathrm{kgf}])$  |  | Static moment |  |  | $D_{\text {w }}$ | Ball slide (kg) | $\begin{aligned} & \hline \text { Rail } \\ & (\mathrm{kg} / \mathrm{m}) \\ & \hline \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  | $\begin{gathered} M_{\mathrm{PO}} \\ \mathrm{~m}[\mathrm{kgf} \end{gathered}$ | $M_{\mathrm{ro}}$ <br> m] |  |  |  |
| 15 | 12.5 | 60 | $\begin{array}{\|c\|} \hline * \\ 3.5 \times 6 \times 4.5 \\ 4.5 \times 7.5 \times 5.3 \end{array}$ | 7.5 | 20 | $\begin{gathered} 2000 \\ (1700) \end{gathered}$ | $\begin{aligned} & 4550 \\ & {[465]} \\ & 6700 \\ & {[685]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 8300 \\ {[845]} \\ 12500 \\ {[1270]} \\ \hline \end{array}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 69 \\ & {[7]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 20 \\ & {[2]} \\ & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \end{aligned}$ | 2.778 | $\begin{array}{l\|l} 0.17 \\ 0.26 \end{array}$ | 1.4 |
| 20 | 15.5 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & \hline 6550 \\ & {[670]} \\ & 8900 \\ & {[910]} \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 12200 \\ {[1240]} \\ 17500 \\ {[1780]} \\ \hline \end{array}$ | $\begin{aligned} & \hline 88 \\ & {[9]} \\ & 127 \\ & {[13]} \end{aligned}$ | $\begin{aligned} & \hline 39 \\ & {[4]} \\ & 88 \\ & {[9]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | 3.175 | $\begin{array}{\|l\|l} 0.24 \\ 0.35 \end{array}$ | 2.3 |
| 23 | 18 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & 10600 \\ & {[1080]} \\ & 14400 \\ & {[1470]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 18600 \\ {[1900]} \\ 29100 \\ {[2970]} \\ \hline \end{array}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 245 \\ & {[25]} \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & 206 \\ & {[21]} \\ & \hline \end{aligned}$ | $\begin{gathered} 69 \\ {[7]} \\ 196 \\ {[20]} \\ \hline \end{gathered}$ | 3.968 | $\begin{array}{\|l\|l} 0.44 \\ 0.66 \end{array}$ | 3.1 |
| 28 | 23 | 80 | $7 \times 11 \times 9$ | 14 | 20 | $\begin{gathered} 4000 \\ (3500) \end{gathered}$ | $\begin{array}{\|l\|} \hline 15900 \\ {[1620]} \\ 23400 \\ {[2390]} \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 26500 \\ {[2700]} \\ 43000 \\ {[4400]} \\ \hline \end{array}$ | $\begin{aligned} & \hline 245 \\ & {[25]} \\ & 470 \\ & {[48]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 108 \\ & {[11]} \\ & 355 \\ & {[36]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 108 \\ & {[11]} \\ & 355 \\ & {[36]} \\ & \hline \end{aligned}$ | 4.762 | $\begin{array}{\|l\|l} 0.76 \\ 1.2 \end{array}$ | 4.8 |
| 34 | 27.5 | 80 | $9 \times 14 \times 12$ | 17 | 20 | $\begin{gathered} 4000 \\ (3500) \end{gathered}$ | $\left\|\begin{array}{l} 22100 \\ {[2250]} \\ 32500 \\ {[3320]} \end{array}\right\|$ | $\left.\begin{array}{\|l\|} \hline 36000 \\ {[3650]} \\ 58500 \\ {[5940]} \end{array} \right\rvert\,$ | $\begin{aligned} & \hline 410 \\ & {[42]} \\ & 775 \\ & {[79]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 560 \\ & {[57]} \end{aligned}$ | 5.556 | $\begin{aligned} & 1.2 \\ & 1.7 \end{aligned}$ | 7.0 |

## LS-KL (Medium load type) <br> LS-FL (High load type)

- Specification number of preloaded assembly
(Custom made assembly)
LH35 0840 FL C 2-PN ZO-II II refers to a set of 2

Model
Rail length (mm
Ball slide shape

Material/surface treatment (See Page A24)
C. Standard material

- K: Stainless steel

Number of ball slides per rail


Accuracy grade

- PN normal grade
- P6 precision grade
- P4 super precision grade - P3 ultra precision grade

Table. I-510

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{\|c\|} \hline \text { Height } \\ H \end{array}$ | E | $W_{2}$ | Width <br> w | Length <br> $L$ | Mounting hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $Q \times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| $\begin{aligned} & \text { LS15KL } \\ & \text { LS15FL } \end{aligned}$ | 24 | 4.6 | 18.5 | 52 | $\begin{aligned} & 40.4 \\ & 56.8 \end{aligned}$ | 41 | $\begin{aligned} & - \\ & 26 \end{aligned}$ | $4.5 \times 7$ | 5.5 | $\begin{array}{\|l\|} 23.6 \\ 40 \end{array}$ | $\begin{gathered} 11.8 \\ 7 \end{gathered}$ | 19.4 | 8 | ¢ 3 | 6 | 3 |
| LS20KL <br> LS20FL | 28 | 6 | 19.5 | 59 | $\begin{aligned} & 47.2 \\ & 65.2 \end{aligned}$ | 49 | $\begin{aligned} & - \\ & 32 \end{aligned}$ | $5.5 \times 9$ | 5 | $\begin{array}{\|l} 30 \\ 48 \end{array}$ | $\begin{array}{r} 15 \\ 8 \end{array}$ | 22 | 10 | M 6×0.75 | 5.5 | 11 |
| LS25KL <br> LS25FL | 33 | 7 | 25 | 73 | $\begin{aligned} & 59.6 \\ & 81.6 \end{aligned}$ | 60 | $\begin{aligned} & - \\ & 35 \end{aligned}$ | $7 \times 10$ | 6.5 | $\begin{aligned} & 38 \\ & 60 \end{aligned}$ | $\begin{array}{\|l\|} \hline 19 \\ 12.5 \end{array}$ | 26 | 11 | M 6×0.75 | 7 | 11 |
| LS30KL <br> LS30FL | 42 | 9 | 31 | 90 | $\begin{aligned} & 67.4 \\ & 96.4 \end{aligned}$ | 72 | $\begin{aligned} & - \\ & 40 \end{aligned}$ | $9 \times 12$ | 9 | $\begin{aligned} & 42 \\ & 71 \end{aligned}$ | $\left\|\begin{array}{l} 21 \\ 15.5 \end{array}\right\|$ | 33 | 11 | M 6×0.75 | 8 | 11 |
| $\begin{aligned} & \text { LS35KL } \\ & \text { LS35FL } \end{aligned}$ | 48 | 10.5 | 33 |  | $\begin{gathered} 77 \\ 108 \end{gathered}$ | 82 | $\begin{aligned} & - \\ & 50 \end{aligned}$ | $9 \times 13$ | 9 | $\begin{aligned} & 49 \\ & 80 \end{aligned}$ | $\begin{aligned} & 24.5 \\ & 15 \end{aligned}$ | 37.5 | 12 | M 6×0.75 | 8.5 | 11 |

*Either M3 (3.5x6x4.5) or M4 (4.5×7.5×5.3) is available for mounting LS15 rail. "T" is added to the end of length code in the reference number of interchangeable rail with M4 mounting hole.

KL type


| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width <br> $W_{1}$ | Height <br> $H_{1}$ | Pitch <br> F | Mounting bolt hole $d \times D \times h$ | $B_{3}$ |  | Max. length $L_{\text {omax }}$ stanless | Dynamic Static <br> $C$ $C_{0}$ <br> $(\mathrm{~N}[\mathrm{kgf]})$  |  | Static moment |  |  | $D_{w}$ | Ball slide (kg) | Rail <br> (kg/m) |
|  |  |  |  |  |  |  |  |  |  | $\begin{gathered} M_{\mathrm{Po}} \\ \mathrm{~m}[\mathrm{kgf} \end{gathered}$ | $M_{\mathrm{Yo}}$ <br> m] |  |  |  |
| 15 | 12.5 | 60 | $\begin{array}{\|c\|} * \\ 3.5 \times 6 \times 4.5 \\ 4.5 \times 7.5 \times 5.3 \end{array}$ | 7.5 | 20 | $\begin{array}{\|c\|} \hline 2000 \\ (1700) \end{array}$ | $\begin{aligned} & 4550 \\ & {[465]} \\ & 6700 \\ & {[685]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 8300 \\ {[845]} \\ 12500 \\ {[1270]} \end{array}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 69 \\ & {[7]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | 2.778 | $\begin{array}{\|l\|l} 0.17 \\ 0.26 \end{array}$ | 1.4 |
| 20 | 15.5 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & \hline 6550 \\ & {[670]} \\ & 8900 \\ & {[910]} \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 12200 \\ {[1240]} \\ 17500 \\ {[1780]} \\ \hline \end{array}$ | $\begin{gathered} \hline 88 \\ {[9]} \\ 127 \\ {[13]} \end{gathered}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | 3.175 | $\begin{array}{\|l\|l} 0.24 \\ 0.35 \\ \hline \end{array}$ | 2.3 |
| 23 | 18 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | $\begin{gathered} 3960 \\ (3500) \end{gathered}$ | $\begin{aligned} & 10600 \\ & {[1080]} \\ & 14400 \\ & {[1470]} \end{aligned}$ | 18600 $[1900]$ 29100 $[2970]$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 245 \\ & {[25]} \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & 206 \\ & {[21]} \end{aligned}$ | $\begin{gathered} 69 \\ {[7]} \\ 196 \\ {[20]} \end{gathered}$ | 3.968 | $\begin{array}{\|l\|l} 0.44 \\ 0.66 \end{array}$ | 3.1 |
| 28 | 23 | 80 | $7 \times 11 \times 9$ | 14 | 20 | $\begin{gathered} 4000 \\ (3500) \end{gathered}$ | $\begin{array}{\|l\|} \hline 15900 \\ {[1620]} \\ 23400 \\ {[2390]} \end{array}$ | $\begin{array}{\|l\|} \hline 26500 \\ {[2700]} \\ 43000 \\ {[4400]} \\ \hline \end{array}$ | $\begin{aligned} & \hline 245 \\ & {[25]} \\ & 470 \\ & {[48]} \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | $\begin{aligned} & \hline 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | 4.762 | $\begin{array}{\|l\|l} 0.76 \\ 1.2 \end{array}$ | 4.8 |
| 34 | 27.5 | 80 | $9 \times 14 \times 12$ | 17 | 20 | $\begin{gathered} 4000 \\ (3500) \end{gathered}$ | $\left\|\begin{array}{l} 22100 \\ {[2250]} \\ 32500 \\ {[3320]} \end{array}\right\|$ | $\left.\begin{array}{\|l\|} \hline 36000 \\ {[3650]} \\ 58500 \\ {[5940]} \end{array} \right\rvert\,$ | $\begin{aligned} & \hline 410 \\ & {[42]} \\ & 775 \\ & {[79]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 560 \\ & {[57]} \end{aligned}$ | 5.556 | $\begin{array}{\|l} 1.2 \\ 1.7 \end{array}$ | 7.0 |

## Dimensions of LS Series (Interchangeable ball slide)

## LAS-CL (Medium load type)

## LAS-AL (High load type)

- See "Table I-4*6 Standardized LS series in stock" on Page A30 for reference number of each interchangeable ball slide.

Table. I-5•11

| M odel No. | Assembly |  |  | Width <br> w | Length <br> L |  |  |  |  | Ball | slide |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W$ 。 |  |  | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  |
| LAS15CL <br> LAS15AL | 24 | 4.6 | 9.5 | 34 | $\begin{aligned} & 40.4 \\ & 56.8 \end{aligned}$ | 26 | $\begin{aligned} & - \\ & 26 \end{aligned}$ | M 4×0.7×6 | 4 | $\begin{aligned} & 23.6 \\ & 40 \end{aligned}$ | $\begin{gathered} 11.8 \\ 7 \end{gathered}$ | 19.4 | 10 |
| LAS20CL <br> LAS20AL | 28 | 6 | 11 | 42 | $\begin{aligned} & 47.2 \\ & 65.2 \end{aligned}$ | 32 | $\begin{aligned} & - \\ & 32 \end{aligned}$ | M 5 x $0.8 \times 7$ | 5 | $\begin{aligned} & 30 \\ & 48 \end{aligned}$ | $\begin{array}{r} 15 \\ 8 \end{array}$ | 22 | 12 |
| LAS25CL <br> LAS25AL | 33 | 7 | 12.5 | 48 | $\begin{aligned} & 59.6 \\ & 81.6 \end{aligned}$ | 35 | $35$ | M $6 \times 1 \times 9$ | 6.5 | $\begin{aligned} & 38 \\ & 60 \end{aligned}$ | 19 $12.5$ | 26 | 12 |
| LAS30CL <br> LAS30AL | 42 | 9 | 16 | 60 | $\begin{aligned} & 67.4 \\ & 96.4 \end{aligned}$ | 40 | $\begin{aligned} & - \\ & 40 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{aligned} & 42 \\ & 71 \end{aligned}$ | 21 15.5 | 33 | 13 |
| LAS35CL <br> LAS35AL | 48 | 10.5 | 18 | 70 | $\begin{array}{r} 77 \\ 108 \end{array}$ | 50 | $\begin{aligned} & - \\ & 50 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{aligned} & 49 \\ & 80 \end{aligned}$ | $24.5$ <br> 15 | 37.5 | 14 |




| Grease fitting |  |  | Unit: mm |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |
|  |  |  | Dynamic | Static | Static moment |  |  | D | Ball slide <br> (kg) |
| Hole size | $T_{1}$ | $N$ |  | $C_{0}$ | $M_{\text {¢ }}$ | $\begin{gathered} M_{m} \\ \mathrm{~m}[\mathrm{kgf} \end{gathered}$ | $M_{\text {m }}$ |  |  |
| ¢ 3 | 6 | 3 | $\begin{aligned} & 4550 \\ & {[465]} \\ & 6700 \\ & {[685]} \end{aligned}$ | $\begin{gathered} 8300 \\ {[845]} \\ 12500 \\ {[1270]} \end{gathered}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 69 \\ & {[7]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \end{aligned}$ | 2.778 | $\begin{aligned} & 0.14 \\ & 0.20 \end{aligned}$ |
| M 6×0.75 | 5.5 | 11 | $\begin{aligned} & 6550 \\ & {[670]} \\ & 8900 \\ & {[910]} \end{aligned}$ | $\begin{aligned} & 12200 \\ & {[1240]} \\ & 17500 \\ & {[1780]} \end{aligned}$ | $\begin{gathered} \hline 88 \\ {[9]} \\ 127 \\ {[13]} \end{gathered}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | 3.175 | $\begin{aligned} & 0.19 \\ & 0.28 \end{aligned}$ |
| M 6×0.75 | 7 | 11 | $\begin{aligned} & 10600 \\ & {[1080]} \\ & 14400 \\ & {[1470]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 18600 \\ & {[1900]} \\ & 29100 \\ & {[2970]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 245 \\ & {[25]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & 206 \\ & {[21]} \\ & \hline \end{aligned}$ | $\begin{gathered} 69 \\ {[7]} \\ 196 \\ {[20]} \\ \hline \end{gathered}$ | 3.968 | $\begin{aligned} & 0.34 \\ & 0.51 \end{aligned}$ |
| M 6×0.75 | 8 | 11 | $\begin{aligned} & 15900 \\ & {[1620]} \\ & 23400 \\ & {[2390]} \end{aligned}$ | $\begin{aligned} & 26500 \\ & {[2700]} \\ & 43000 \\ & {[4400]} \end{aligned}$ | $\begin{aligned} & 245 \\ & {[25]} \\ & 470 \\ & {[48]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | 4.762 | $\begin{aligned} & 0.58 \\ & 0.85 \end{aligned}$ |
| M6×0.75 | 8.5 | 11 | $\begin{aligned} & 22100 \\ & {[2250]} \\ & 32500 \\ & {[3320]} \end{aligned}$ | $\begin{aligned} & 36000 \\ & {[3650]} \\ & 58500 \\ & {[5940]} \end{aligned}$ | $\begin{aligned} & 410 \\ & {[42]} \\ & 775 \\ & {[79]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 560 \\ & {[57]} \end{aligned}$ | 5.556 | $\begin{aligned} & 0.86 \\ & 1.3 \end{aligned}$ |

## LAS-EL (High load type)



Table. I-5•12

| Model No. | Assembly |  |  | Width <br> w | Length <br> L |  |  |  |  |  | slide |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ |  |  | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ |
|  |  |  |  |  |  | B | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |
| LAS15EL | 24 | 4.6 | 18.5 | 52 | 56.8 | 41 | 26 | M $5 \times 0.8 \times 8$ | 5.5 | 40 | 7 | 19.4 | 8 |
| LAS20EL | 28 | 6 | 19.5 | 59 | 65.2 | 49 | 32 | $\mathrm{M} \times \times 1 \times 10$ | 5 | 48 | 8 | 22 | 10 |
| LAS25EL | 33 | 7 | 25 | 73 | 81.6 | 60 | 35 | M $8 \times 1.25 \times 12$ | 6.5 | 60 | 12.5 | 26 | 11 |
| LAS30EL | 42 | 9 | 31 | 90 | 96.4 | 72 | 40 | M $10 \times 1.5 \times 18$ | 9 | 71 | 15.5 | 33 | 11 |
| LAS35EL | 48 | 10.5 | 33 | 100 | 108 | 82 | 50 | M $10 \times 1.5 \times 20$ | 9 | 80 | 15 | 37.5 | 12 |




## LAS-KL (Medium load type)

## LAS-FL (High load type)

- See "Table I-4*6 Standardized LS series in stock" on Page A30 for reference number of each interchangeable ball slide.


Table. I-5•13

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Height } \\ H \end{gathered}$ | $E$ | $W_{2}$ | Width <br> W | Length <br> $L$ | Mounting hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ |
|  |  |  |  |  |  | B | J | $Q \times \ell$ |  |  |  |  |  |
| LAS15KL LAS15FL | 24 | 4.6 | 18.5 | 52 | $\begin{aligned} & 40.4 \\ & 56.8 \end{aligned}$ | 41 | $\begin{aligned} & - \\ & 26 \end{aligned}$ | $4.5 \times 7$ | 5.5 | $\begin{aligned} & 23.6 \\ & 40 \end{aligned}$ | $\begin{gathered} 11.8 \\ 7 \end{gathered}$ | 19.4 | 8 |
| LAS20KL <br> LAS20FL | 28 | 6 | 19.5 | 59 | $\begin{aligned} & 47.2 \\ & 65.2 \end{aligned}$ | 49 | $\begin{aligned} & - \\ & 32 \end{aligned}$ | $5.5 \times 9$ | 5 | $\begin{aligned} & 30 \\ & 48 \end{aligned}$ | $15$ $8$ | 22 | 10 |
| LAS25KL <br> LAS25FL | 33 | 7 | 25 | 73 | $\begin{aligned} & 59.6 \\ & 81.6 \end{aligned}$ | 60 | $\begin{aligned} & - \\ & 35 \end{aligned}$ | $7 \times 10$ | 6.5 | $\begin{aligned} & 38 \\ & 60 \end{aligned}$ | $19$ $12.5$ | 26 | 11 |
| LAS30KL LAS30FL | 42 | 9 | 31 | 90 | $\begin{aligned} & 67.4 \\ & 96.4 \end{aligned}$ | 72 | $\begin{aligned} & - \\ & 40 \end{aligned}$ | $9 \times 12$ | 9 | $\begin{aligned} & 42 \\ & 71 \end{aligned}$ | $21$ $15.5$ | 33 | 11 |
| LAS35KL LAS35FL | 48 | 10.5 | 33 | 100 | $\begin{array}{r} 77 \\ 108 \end{array}$ | 82 | $\begin{aligned} & - \\ & 50 \end{aligned}$ | $9 \times 13$ | 9 | $49$ $80$ | $\begin{aligned} & 24.5 \\ & 15 \end{aligned}$ | 37.5 | 12 |

KL type


| Grease fitting |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Dynamic | Static | Static moment |  |  | $D_{w}$ | Ball slide <br> (kg) |
| Hole size | $T_{1}$ | $N$ |  | $C_{0}$ | $M_{\text {Ro }}$ | $\begin{gathered} M_{\mathrm{PO}} \\ \mathrm{~m}[\mathrm{kgf} \end{gathered}$ |  |  |  |
| ¢ 3 | 6 | 3 | $\begin{aligned} & 4550 \\ & {[465]} \\ & 6700 \\ & {[685]} \\ & \hline \end{aligned}$ | $\begin{gathered} 8300 \\ {[845]} \\ 12500 \\ \text { [1270] } \\ \hline \end{gathered}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 69 \\ & {[7]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \end{aligned}$ | $\begin{aligned} & 20 \\ & {[2]} \\ & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | 2.778 | $\begin{aligned} & 0.17 \\ & 0.26 \end{aligned}$ |
| M $6 \times 0.75$ | 5.5 | 11 | $\begin{aligned} & 6550 \\ & {[670]} \\ & 8900 \\ & {[910]} \end{aligned}$ | $\begin{aligned} & 12200 \\ & {[1240]} \\ & 17500 \\ & {[1780]} \end{aligned}$ | $\begin{aligned} & 88 \\ & {[9]} \\ & 127 \\ & {[13]} \end{aligned}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | $\begin{aligned} & 39 \\ & {[4]} \\ & 88 \\ & {[9]} \end{aligned}$ | 3.175 | $\begin{aligned} & 0.24 \\ & 0.35 \end{aligned}$ |
| M6x 0.75 | 7 | 11 | $\begin{aligned} & 10600 \\ & {[1080]} \\ & 14400 \\ & {[1470]} \end{aligned}$ | $\begin{aligned} & 18600 \\ & {[1900]} \\ & 29100 \\ & {[2970]} \end{aligned}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 245 \\ & {[25]} \end{aligned}$ | $\begin{gathered} 69 \\ {[7]} \\ 206 \\ {[21]} \\ \hline \end{gathered}$ | $\begin{gathered} 69 \\ {[7]} \\ 196 \\ {[20]} \end{gathered}$ | 3.968 | $\begin{aligned} & 0.44 \\ & 0.66 \end{aligned}$ |
| M $6 \times 0.75$ | 8 | 11 | $\begin{aligned} & 15900 \\ & {[1620]} \\ & 23400 \\ & {[2390]} \end{aligned}$ | 26500 [2700] 43000 [4400] | $\begin{aligned} & 245 \\ & {[25]} \\ & 470 \\ & {[48]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \\ & 355 \\ & {[36]} \end{aligned}$ | $\begin{aligned} & \hline 108 \\ & {[11]} \\ & 355 \\ & {[36]} \\ & \hline \end{aligned}$ | 4.762 | $\begin{aligned} & 0.76 \\ & 1.2 \end{aligned}$ |
| M $6 \times 0.75$ | 8.5 | 11 | $\begin{aligned} & 22100 \\ & {[2250]} \\ & 32500 \\ & {[3320]} \end{aligned}$ | $\begin{aligned} & 36000 \\ & {[3650]} \\ & 58500 \\ & {[5940]} \end{aligned}$ | $\begin{aligned} & \hline 410 \\ & {[42]} \\ & 775 \\ & {[79]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 177 \\ & {[18]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & \hline 177 \\ & {[18]} \\ & 560 \\ & {[57]} \end{aligned}$ | 5.556 | $\begin{aligned} & 1.2 \\ & 1.7 \end{aligned}$ |

## LS Series (Interchangeable part)

## Dimensions of LS Series (Interchangeable rail)

Regular rails Butting rails

- See "Table I-46 Standardized LS series in stock" on Page A30 for reference number of each interchangeable rail.


Table I-514
Unit: mm

|  | Rail |  |  |  |  |  |  | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model No. | Width <br> $W_{1}$ | Height <br> $H_{1}$ | Pitch <br> $F$ | Mounting bolt hole <br> $d \times D \times h$ | $B_{3}$ | G <br> Recommended | Max. length <br> () for somaxinless | Rail <br> $(\mathrm{Kg} / \mathrm{m})$ |
| L1S15 | 15 | 12.5 | 60 | $3.5 \times 6 \times 4.5^{*}$ <br> $4.5 \times 7.5 \times 5.3$ | 7.5 | 20 | 2000 <br> $(1700)$ | 1.4 |
| L1S20 | 20 | 15.5 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | 3960 <br> $(3500)$ | 2.3 |
| L1S25 | 23 | 18 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | 3960 <br> $(3500)$ | 3.1 |
| L1S30 | 28 | 23 | 80 | $7 \times 11 \times 9$ | 14 | 20 | 4000 <br> $(3500)$ | 4.8 |
| L1S35 | 34 | 27.5 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 4000 <br> $(3500)$ | 7.0 |

G dimension is $1 / 2 \mathrm{~F}^{0.5}$ for butting rail.

* Bolt holes of L1S15 is available in M3 ( $3.5 \times 6 \times 4.5$ ) and M4 ( $4.5 \times 7 \times 5.3$ ).

Please refer to Page A30 for their reference numbers.

A-I-5.3 LA Series


## (1) High rigidity and high load carrying capacity

A set of three ball grooves is made on both sides. This contributes to the increased rigidity and load carrying capacity. The top and bottom groove are formed in the circular arc, with a closer radius of ball, which ensures great rigidity and load carrying capacity. With the gothic-arch center groove, rigidity and load carrying capacity are further increased.

## (2) Moderate friction

A well-balanced combination of 2-point contacts at the top and bottom grooves and 4 points contact at the center groove provides moderate friction while ensuring rigidity by appropriate preload.

## (3) Load distribution four directions

Contact angle is set at 45 degrees in all grooves, dispersing the load to four rows irrespective of load direction. This realizes equal rigidity and load carrying capacity in vertical and lateral directions and provides well-balanced design.

## (4) Strong against shock load

Load from any direction, vertical and lateral, is received by four rows at all times. The number of the row which receives the load is larger than in other linear guides, making this series stronger against shock load.

## (5) Highly accurate

Fixing the measuring rollers is easy thanks to the gothic-arch groove. Ball-groove measuring is accurate and simple. This benefits a highly precise and stable processing.

## (6) The dust protection design

The rail's cross section is designed as simple as possible. Furthermore, the improved seal enhances the sealing function. Inner seal is available as an option.


Fig. I-59 LA Series


Fig. I-510 Super rigidity design


Fig. I-511 Rail grinding


Fig. I-512 Measuring groove accuracy

## Dimensions of LA Series (Preloaded assembly)

## LA-AL (High load type)

## LA-BL (Super high load type)

## - Specification number of preloaded assembly <br> (Custom made assembly)

LA 35 0840 AL C 2 - P6 Z3-
Model
number

## Rail length (mm)

Ball slide shape
Material/surface treatment
Number of ball slides per rail

```
Iinears to a set of 2
linear guides; no linear guides; no
code refers to one Pre load code - Z4 heavy preload
```

- P6 precision grade
- P5 high precision grade
- P4 super precision grad - P3 ultra precision grade

Table. I-515

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{\|c\|} \hline \text { Height } \\ H \\ \hline \end{array}$ | E | $W_{2}$ | Width w | Length$L$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | B | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LA35AL | 48 | 7.5 | 18 | 70 | $110.6$ | 50 | $50$ | M $8 \times 1.25 \times 10$ | 10 | $80$ | $15$ | 40.5 | 15 | M6×0.75 | 8 | 11 |
| LA35BL |  |  |  |  | 144.6 |  | 72 |  |  | 114 | 21 |  |  |  |  |  |
| LA45AL | 60 | 10 | 20.5 | 86 | $141.4$ | 60 | $60$ | M $10 \times 1.5 \times 16$ | 13 | $105$ | $22.5$ | 50 | 17 | PT1/8 | 10 | 13 |
| LA45BL |  |  |  |  | 173.4 |  | 80 |  |  | 137 | 28.5 |  |  |  |  |  |
| LA55AL | 70 | 12 | 23.5 | 100 | $165.4$ | 75 |  | M $12 \times 1.75 \times 16$ | 12.5 |  | $25.5$ | 58 | 18 | PT1/8 | 11 | 13 |
| LA55BL |  |  |  |  | 203.4 |  | 95 |  |  | 164 | 34.5 |  |  |  |  |  |

LA Series does not have a ball retainer. Be aware that balls fall out when the ball slider is withdrawn from the rail.



| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width $W_{1}$ | Height <br> $H_{1}$ | Pitch <br> F | Mounting bolt hole $d \times D \times h$ | $B_{3}$ | $\left\|\begin{array}{c} \mathrm{G} \\ \text { recomm } \\ \text { ended) } \end{array}\right\|$ | Max. length <br> $L_{\text {Omax }}$ | Dynamic <br> $C$ <br> (N[kg | $\begin{array}{\|l\|} \hline \text { Static } \\ \hline \text { gf]) } \\ \hline \end{array}$ | $\begin{aligned} & \text { Sta } \\ & \hline M_{\mathrm{Ro}} \\ & \text { ( } \mathrm{N} \cdot \mathrm{I} \end{aligned}$ |  | $\begin{aligned} & \hline \text { ent } \\ & \hline M_{\mathrm{Yo}} \end{aligned}$ <br> ]) | $D_{w}$ | Ball slide (kg) | Rail <br> (kg/m) |
| 34 | 30.8 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 4000 | $\begin{aligned} & 49400 \\ & {[5050]} \\ & 64600 \\ & {[6600]} \end{aligned}$ | $\begin{array}{c\|} \hline 82800 \\ {[8450]} \\ 120000 \\ {[12300]} \end{array}$ | $\begin{aligned} & 1070 \\ & {[109]} \\ & 1560 \\ & {[159]} \end{aligned}$ | $\begin{gathered} \hline 920 \\ {[94]} \\ 1890 \\ {[193]} \end{gathered}$ | $\begin{array}{\|c\|} \hline 920 \\ {[94]} \\ 1890 \\ {[193]} \end{array}$ | 5.556 | $\begin{aligned} & 1.3 \\ & 1.6 \end{aligned}$ | 7.7 |
| 45 | 36 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3990 | $\begin{aligned} & 73000 \\ & {[7450]} \\ & 89100 \\ & {[9100]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 124000 \\ {[12700]} \\ 166000 \\ {[17000]} \end{array}$ | $\begin{aligned} & 2190 \\ & {[223]} \\ & 2910 \\ & {[297]} \end{aligned}$ | $\begin{aligned} & 1790 \\ & {[183]} \\ & 3100 \\ & {[315]} \end{aligned}$ | $\begin{aligned} & \hline 1790 \\ & {[183]} \\ & 3100 \\ & {[315]} \end{aligned}$ | 6.350 | $\begin{aligned} & 2.5 \\ & 3.2 \end{aligned}$ | 12.0 |
| 53 | 43.2 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3960 | $\begin{array}{\|l\|} \hline 117000 \\ {[12000]} \\ 138000 \\ {[14100]} \end{array}$ | $\begin{aligned} & \hline 195000 \\ & {[19900]} \\ & 246000 \\ & {[25200]} \end{aligned}$ | $\begin{aligned} & 4000 \\ & {[410]} \\ & 5100 \\ & {[520]} \end{aligned}$ | $\begin{aligned} & \hline 3550 \\ & {[360]} \\ & 5500 \\ & {[560]} \end{aligned}$ | $\begin{aligned} & 3550 \\ & {[360]} \\ & 5500 \\ & {[560]} \end{aligned}$ | 7.937 | 3.9 <br> 5.1 | 17.2 |



## LA-AN (High load type)

## LA-BN (Super high load type)



Table. I-5-16

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width <br> W | $\left.\begin{gathered} \text { Length } \\ L \end{gathered} \right\rvert\,$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ |  | Grease fitting |  |  |
|  |  |  |  |  |  | B | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LA30AN <br> LA30BN | 45 | 7.5 | 16 | 60 | $\begin{gathered} 100.2 \\ 126.2 \end{gathered}$ | 40 | 40 <br> 60 | M $8 \times 1.25 \times 11$ | 10 | $72$ $98$ | 16 <br> 19 | 37.5 | 14 | M6×0.75 | 9.5 | 11 |
| LA35AN <br> LA35BN | 55 | 7.5 | 18 | 70 | $\begin{aligned} & 110.6 \\ & 144.6 \end{aligned}$ | 50 | $50$ $72$ | M $8 \times 1.25 \times 12$ | 10 | $\left.\begin{gathered} 80 \\ 114 \end{gathered} \right\rvert\,$ | 15 <br> 21 | 47.5 | 15 | M $6 \times 0.75$ | 15 | 11 |
| LA45AN <br> LA45BN | 70 | 10 | 20.5 | 86 | $\begin{gathered} 141.4 \\ 173.4 \end{gathered}$ | 60 | 60 $80$ | M 10×1.5×16 | 13 | $\begin{aligned} & 105 \\ & 137 \end{aligned}$ | $\begin{aligned} & 22.5 \\ & 28.5 \end{aligned}$ | 60 | 17 | PT1/8 | 20 | 13 |
| LA55AN <br> LA55BN | 80 | 12 | 23.5 | 100 | $\begin{aligned} & 165.4 \\ & 203.4 \end{aligned}$ | 75 | $75$ $95$ | M $12 \times 1.75 \times 18$ | 12.5 | $\begin{aligned} & 126 \\ & 164 \end{aligned}$ | $\begin{aligned} & 25.5 \\ & 34.5 \end{aligned}$ | 68 | 18 | PT1/8 | 21 | 13 |
| LA65AN <br> LA65BN | 90 | 14 | 31.5 | 126 | $\begin{aligned} & 196.2 \\ & 256.2 \end{aligned}$ | 76 | $\begin{aligned} & 70 \\ & 120 \end{aligned}$ | M 16×2×19 | 25 | $\begin{gathered} 147 \\ 207 \end{gathered}$ | $\begin{aligned} & 38.5 \\ & 43.5 \end{aligned}$ | 76 | 22 | PT1/8 | 19 | 13 |

[^8]

## LA-EL (High load type)

- Specification number of preloaded assembly
(Custom made assembly)
LA 35 0840 EL C 2 - P6 Z3-



## Rail length (mm)

Ball slide shape
Material/surface treatment
Number of ball slides per rail


- P6 hrecision grade precision grade
- P4 super precision grade
- P3 ultra precision grade

Table. I-5-17

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\square$ | E | $W_{2}$ | Width <br> w | $\left.\begin{gathered} \text { Length } \\ L \end{gathered} \right\rvert\,$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | B | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LA30EL <br> LA30GL | 42 | 7.5 | 31 | 90 | $\begin{aligned} & 100.2 \\ & 126.2 \end{aligned}$ | 72 | 52 | M 10x1.5 thru | 9 | $72$ $98$ | $\begin{aligned} & 10 \\ & 23 \end{aligned}$ | 34.5 | 11 | M 6×0.75 | 6.5 | 11 |
| LA35EL <br> LA35GL | 48 | 7.5 | 33 | 100 | $\begin{aligned} & 110.6 \\ & 144.6 \end{aligned}$ | 82 | 62 | M 10×1.5×15 | 9 | $\left.\begin{gathered} 80 \\ 114 \end{gathered} \right\rvert\,$ | $\begin{array}{r} 9 \\ 26 \end{array}$ | 40.5 | 12 | M 6×0.75 | 8 | 11 |
| LA45EL <br> LA45GL | 60 | 10 | 37.5 | 120 | $\begin{gathered} 141.4 \\ 173.4 \end{gathered}$ | 100 | 80 | M 12×1.75×18 | 10 | $\begin{aligned} & 105 \\ & 137 \end{aligned}$ | $\begin{aligned} & 12.5 \\ & 28.5 \end{aligned}$ | 50 | 13 | PT1/8 | 10 | 13 |
| LA55EL <br> LA55GL | 70 | 12 | 43.5 | 140 | $\begin{gathered} 165.4 \\ 203.4 \end{gathered}$ | 116 | 95 | M 14×2×21 | 12 | $\begin{aligned} & 126 \\ & 164 \end{aligned}$ | $\begin{aligned} & 15.5 \\ & 34.5 \end{aligned}$ | 58 | 15 | PT1/8 | 11 | 13 |
| LA65EL <br> LA65GL | 90 | 14 | 53.5 | 170 | $\begin{aligned} & 196.2 \\ & 256.2 \end{aligned}$ | 142 | 110 | M 16×2×24 | 14 | $\begin{aligned} & 147 \\ & 207 \end{aligned}$ | $\begin{gathered} 18.5 \\ 48.5 \end{gathered}$ | 76 | 22 | PT1/8 | 19 | 13 |

LA Series does not have a ball retainer. Be aware that balls fall out when the ball slider is withdrawn from the rail


Unit: mm

| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width <br> $W_{1}$ | Height <br> $H_{1}$ | $\begin{gathered} \text { Pitch } \\ F \end{gathered}$ | Mounting bolt hole$d \times D \times h$ | $\begin{aligned} & \\ & B_{3} \end{aligned}$ | G <br> (recomm <br> ended | Max. length$\qquad$ $L_{0 \text { max }}$ | Dynamic Static <br> $C$ $C_{0}$ <br> $(N[k g f])$  |  | Static moment |  |  | $D_{\text {w }}$ | Ball slide (kg) | $\begin{aligned} & \text { Rail } \\ & \text { (kg/m) } \end{aligned}$ |
|  |  |  |  |  |  |  |  |  | $\begin{gathered} M_{\text {RO }} \\ (\mathrm{N} \cdot \mathrm{~m} \end{gathered}$ | $\begin{array}{\|l\|} \hline M_{P O} \\ n[k g f \cdot m \end{array}$ | $M_{\mathrm{Yo}}$ |  |  |  |
| 28 | 28 | 80 | $9 \times 14 \times 12$ | 14 | 20 | 4000 | $\begin{aligned} & 35700 \\ & {[3650]} \\ & 46500 \\ & {[4750]} \end{aligned}$ | $\begin{aligned} & 60700 \\ & {[6200]} \\ & 88600 \\ & {[9050]} \end{aligned}$ | $\begin{aligned} & 635 \\ & {[65]} \\ & 940 \\ & {[96]} \end{aligned}$ | 580 <br> [59] <br> 1190 <br> [121] | $\left\lvert\, \begin{gathered} 580 \\ {[59]} \\ 1190 \\ {[121]} \end{gathered}\right.$ | 4.762 | $\begin{aligned} & 1.3 \\ & 1.8 \end{aligned}$ | 5.8 |
| 34 | 30.8 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 4000 | $\begin{aligned} & 49400 \\ & {[5050]} \\ & 64600 \\ & {[6600]} \end{aligned}$ | 82800 $[8450]$ 120000 $[12300]$ | $\begin{aligned} & 1070 \\ & {[109]} \\ & 1560 \\ & {[159]} \end{aligned}$ | $\begin{aligned} & \hline 920 \\ & {[94]} \\ & 1890 \\ & {[193]} \end{aligned}$ | 920 $[94]$ 1890 $[193]$ | 5.556 | $\begin{aligned} & 1.9 \\ & 2.6 \end{aligned}$ | 7.7 |
| 45 | 36 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3990 | $\begin{aligned} & 73000 \\ & {[7450]} \\ & 89100 \\ & {[9100]} \end{aligned}$ | $\begin{aligned} & 124000 \\ & {[12700]} \\ & 166000 \\ & {[17000]} \end{aligned}$ | $\begin{aligned} & 2190 \\ & {[223]} \\ & 2910 \\ & {[297]} \end{aligned}$ | $\begin{aligned} & 1790 \\ & {[183]} \\ & 3100 \\ & {[315]} \end{aligned}$ | $\begin{aligned} & 1790 \\ & {[183]} \\ & 3100 \\ & {[315]} \end{aligned}$ | 6.350 | $\begin{aligned} & 3.3 \\ & 4.3 \end{aligned}$ | 12.0 |
| 53 | 43.2 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3960 | $\begin{array}{\|l\|} \hline 117000 \\ {[12000]} \\ 138000 \\ {[14100]} \end{array}$ | $\begin{aligned} & \hline 195000 \\ & {[19900]} \\ & 246000 \\ & {[25200]} \end{aligned}$ | $\begin{aligned} & 4010 \\ & {[410]} \\ & 5100 \\ & {[520]} \end{aligned}$ | $\begin{aligned} & \hline 3550 \\ & {[360]} \\ & 5500 \\ & {[560]} \end{aligned}$ | $\begin{aligned} & 3550 \\ & {[360]} \\ & 5500 \\ & {[560]} \end{aligned}$ | 7.937 | $\begin{aligned} & 5.5 \\ & 7.2 \end{aligned}$ | 17.2 |
| 63 | 55 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3900 | $\begin{array}{\|l\|} \hline 210000 \\ {[21500]} \\ 275000 \\ {[28100]} \end{array}$ | $\begin{aligned} & \hline 323000 \\ & {[33000]} \\ & 475000 \\ & {[48500]} \end{aligned}$ | $\begin{array}{\|c\|} \hline 8050 \\ {[820]} \\ 11800 \\ {[1200]} \end{array}$ | $\begin{array}{\|c\|} \hline 6650 \\ {[680]} \\ 13600 \\ {[1390]} \end{array}$ | $\begin{aligned} & 6650 \\ & {[680]} \\ & 13600 \\ & {[1390]} \end{aligned}$ | $10.318$ | 11.0 15.5 | 25.9 |

## LA-FL (High load type)

- Specification number of preloaded assembly



## Rail length (mm)

## Ball slide shape

Material/surface treatment
Number of ball slides per rail


Table. I -5•18

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width <br> w | $\begin{array}{c\|} \hline \text { Length } \\ L \end{array}$ | Mounting hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $Q \times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LA30FL <br> LA30HL | 42 | 7.5 | 31 | 90 | $\begin{aligned} & 100.2 \\ & 126.2 \end{aligned}$ | 72 | 52 | $9 \times 12$ | 9 | $\begin{aligned} & 72 \\ & 98 \end{aligned}$ | $10$ $23$ | 34.5 | 11 | M6×0.75 | 6.5 | 11 |
| LA35FL <br> LA35HL | 48 | 7.5 | 33 | 100 | $\begin{aligned} & 110.6 \\ & 144.6 \end{aligned}$ | 82 | 62 | $9 \times 13$ | 9 | $\left.\begin{gathered} 80 \\ 114 \end{gathered} \right\rvert\,$ | $\begin{array}{r} 9 \\ 26 \end{array}$ | 40.5 | 12 | M 6×0.75 | 8 | 11 |
| LA45FL <br> LA45HL | 60 | 10 | 37.5 | 120 | $\begin{gathered} 141.4 \\ 173.4 \end{gathered}$ | 100 | 80 | $11 \times 15$ | 10 | $\begin{aligned} & 105 \\ & 137 \end{aligned}$ | $\begin{aligned} & 12.5 \\ & 28.5 \end{aligned}$ | 50 | 13 | PT1/8 | 10 | 13 |
| LA55FL <br> LA55HL | 70 | 12 | 43.5 | 140 | $\begin{gathered} 165.4 \\ 203.4 \end{gathered}$ | 116 | 95 | $14 \times 18$ | 12 | $\begin{gathered} 126 \\ 164 \end{gathered}$ | $\left\|\begin{array}{c} 15.5 \\ 34.5 \end{array}\right\|$ | 58 | 15 | PT1/8 | 11 | 13 |
| LA65FL <br> LA65HL | 90 | 14 | 53.5 | 170 | $\begin{aligned} & 196.2 \\ & 256.2 \end{aligned}$ | 142 | 110 | $16 \times 23$ | 14 | $\begin{aligned} & 147 \\ & 207 \end{aligned}$ | $\left\|\begin{array}{c} 18.5 \\ 48.5 \end{array}\right\|$ | 76 | 22 | PT1/8 | 19 | 13 |

[^9]

FL type

## A-I-5.4 LY Series



## (1) Equal load carrying capacity in four directions.

Contact angle is set at 45 degrees. Therefore, rigidity and load carrying capacity are equal in vertical and lateral directions.

## (2) High rigidity

All four grooves are of gothic-arch. The center of the top and bottom grooves are offset.
It is designed in such way that the contact lines of balls in top and bottom grooves cross outside as shown in Fig.I-5•14 (DB combination). This increases moment rigidity.
With preload higher than medium level (Z3, Z4), ball contact is made at four points as shown in Fig.I$5 \cdot 15$. The increase in contact points enhances both rigidity and load carrying capacity.

## (3) High resistance against shock load

Four rows support the load when a high load, such as shock, is applied.

## (4) Absorbs vibration (higher than medium preload).

The contact point becomes four under the preload which is higher than medium level (Z3, Z4). This slightly increases the friction coefficient, and enhances vibration-absorbing capacity.

## (5) Detects abnormal level of error in installation.

When the error in installation is too large, unlike other series, the friction to the four-groove gothicarch suddenly becomes large. Thus the abnormality is detected and a warning is signaled.
(6) Easy to handle, and designed with safety in mind.
Balls are retained in the retainer and do not fall out when a ball slide is withdrawn from the rail.

## (7) Highly accurate.

As shown in Fig. I-5•16, fixing the master rollers to the groove is easy thanks to the gothic-arch groove. Groove measuring is accurate.


Fig. I-5•13 LY Series


Fig. I-5•14 High rigidity design (DB combination)


Fig. I-515 Ball contact under high preload


Fig. I-5•16 Rail grinding and measuring

## Dimensions of LY Series (Preloaded assembly)

LY-AL (High load type)
LY-BL (Super high load type)

- Specification number of preloaded assembly
(Custom made assembly)

LY 350840 AL C $2-$ P6 ZO-II | Model |
| :---: |
| number | Rail length(mm)

Ball slide shape
Material/surface treatment
Number of ball slides per rail

BL type



Table. I -519

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width <br> W | $\begin{gathered} \text { Length } \\ L \end{gathered}$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LY15AL | 24 | 4.5 | 9.5 | 34 | 55 | 26 | 26 | M 4×0.7×6 | 4 | 39 | 6.5 | 19.5 | 10 | ¢ 3 | 5 | 3 |
|  | 30 | 7 | 12 | 44 | $\begin{aligned} & 69.4 \\ & 85.4 \end{aligned}$ | 32 | 36 $50$ | M 5 $\times 0.8 \times 8$ | 6 | $\begin{aligned} & 50 \\ & 66 \end{aligned}$ | 7 <br> 8 | 23 | 12 | $\phi 3$ | 5 | 3 |
| LY25AL <br> LY25BL | 36 | 5.5 | 12.5 | 48 |  | 35 | $35$ $50$ | M $6 \times 1 \times 10$ | 6.5 | $58$ <br> 80 | $\begin{aligned} & 11.5 \\ & 15 \end{aligned}$ | 30.5 | 10 | M 6×0.75 | 6 | 11 |
|  | 42 | 7.5 | 16 | 60 | $\begin{gathered} 95.2 \\ 115.2 \end{gathered}$ | 40 | 40 <br> 60 | M $8 \times 1.25 \times 11$ | 10 |  | 14 | 34.5 | 11 | M 6×0.75 | 6.5 | 11 |
| LY35AL <br> LY35BL | 48 | 7.5 | 18 | 70 | $\begin{aligned} & 110.4 \\ & 133.4 \end{aligned}$ | 50 | 50 $72$ | M $8 \times 1.25 \times 12$ | 10 | $\left\|\begin{array}{c} 80 \\ 103 \end{array}\right\|$ | $15$ $15.5$ | 40.5 | 12 | M 6×0.75 | 8 | 11 |
| LY45AL <br> LY45BL | 60 | 10 | 20.5 | 86 | $\begin{aligned} & 137 \\ & 169 \end{aligned}$ | 60 | $\begin{aligned} & 60 \\ & 80 \end{aligned}$ | M 10×1.5×16 | 13 | $\left\|\begin{array}{l} 102 \\ 134 \end{array}\right\|$ | $\begin{aligned} & 21 \\ & 27 \end{aligned}$ | 50 | 13 | PT1/8 | 10 | 13 |
| LY55AL <br> LY55BL | 70 | 13 | 23.5 | 100 | $\begin{aligned} & 160 \\ & 200 \end{aligned}$ | 75 | 75 95 | M $12 \times 1.75 \times 18$ | 12.5 | $\left\|\begin{array}{l} 120 \\ 160 \end{array}\right\|$ | $\begin{aligned} & 22.5 \\ & 32.5 \end{aligned}$ | 57 | 15 | PT1/8 | 11 | 13 |


| Unit: mm |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| Width | Height | Pitch | Mounting |  | G | Max | Dynamic | Static | Static moment |  |  | $D_{\text {w }}$ |  |  |
| $W_{1}$ | $H_{1}$ | F | bolt hole $d \times D \times h$ | $B_{3}$ | $\left\|\begin{array}{l} \text { recomm } \\ \text { ended) } \end{array}\right\|$ | length <br> $L_{0 \text { max }}$ | C | ${ }_{\text {kgf] }} \mathrm{C}_{0}$ | $\begin{array}{\|} \hline M_{\mathrm{RO}} \\ (\mathrm{~N} \end{array}$ | $M_{\text {PO }}$ $\mathrm{m}[\mathrm{kgf}$ . | $\begin{gathered} M_{y o} \\ \mathrm{~m}]) \end{gathered}$ |  |  |  |
| 15 | 14 | 60 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 20 | 2000 | $\begin{aligned} & 5950 \\ & {[605]} \end{aligned}$ | $\begin{aligned} & 7300 \\ & {[745]} \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | 3.175 | 0.16 | 1.6 |
| 20 | 19 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | 2000 | 9550 [975] 11700 [1190] | $\begin{array}{\|l\|} \hline 11100 \\ {[1130]} \\ 15100 \\ {[1540]} \\ \hline \end{array}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 147 \\ & {[15]} \end{aligned}$ | $\begin{gathered} \hline 88 \\ {[9]} \\ 137 \\ {[14]} \\ \hline \end{gathered}$ | $\begin{gathered} \hline 88 \\ {[9]} \\ 137 \\ {[14]} \end{gathered}$ | 3.968 | $\begin{aligned} & 0.3 \\ & 0.41 \end{aligned}$ | 2.9 |
| 23 | 22.5 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | 2200 | $\begin{aligned} & 17100 \\ & {[1740]} \\ & 22500 \\ & {[2290]} \end{aligned}$ | $\begin{array}{l\|} \hline 26000 \\ {[2650]} \\ 38500 \\ {[3910]} \end{array}$ | $\begin{aligned} & 305 \\ & {[31]} \\ & 345 \\ & {[35]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \\ & \hline \end{aligned}$ | 3.968 | $\begin{aligned} & 0.49 \\ & 0.66 \end{aligned}$ | 3.9 |
| 28 | 27.5 | 80 | $9 \times 14 \times 12$ | 14 | 20 | 3000 | $\begin{aligned} & 25200 \\ & {[2570]} \\ & 30500 \\ & {[3120]} \end{aligned}$ | 37500 $[3840]$ 49500 $[5030]$ | $\begin{aligned} & 530 \\ & {[54]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & 600 \\ & {[61]} \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & 600 \\ & {[61]} \end{aligned}$ | 4.762 | $\begin{aligned} & 0.82 \\ & 1.0 \end{aligned}$ | 5.8 |
| 34 | 31 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 3000 | 35000 $[3590]$ 42500 $[4330]$ | 51000 $[5220]$ 67000 $[6850]$ | $\begin{aligned} & 880 \\ & {[90]} \\ & 920 \\ & {[94]} \end{aligned}$ | $\begin{aligned} & 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | 580 $[59]$ 940 $[96]$ | 5.556 | $\begin{aligned} & 1.3 \\ & 1.6 \end{aligned}$ | 7.9 |
| 45 | 37.5 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3000 | 51500 $[5260]$ 63500 $[6450]$ | 77500 $[7880]$ 104000 $[10600]$ | $\begin{aligned} & 1790 \\ & {[183]} \\ & 1830 \\ & {[187]} \end{aligned}$ | $\begin{aligned} & 1160 \\ & {[118]} \\ & 1880 \\ & {[192]} \end{aligned}$ | $\begin{aligned} & 1160 \\ & {[118]} \\ & 1880 \\ & {[192]} \end{aligned}$ | 6.350 | $\begin{aligned} & 2.5 \\ & 3.2 \end{aligned}$ | 12.7 |
| 53 | 45 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3000 | $\left.\begin{array}{l}79500 \\ {[8090]} \\ 99000 \\ {[10100]}\end{array}\right]$ | $\begin{aligned} & 113000 \\ & {[11500]} \\ & 154000 \\ & {[15700]} \end{aligned}$ | 3050 $[313]$ 3400 $[345]$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | 7.937 | $\begin{aligned} & 3.9 \\ & 5.1 \end{aligned}$ | 17.9 |

## LY-AN (High load type)

## LY-BN (Super high load type)

- Specification number of preloaded assembly
(Custom made assembly)
LY 350840 AN C 2-P6 ZO-II Model
number Rail length(mm) Ball slide shape Material/surface treatment
Number of ball slides per rail


-P5 high precision grade
-P3 ultra precision grade


Table. I -5•20

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width <br> W | $\begin{gathered} \text { Length } \\ L \end{gathered}$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | B | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LY15AN | 28 | 4.5 | 9.5 | 34 | 55 | 26 | 26 | M $4 \times 0.7 \times 6$ | 4 | 39 | 6.5 | 23.5 | 11 | $\phi 3$ | 9 | 3 |
| LY25AN <br> LY25BN | 40 | 5.5 | 12.5 | 48 | $\begin{gathered} 80.8 \\ 102.8 \end{gathered}$ | 35 | $\begin{aligned} & 35 \\ & 50 \end{aligned}$ | M $6 \times 1 \times 10$ | 6.5 | $\begin{aligned} & 58 \\ & 80 \end{aligned}$ | $\begin{aligned} & 11.5 \\ & 15 \end{aligned}$ | 34.5 | 12 | M 6×0.75 | 10 | 11 |
| LY30AN <br> LY30BN | 45 | 7.5 | 16 | 60 | $\begin{gathered} 95.2 \\ 115.2 \end{gathered}$ | 40 | $\begin{aligned} & 40 \\ & 60 \end{aligned}$ | M $8 \times 1.25 \times 11$ | 10 | $\begin{aligned} & 68 \\ & 88 \end{aligned}$ | 14 | 37.5 | 14 | M 6×0.75 | 9.5 | 11 |
| LY35AN <br> LY35BN | 55 | 7.5 | 18 | 70 | $\begin{aligned} & 110.4 \\ & 133.4 \end{aligned}$ | 50 | $\begin{aligned} & 50 \\ & 72 \end{aligned}$ | M $8 \times 1.25 \times 12$ | 10 | $\begin{aligned} & 80 \\ & 103 \end{aligned}$ | $15$ $15.5$ | 47.5 | 15 | M 6×0.75 | 15 | 11 |
| LY45AN <br> LY45BN | 70 | 10 | 20.5 | 86 | $\begin{aligned} & 137 \\ & 169 \end{aligned}$ | 60 | $\begin{aligned} & 60 \\ & 80 \end{aligned}$ | M 10×1.5×16 | 13 | $\left\|\begin{array}{l} 102 \\ 134 \end{array}\right\|$ | $\begin{aligned} & 21 \\ & 27 \end{aligned}$ | 60 | 17 | PT1/8 | 20 | 13 |
| LY55AN <br> LY55BN | 80 | 13 | 23.5 | 100 | $\begin{aligned} & 160 \\ & 200 \end{aligned}$ | 75 | $75$ | M $12 \times 1.75 \times 18$ | 12.5 | $\left\lvert\, \begin{aligned} & 120 \\ & 160 \end{aligned}\right.$ | $22.5$ $32.5$ | 67 | 18 | PT1/8 | 21 | 13 |
| LY65AN <br> LY65BN | 90 | 14 | 31.5 | 126 | $\begin{aligned} & 184.6 \\ & 244.6 \end{aligned}$ | 76 | $\begin{gathered} 70 \\ 120 \end{gathered}$ | M 16×2×23 | 25 | $\left\|\begin{array}{c} 137 \\ 197 \end{array}\right\|$ | $\left\|\begin{array}{l} 33.5 \\ 38.5 \end{array}\right\|$ | 76 | 23 | PT1/8 | 19 | 13 |

[^10]A79

| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width | Height | Pitch | Mounting |  | G |  | Dynamic | Static | Static moment |  |  | $D_{\text {w }}$ | Ball slide (kg) | $\begin{aligned} & \text { Rail } \\ & (\mathrm{kg} / \mathrm{m}) \end{aligned}$ |
|  | $H_{1}$ |  | bolt hole $d \times D \times h$ | $B_{3}$ | $\left\|\begin{array}{l} \text { recomm } \\ \text { ended }) \end{array}\right\|$ | $L_{0 \text { max }}$ | ( $\mathrm{N}[\mathrm{kgf]}$ ) | ${ }_{\text {kgf] }}{ }_{0}$ | $\begin{gathered} M_{\mathrm{RO}} \\ (\mathrm{~N} . \end{gathered}$ | $\begin{gathered} M_{\mathrm{Po}} \\ \cdot \mathrm{~m}[\mathrm{kgf} . \end{gathered}$ | $\begin{gathered} M_{\mathrm{Yo}} \\ \mathrm{~m}]) \end{gathered}$ |  |  |  |
| 15 | 14 | 60 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 20 | 2000 | $\begin{aligned} & 5950 \\ & {[605]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 7300 \\ {[745]} \\ \hline \end{array}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | 3.175 | 0.2 | 1.6 |
| 23 | 22.5 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | 2200 | $\begin{array}{\|l\|} \hline 17100 \\ {[1740]} \\ 22500 \\ {[2290]} \end{array}$ | $\begin{aligned} & 26000 \\ & {[2650]} \\ & 38500 \\ & {[3910]} \end{aligned}$ | $\begin{aligned} & 305 \\ & {[31]} \\ & 345 \\ & {[35]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | 3.968 | $\begin{aligned} & 0.58 \\ & 0.78 \end{aligned}$ | 3.9 |
| 28 | 27.5 | 80 | $9 \times 14 \times 12$ | 14 | 20 | 3000 | $\begin{aligned} & 25200 \\ & {[2570]} \\ & 30500 \\ & {[3120]} \end{aligned}$ | $\begin{aligned} & 37500 \\ & {[3840]} \\ & 49500 \\ & {[5030]} \end{aligned}$ | $\begin{aligned} & 530 \\ & {[54]} \\ & 570 \\ & {[58]} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 355 \\ & {[36]} \\ & 600 \\ & {[61]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & 600 \\ & {[61]} \\ & \hline \end{aligned}$ | 4.762 | $\begin{aligned} & 0.91 \\ & 1.1 \end{aligned}$ | 5.8 |
| 34 | 31 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 3000 | $\begin{aligned} & 35000 \\ & {[3590]} \\ & 42500 \\ & {[4330]} \end{aligned}$ | 51000 $[5220]$ 67000 $[6850]$ | $\begin{aligned} & 880 \\ & {[90]} \\ & 920 \\ & {[94]} \end{aligned}$ | $\begin{aligned} & 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | $\begin{aligned} & 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | 5.556 | $\begin{aligned} & 1.6 \\ & 2 \end{aligned}$ | 7.9 |
| 45 | 37.5 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3000 | $\begin{aligned} & \hline 51500 \\ & {[5260]} \\ & 63500 \\ & {[6450]} \\ & \hline \end{aligned}$ | 77500 $[7880]$ 104000 $[10600]$ | $\begin{aligned} & \hline 1790 \\ & {[183]} \\ & 1830 \\ & {[187]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 1160 \\ {[118]} \\ 1880 \\ {[192]} \\ \hline \end{array}$ | $\begin{aligned} & \hline 1160 \\ & {[118]} \\ & 1880 \\ & {[192]} \end{aligned}$ | 6.350 | $\begin{aligned} & 3.2 \\ & 4.1 \end{aligned}$ | 12.7 |
| 53 | 45 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3000 | $\begin{gathered} \hline 79500 \\ {[8090]} \\ 99000 \\ {[10100]} \\ \hline \end{gathered}$ | $\left.\begin{array}{\|l\|} \hline 113000 \\ {[11500]} \\ 154000 \\ {[15700]} \end{array}\right]$ | $\begin{aligned} & 3050 \\ & {[313]} \\ & 3400 \\ & {[345]} \end{aligned}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | 7.937 | $\begin{aligned} & 4.8 \\ & 6.3 \end{aligned}$ | 17.9 |
| 63 | 53 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3000 | $\begin{aligned} & 168000 \\ & {[17100]} \\ & 225000 \\ & {[22900]} \end{aligned}$ | $\left[\begin{array}{l}226000 \\ {[23000]} \\ 340000 \\ {[34800]}\end{array}\right]$ | $\begin{array}{\|c\|} \hline 8350 \\ {[853]} \\ 10200 \\ {[1040]} \end{array}$ | $\begin{aligned} & 5350 \\ & {[544]} \\ & 9750 \\ & {[994]} \end{aligned}$ | $\begin{aligned} & 5350 \\ & {[544]} \\ & 9750 \\ & {[994]} \end{aligned}$ | 10.318 | $\left.8\right\|_{11.2} ^{8}$ | 25.1 |

Remarks: There are no LY20AN or LY20BN. LY20AL is equivalent to LY20AN. LY20BL is equivalent to LY20BN. (See Page A77)

LY-EL (High load type)
LY-GL (Super high load type)
LY-TL (High-load type, small installation tap hole)

## - Specification number of preloaded assembly

(Custom made assembly)
LY 35 0840 EL C 2-P6 ZO-II

Model
number
Rail length (mm)
Ball slide shape
Material/surface treatment
Number of ball slides per rail II refers to a set of 2
linear guides; no code

-Z0 fine clearance

- Z1 slight preload
- Z3 medium preload
ccuracy grade
- P6 precision grade
- P6 precision grade
-P5 high precision grade
$\bullet$ P4 super precision grade
- P4 super precision grade
- P3 ultra precision grade

Table. I-5•21

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | $W_{2}$ | Width <br> w | $\begin{gathered} \text { Length } \\ L \end{gathered}$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ | $T$ | Grease fitting |  |  |
|  |  |  |  |  |  | $B$ | $J$ | $M \times$ pitch $\times \ell$ |  |  |  |  |  | Hole size | $T_{1}$ | $N$ |
| LY15EL | 24 | 4.5 | 16 | 47 | 55 | 38 | 30 | M $5 \times 0.8 \times 8$ | 4.5 | 39 | 4.5 | 19.5 | 8 | $\phi 3$ | 5 | 3 |
| LY20EL <br> LY20GL | 30 | 7 | 21.5 | 63 | $\begin{aligned} & 69.4 \\ & 85.4 \end{aligned}$ | 53 | 40 | M 6 $\times 1 \times 10$ | 5 | $\begin{array}{\|l\|} \hline 50 \\ 66 \end{array}$ | $\begin{array}{r\|r} 5 \\ 13 \end{array}$ | 23 | 10 | ¢ 3 | 5 | 3 |
| LY25EL <br> LY25GL | 36 | 5.5 | 23.5 | 70 | $\begin{gathered} 80.8 \\ 102.8 \end{gathered}$ | 57 | 45 | M $8 \times 1.25 \times 16$ | 6.5 | $\begin{aligned} & 58 \\ & 80 \end{aligned}$ | $\begin{array}{r} 6.5 \\ 17.5 \end{array}$ | 30.5 | 11 | M 6×0.75 | 6 | 11 |
| LY30EL <br> LY30GL <br> LY30TL | 42 | 7.5 | 31 | 90 | $\begin{array}{r} 95.2 \\ 115.2 \\ 95.2 \end{array}$ | 72 | 52 | $\begin{aligned} & \text { M } 10 \times 1.5 \times 18 \\ & \text { M } 10 \times 1.5 \times 18 \\ & \text { M } 8 \times 1.25 \times 18 \end{aligned}$ | 9 | $\begin{aligned} & 68 \\ & 88 \\ & 68 \end{aligned}$ | $\begin{array}{r} 8 \\ 18 \\ 8 \end{array}$ | 34.5 | 11 | M 6×0.75 | 6.5 | 11 |
| LY35EL LY35GL | 48 | 7.5 | 33 | 100 | $\begin{aligned} & 110.4 \\ & 133.4 \end{aligned}$ | 82 | 62 | M 10×1.5×20 | 9 | 80 103 | $\begin{gathered} 9 \\ 20.5 \end{gathered}$ | 40.5 | 12 | M 6×0.75 | 8 | 11 |
| LY45EL LY45GL | 60 | 10 | 37.5 | 120 | $\begin{aligned} & 137 \\ & 169 \end{aligned}$ | 100 | 80 | M $12 \times 1.75 \times 24$ | 10 | $1 \begin{aligned} & 102 \\ & 134 \end{aligned}$ | $\begin{aligned} & 11 \\ & 27 \end{aligned}$ | 50 | 13 | PT1/8 | 10 | 13 |
| LY55EL <br> LY55GL | 70 | 13 | 43.5 | 140 | $\begin{aligned} & 160 \\ & 200 \end{aligned}$ | 116 | 95 | M $14 \times 2 \times 28$ | 12 | $\begin{aligned} & 120 \\ & 160 \end{aligned}$ | $\begin{aligned} & 12.5 \\ & 32.5 \end{aligned}$ | 57 | 14 | PT1/8 | 11 | 13 |
| LY65EL <br> LY65GL | 90 | 14 | 53.5 | 170 | $\begin{aligned} & 184.6 \\ & 244.6 \end{aligned}$ | 142 | 110 | M 16×2×37 | 14 | 137 197 | $\begin{aligned} & 13.5 \\ & 43.5 \end{aligned}$ | 76 | 23 | PT1/8 | 19 | 13 |

GL type



EL, TL type $\xrightarrow{M_{\text {PO }}}$

| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width | Height | Pitch | Mounting |  | G | Max | Dynamic | Static | Static moment |  |  | $D_{\text {w }}$ | Ball <br> slide <br> (kg) | $\begin{aligned} & \text { Rail } \\ & (\mathrm{kg} / \mathrm{m}) \\ & \hline \end{aligned}$ |
| $W_{1}$ | $H_{1}$ | $F$ | bolt hole $d \times D \times h$ | $B_{3}$ | $\left\lvert\, \begin{gathered} \text { (recomm } \\ \text { ended) } \end{gathered}\right.$ |  | C | ${ }_{\text {kgf] }}{ }_{0}$ | $\begin{aligned} & \hline M_{\mathrm{RO}} \\ & (\mathrm{~N} \end{aligned}$ | $\begin{gathered} M_{\mathrm{PO}} \\ \cdot \mathrm{~m}[\mathrm{kgf} \end{gathered}$ | $\begin{aligned} & M_{\mathrm{Yo}} \\ & \mathrm{~m}]) \end{aligned}$ |  |  |  |
| 15 | 14 | 60 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 20 | 2000 | $\begin{aligned} & 5950 \\ & {[605]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 7300 \\ & {[745]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \\ & \hline \end{aligned}$ | 3.175 | 0.2 | 1.6 |
| 20 | 19 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | 2000 | $\begin{array}{\|c\|} \hline 9550 \\ {[975]} \\ 11700 \\ {[1190]} \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 11100 \\ {[1130]} \\ 15100 \\ {[1540]} \end{array}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 147 \\ & {[15]} \end{aligned}$ | $\begin{aligned} & 88 \\ & {[9]} \\ & 137 \\ & {[14]} \end{aligned}$ | $\begin{gathered} \hline 88 \\ {[9]} \\ 137 \\ {[14]} \\ \hline \end{gathered}$ | 3.968 | $\begin{aligned} & 0.37 \\ & 0.51 \end{aligned}$ | 2.9 |
| 23 | 22.5 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | 2200 | $\begin{array}{\|l\|} \hline 17100 \\ {[1740]} \\ 22500 \\ {[2290]} \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 26000 \\ {[2650]} \\ 38500 \\ {[3910]} \\ \hline \end{array}$ | $\begin{aligned} & 305 \\ & {[31]} \\ & 345 \\ & {[35]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | 3.968 | $\begin{aligned} & 0.66 \\ & 0.83 \end{aligned}$ | 3.9 |
| 28 | 27.5 | 80 | $9 \times 14 \times 12$ | 14 | 20 | 3000 | $\begin{aligned} & 25200 \\ & {[2570]} \\ & 30500 \\ & {[3120]} \\ & 25200 \\ & {[2570]} \\ & \hline \end{aligned}$ | 37500 $[3840]$ 49500 $[5030]$ 37500 $[3840]$ | $\begin{aligned} & 530 \\ & {[54]} \\ & 570 \\ & {[58]} \\ & 530 \\ & {[54]} \end{aligned}$ | $\begin{aligned} & \hline 355 \\ & {[36]} \\ & 600 \\ & {[61]} \\ & 355 \\ & {[36]} \\ & \hline \end{aligned}$ | 355 $[36]$ 600 $[61]$ 355 $[36]$ | 4.762 | $\begin{aligned} & 1.1 \\ & 1.3 \\ & 1.1 \end{aligned}$ | 5.8 |
| 34 | 31 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 3000 | 35000 $[3590]$ 42500 $[4330]$ | 51000 $[5220]$ 67000 $[6850]$ | $\begin{aligned} & 880 \\ & {[90]} \\ & 920 \\ & {[94]} \end{aligned}$ | $\begin{aligned} & \hline 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | $\begin{aligned} & \hline 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | 5.556 | $\begin{aligned} & 1.7 \\ & 2.0 \end{aligned}$ | 7.9 |
| 45 | 37.5 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3000 | 51500 $[5260]$ 63500 $[6450]$ | 77500 $[7880]$ 104000 $[10600]$ | $\begin{aligned} & 1790 \\ & {[183]} \\ & 1830 \\ & {[187]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 1160 \\ \text { [118] } \\ 1880 \\ \text { [192] } \end{array}$ | $\begin{aligned} & 1160 \\ & {[118]} \\ & 1880 \\ & {[192]} \end{aligned}$ | 6.350 | $\begin{aligned} & 3.2 \\ & 3.9 \end{aligned}$ | 12.7 |
| 53 | 45 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3000 | 79500 $[8090]$ 99000 $[10100]$ | $\begin{aligned} & 113000 \\ & {[11500]} \\ & 154000 \\ & {[15700]} \end{aligned}$ | $\begin{aligned} & 3050 \\ & {[313]} \\ & 3400 \\ & {[345]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 2020 \\ {[206]} \\ 3400 \\ {[346]} \\ \hline \end{array}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | 7.937 | $\begin{aligned} & 4.9 \\ & 6.1 \end{aligned}$ | 17.9 |
| 63 | 53 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3000 | $\begin{aligned} & \hline 168000 \\ & {[17100]} \\ & 225000 \\ & {[22900]} \\ & \hline \end{aligned}$ | $\left[\begin{array}{l} 226000 \\ {[23000]} \\ 340000 \\ {[34800]} \end{array}\right.$ | $\begin{array}{c\|} \hline 8350 \\ {[853]} \\ 10200 \\ {[1040]} \end{array}$ | $\begin{aligned} & 5350 \\ & {[544]} \\ & 9750 \\ & {[994]} \end{aligned}$ | $\begin{aligned} & 5350 \\ & {[544]} \\ & 9750 \\ & {[994]} \end{aligned}$ | 10.318 | $\text { 8 } \begin{gathered} 9.3 \\ 12.3 \end{gathered}$ | 25.1 |

## LY-FL (High load type)

LY-HL (Super high load type)

- Specification number of preloaded assembly
(Custom made assembly)
LY 350840 FL C 2-P6 Z0-II Model Rail length(mm)
Ball slide shape
Material/surface treatment
Number of ball slides per rail

HL type
FL type


|  |  |  |  |  |  |  |  |  |  |  |  |  |  | nit: mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rail |  |  |  |  |  |  | Basic load rating |  |  |  |  |  Ball dia. <br>   <br> $D_{w}$  | Weight |  |
| Width$W_{1}$ | Height$H_{1}$ | Pitch <br> F | Mounting bolt hole$d \times D \times h$ |  | G |  | Dynamic | Static | Static moment |  |  |  | $\begin{array}{\|c\|} \hline \text { Ball } \\ \text { slide } \\ \text { (kg) } \end{array}$ | Rail |
|  |  |  |  | $B_{3}$ | $\left\|\begin{array}{l} \text { recomm } \\ \text { ended } \end{array}\right\|$ | $L_{0 \text { max }}$ |  | ${ }_{\text {kgf]) }} C_{0}$ | $\begin{gathered} M_{\mathrm{RO}} \\ (\mathrm{~N} . \end{gathered}$ | $\begin{gathered} M_{\mathrm{PO}} \\ \cdot \mathrm{~m}[\mathrm{kgf} \end{gathered}$ | $\begin{gathered} M_{Y 0} \\ \mathrm{~m}]) \end{gathered}$ |  |  |  |
| 15 | 14 | 60 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 20 | 2000 | $\begin{aligned} & 5950 \\ & {[605]} \end{aligned}$ | $\begin{aligned} & 7300 \\ & {[745]} \end{aligned}$ | $\begin{aligned} & 69 \\ & {[7]} \end{aligned}$ | $\begin{aligned} & 49 \\ & {[5]} \end{aligned}$ | $\begin{aligned} & 49 \\ & 151 \end{aligned}$ | 3.175 | 0.2 | 1.6 |
| 20 | 19 | 60 | $6 \times 9.5 \times 8.5$ | 10 | 20 | 2000 | 9550 $[975]$ 11700 $[1190]$ | $\begin{array}{\|l\|} \hline 11100 \\ {[1130]} \\ 15100 \\ {[1540]} \end{array}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & 147 \\ & {[15]} \end{aligned}$ | $\begin{aligned} & 88 \\ & {[9]} \\ & 137 \\ & {[14]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 88 \\ & {[9]} \\ & 137 \\ & {[14]} \end{aligned}$ | 3.968 | $\begin{aligned} & 0.37 \\ & 0.51 \end{aligned}$ | 2.9 |
| 23 | 22.5 | 60 | $7 \times 11 \times 9$ | 11.5 | 20 | 2200 | $\begin{aligned} & 17100 \\ & {[1740]} \\ & 22500 \\ & {[2290]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 26000 \\ {[2650]} \\ 38500 \\ {[3910]} \end{array}$ | $\begin{aligned} & 305 \\ & {[31]} \\ & 345 \\ & {[35]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \\ & 430 \\ & {[44]} \end{aligned}$ | 3.968 | $\begin{aligned} & 0.66 \\ & 0.83 \end{aligned}$ | 3.9 |
| 28 | 27.5 | 80 | $9 \times 14 \times 12$ | 14 | 20 | 3000 | $\begin{aligned} & 25200 \\ & {[2570]} \\ & 30500 \\ & {[3120]} \end{aligned}$ | 37500 $[3840]$ 49500 $[5030]$ | $\begin{aligned} & 530 \\ & {[54]} \\ & 570 \\ & {[58]} \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & 600 \\ & {[61]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & 600 \\ & {[61]} \end{aligned}$ | 4.762 | $\begin{aligned} & 1.1 \\ & 1.3 \end{aligned}$ | 5.8 |
| 34 | 31 | 80 | $9 \times 14 \times 12$ | 17 | 20 | 3000 | 35000 $[3590]$ 42500 $[4330]$ | $\begin{array}{\|l\|} \hline 51000 \\ {[5220]} \\ 67000 \\ {[6850]} \\ \hline \end{array}$ | $\begin{aligned} & \hline 880 \\ & {[90]} \\ & 920 \\ & {[94]} \end{aligned}$ | $\begin{aligned} & 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | $\begin{aligned} & 580 \\ & {[59]} \\ & 940 \\ & {[96]} \end{aligned}$ | 5.556 | $\begin{aligned} & 1.7 \\ & 2.0 \end{aligned}$ | 7.9 |
| 45 | 37.5 | 105 | $14 \times 20 \times 17$ | 22.5 | 22.5 | 3000 | $\begin{aligned} & 51500 \\ & {[5260]} \\ & 63500 \\ & {[6450]} \end{aligned}$ | $\begin{array}{\|l\|} \hline 77500 \\ {[7880]} \\ 104000 \\ {[10600]} \end{array}$ | $\begin{array}{\|l\|} \hline 1790 \\ {[183]} \\ 1830 \\ {[187]} \\ \hline \end{array}$ | $\begin{aligned} & 1160 \\ & {[118]} \\ & 1880 \\ & {[192]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1160 \\ & {[118]} \\ & 1880 \\ & {[192]} \end{aligned}$ | 6.350 | $\begin{aligned} & 3.2 \\ & 3.9 \end{aligned}$ | 12.7 |
| 53 | 45 | 120 | $16 \times 23 \times 20$ | 26.5 | 30 | 3000 | $\left.\begin{array}{c} 79500 \\ {[8090]} \\ 99000 \\ {[10100]} \end{array}\right]$ | $\begin{aligned} & 113000 \\ & {[11500]} \\ & 154000 \\ & {[15700]} \end{aligned}$ | $\begin{aligned} & 3050 \\ & {[313]} \\ & 3400 \\ & {[345]} \end{aligned}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & 3400 \\ & {[346]} \end{aligned}$ | 7.937 | $\begin{aligned} & 4.9 \\ & 6.1 \end{aligned}$ | 17.9 |
| 63 | 53 | 150 | $18 \times 26 \times 22$ | 31.5 | 35 | 3000 | $\left.\begin{array}{l} 168000 \\ {[17100]} \\ 225000 \\ {[22900]} \end{array}\right]$ | $\left[\begin{array}{l} 226000 \\ {[23000]} \\ 340000 \\ {[34800]} \end{array}\right]$ | $\left\|\begin{array}{c\|} \hline 8350 \\ {[853]} \\ 10200 \\ {[1040]} \end{array}\right\|$ | $\begin{array}{\|l} \hline 5350 \\ {[544]} \\ 9750 \\ {[994]} \end{array}$ | $\begin{aligned} & 5350 \\ & {[544]} \\ & 9750 \\ & {[994]} \end{aligned}$ | 10.318 | $\begin{aligned} & 9.3 \\ & 12.3 \end{aligned}$ | 25.1 |

LY15 and 20 have a single row of balls on each right and left side.

## A-I -5.5 LW Series (Wide rail type)



## (1) Ideal for use of single rail

Thanks to the wide rail, rigidity and load carrying capacity are high against moment load from rolling direction. This makes LW linear guides ideal in use of single rail linear guide as the guide way bearing.
(2) Large load carrying capacity against vertical direction
Contact angle is set at 50 degrees. This enhances load carrying capacity from vertical direction as well as rigidity.

## (3) High resistance to shock load

Same as the LH and LS series, the offset gothic-arch grooves supports a large load, such as a shock, by four rows.

## (4) High accuracy

Fixing master rollers is easy thanks to the gothicarch groove. This makes easy and accurate measuring of ball grooves.

## (5) Interchangeable rail and ball slide (short delivery time)

Randomly matching rails and ball slides are stocked as standardized interchangeable items. This reduces delivery time.
(6) Easy to handle, and designed with safety in mind.
Balls are retained in the retainer and do not fall out when a ball slide is withdrawn from the rail.


Fig. I-5•17 LW Series


Fig. I-5•18 Balls in contact

## Dimensions of LW Series (Preloaded assembly)

## LW-EL (Wide rail type)


-Standardized items in stock. See "Tables I-4.10 Standardized LW Series in stock" in Page A34.


| Rail |  |  |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width $W_{1}$ | $\begin{array}{\|c\|} \hline \text { Height } \\ H_{1} \\ \hline \end{array}$ | $B_{2}$ | $\begin{array}{\|c\|} \hline \text { Pitch } \\ F \\ \hline \end{array}$ | Mounting bolt hole $d \times D \times h$ | $B_{3}$ | $\substack{\text { G } \\ \text { (recomn } \\ \text { ended) }}$ | Max. length $L_{0 \text { max }}$ | Dynamic <br> $C$ <br> $(N[k$ | Static <br> $C_{0}$ <br> kgf] $)$ | Static  <br> $M_{\text {Ro }}$  <br> $(\mathrm{N}$.  | tatic mom <br> $M_{\text {Po }}$ <br> m[kgf. | ent <br> $M_{\text {ro }}$ <br> m]) | $D_{w}$ | Ball slide (kg) | $\begin{aligned} & \text { Rail } \\ & (\mathrm{kg} / \mathrm{m}) \end{aligned}$ |
| 33 | 8.7 | 18 | 40 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 15 | 1000 | $\begin{aligned} & 4200 \\ & {[430]} \end{aligned}$ | $\begin{aligned} & 9100 \\ & {[930]} \end{aligned}$ | $\begin{array}{\|c\|} 114 \\ {[11.6]} \end{array}$ | $\begin{gathered} 36 \\ {[3.7]} \end{gathered}$ | $\begin{gathered} 33 \\ {[3.4]} \end{gathered}$ | 2.381 | 0.2 | 2.1 |
| 37 | 10.5 | 22 | 50 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 15 | 1600 | $\begin{aligned} & 4700 \\ & {[480]} \end{aligned}$ | $\begin{aligned} & 10600 \\ & {[1080]} \end{aligned}$ | $\begin{aligned} & 147 \\ & {[15]} \end{aligned}$ | $\begin{gathered} 47 \\ {[4.8]} \end{gathered}$ | $\begin{gathered} 44 \\ {[4.5]} \end{gathered}$ | 2.381 | 0.3 | 2.9 |
| 42 | 15 | 24 | 60 | $4.5 \times 7.5 \times 5.3$ | 9 | 20 | 2000 | $\begin{gathered} 9800 \\ {[1000]} \end{gathered}$ | $\begin{gathered} 21600 \\ {[2200]} \end{gathered}$ | $\begin{gathered} 350 \\ {[35.6]} \end{gathered}$ | $\begin{gathered} 140 \\ {[14.3]} \end{gathered}$ | $\begin{gathered} 135 \\ {[13.8]} \end{gathered}$ | 3.175 | 0.5 | 4.7 |
| 69 | 19 | 40 | 80 | $7 \times 11 \times 9$ | 14.5 | 20 | 2400 | $\begin{aligned} & 25700 \\ & {[2620]} \end{aligned}$ | $\begin{aligned} & 52500 \\ & {[5340]} \end{aligned}$ | $\left\|\begin{array}{c} 1470 \\ {[149.5]} \end{array}\right\|$ | $\begin{gathered} 535 \\ {[54.4]} \end{gathered}$ | $\begin{gathered} 525 \\ {[53.5]} \end{gathered}$ | 4.762 | 1.5 | 9.6 |
| 90 | 24 | 60 | 80 | $9 \times 14 \times 12$ | 15 | 20 | 3000 | $\begin{aligned} & 47500 \\ & {[4840]} \end{aligned}$ | $\begin{aligned} & 91500 \\ & {[9350]} \end{aligned}$ | $\begin{aligned} & 3400 \\ & {[347]} \end{aligned}$ | $\left[\begin{array}{c} 1260 \\ {[128.9]} \end{array}\right]$ | $\begin{gathered} 1240 \\ {[126.2]} \end{gathered}$ | 6.350 | 4 | 15.8 |

## Dimensions of LW Series (Interchangeable ball slide)

## LAW-EL (Wide rail type)

- Standardized items in stock. See "Tables I-4•11 Standardized LW Series in stock" in Page A34.



|  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grease fitting |  |  | Dynamic | Static | Static moment |  |  | $D_{w}$ | Ball slide <br> (kg) |
| Hole size | $T_{1}$ | $N$ | (N[kgf]) |  |  | $\begin{gathered} M_{\mathrm{Po}} \\ \cdot \mathrm{~m}[\mathrm{kgf} . \end{gathered}$ | $M_{y 0}$ |  |  |
| $\phi 3$ | 4 | 3 | $\begin{aligned} & 4200 \\ & {[430]} \end{aligned}$ | $\begin{aligned} & 9120 \\ & {[930]} \end{aligned}$ | $\begin{gathered} 114 \\ {[11.6]} \end{gathered}$ | $\begin{gathered} 36 \\ {[3.7]} \end{gathered}$ | $\begin{gathered} 33 \\ {[3.4]} \end{gathered}$ | 2.381 | 0.2 |
| M 6×0.75 | 4.5 | 11 | $\begin{aligned} & 4700 \\ & {[480]} \end{aligned}$ | $\begin{aligned} & 10600 \\ & {[1080]} \end{aligned}$ | $\begin{aligned} & 147 \\ & {[15]} \end{aligned}$ | $\begin{gathered} 47 \\ {[4.8]} \end{gathered}$ | $\begin{gathered} 44 \\ {[4.5]} \end{gathered}$ | 2.381 | 0.3 |
| M 6×0.75 | 6 | 11 | $\begin{gathered} 9800 \\ {[1000]} \end{gathered}$ | $\begin{aligned} & 21600 \\ & {[2200]} \end{aligned}$ | $\begin{gathered} 350 \\ {[35.6]} \end{gathered}$ | $\begin{gathered} 140 \\ {[14.3]} \end{gathered}$ | $\begin{gathered} 135 \\ {[13.8]} \end{gathered}$ | 3.175 | 0.5 |
| M 6×0.75 | 8 | 11 | $\begin{aligned} & 25700 \\ & {[2620]} \end{aligned}$ | $\begin{aligned} & 52500 \\ & {[5340]} \end{aligned}$ | $\begin{gathered} 1470 \\ {[149.5]} \end{gathered}$ | $\begin{gathered} 535 \\ {[54.4]} \end{gathered}$ | $\begin{gathered} 525 \\ {[53.5]} \end{gathered}$ | 4.762 | 1.5 |
| PT1/8 | 14 | 14 | $\begin{aligned} & 47500 \\ & {[4840]} \end{aligned}$ | $\begin{aligned} & 91500 \\ & {[9350]} \end{aligned}$ | $\begin{aligned} & 3400 \\ & {[347]} \end{aligned}$ | $\begin{gathered} 1260 \\ {[128.9]} \end{gathered}$ | $\begin{gathered} 1240 \\ {[126.2]} \end{gathered}$ | 6.350 | 4 |

## LW Series (Interchangeable parts)

## Dimensions of LW Series (Interchangeable ball slide)

## Regular rails

## L1W (fine clearance)

-See Standardized LE Series in stock in Page A34 for reference number.


Table. I-5•25
Unit: mm

| Model No. | Rail |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Width $W_{1}$ | Height $H_{1}$ | $B_{2}$ | $\begin{gathered} \text { Pitch } \\ F \end{gathered}$ | Mounting bolt hole $d \times D \times h$ | $B_{3}$ | Gecommended | Max. length $L_{\text {omax }}$ | Weight <br> (Kg/m) |
| L1W17 | 33 | 8.7 | 18 | 40 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 15 | 1000 | 2.1 |
| L1W21 | 37 | 10.5 | 22 | 50 | $4.5 \times 7.5 \times 5.3$ | 7.5 | 15 | 1600 | 2.9 |
| L1W27 | 42 | 15 | 24 | 60 | $4.5 \times 7.5 \times 5.3$ | 9 | 20 | 2000 | 4.7 |
| L1W35 | 69 | 19 | 40 | 80 | $7 \times 11 \times 9$ | 14.5 | 20 | 2400 | 9.6 |
| L1W50 | 90 | 24 | 60 | 80 | $9 \times 14 \times 12$ | 15 | 20 | 3000 | 15.8 |

## A-I-5.6 LE Series

(Miniature wide rail type)


## (1) Ideal for use of single rail

LE Series linear guides are miniature, wide rail type. Thanks to the wide rail, load carrying capacity is high against moment load from rolling direction.
(2) Equal load carrying capacity in vertical and lateral directions
Contact angle is set at 45 degrees, equally dispersing the load from vertical and lateral directions. This also provides equal rigidity in the two directions.

## (3) Guides are super-thin.

Super-thin guides owe their design to the single ball groove on right and left sides (gothic-arch).

## (4) Highly accurate

Fixing the master rollers is easy thanks to the gothic-arc groove. Groove measuring is accurate and easy.
(5) Stainless steel is standard.

Rails and ball slides are made of martensitic stainless steel.

## (6) Interchangeable rails and ball slides (short delivery time).

Randomly-matching rails and ball slides are stocked as standardized interchangeable items. This reduces delivery time.

## (7) Ball retainer is available in some series.

Some series come with a ball retainer (ball slide model: AR and TR). Balls are retained in the retainer and do not fall out when a ball slide is withdrawn from the rail (interchangeable ball slides come with a ball retainer).


Table I-5•19 LE Series


Table I-5•20 Balls are in contact

Dimensions of LE Series
LE-AL (Wide rail, miniature)
LE-TL (Wide rail, miniature, large mounting tap hole)
LE-AR (Wide rail, miniature, with ball retainer)
LE-TR (Wide rail, miniature, large mounting tap hole, with ball retainer)

## -Specification number

LE12 0310 AL K 2-PN ZO
Model
Preload code -Z0 fine clearance
Rail length ( mm ) - Z1 slight preload

Ball slide shape
Accuracy grade

- PN normal grade

Material/surface treatment
Number of ball slides per rail

- P6 precision grade
- Standardized items in stock. See "Table I-4•10 Standardized LE Series in stock" in Page A35.interchangeable rail.


LE05, 07, 09, 12


LE15

Table. I-5•26

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  | Width <br> $W_{1}$ | Height <br> $H_{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{\|c\|} \hline \text { Height } \\ H \\ \hline \end{array}$ | E | $W_{2}$ | Width <br> w | Length <br> L | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K |  |  |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |  |
| LE05AL | 6.5 | 1.4 | 3.5 | 17 | 24 | 13 | - | M $2.5 \times 0.45 \times 2$ | 2 | 17 | 8.5 | 5.1 | 10 | 4 |
| LE07TL | 9 | 2 | 5.5 | 25 | 31 | 19 | 10 | M $3 \times 0.5 \times 3$ | 3 | 21.2 | 5.6 | 7 | 14 | 5.2 |
| $\begin{aligned} & \text { LE09AL } \\ & \text { LE09TL } \end{aligned}$ | 12 | 4 | 6 | 30 | 39 | 21 | 12 | $\begin{gathered} \text { M } 2.6 \times 0.45 \times 3 \\ \text { M } 3 \times 0.5 \times 3 \end{gathered}$ | 4.5 | 27.6 | 7.8 | 8 | 18 | 7.5 |
| $\begin{aligned} & \text { LE09AR } \\ & \text { LE09TR } \end{aligned}$ | 12 | 4 | 6 | 30 | 39.8 | 21 | 12 | $\begin{gathered} \text { M } 2.6 \times 0.45 \times 3 \\ \text { M } 3 \times 0.5 \times 3 \end{gathered}$ | 4.5 | 27.6 | 7.8 | 8 | 18 | 7.5 |
| $\begin{aligned} & \text { LE12AL } \\ & \text { LE12AR } \end{aligned}$ | 14 | 4 | 8 | 40 | $\begin{aligned} & 44 \\ & 45 \end{aligned}$ | 28 | 15 | M $3 \times 0.5 \times 4$ | 6 | 31 | 8 | 10 | 24 | 8.5 |
| $\begin{aligned} & \text { LE15AL } \\ & \text { LE15AR } \end{aligned}$ | 16 | 4 | 9 | 60 | $\begin{aligned} & \hline 55 \\ & 56.6 \end{aligned}$ | 45 | 20 | $\mathrm{M} 4 \times 0.7 \times 4.5$ | 7.5 | 38.4 | 9.2 | 12 | 42 | 9.5 |

LE has only two mounting tap holes


## LE-BL (High load type, wide rail, miniature)

## LE-UL (High load type, wide rail, miniature, large mounting tap hole)

## - Specification number <br> LE 120310 BL K 2- P6 Z0 -II II refers to a set of 2 Model number Rail length (mm) Ball slide shape Material/surface treatment <br> II refers to a set of 2 linear guides; no code refers to <br> refers to o <br> reload code - Z0 fine clearance <br> - Z1 slight preload <br> \section*{Accuracy grade}

 Number of ball slides per rail- PN normal grade
- P5 high precision grade


LE07, 09, 12


LE15

Table. I-5•27

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  | Width <br> $W_{1}$ | Height <br> $H_{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W_{2}$ | Width <br> w | Length <br> L | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K |  |  |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |  |
| LE07UL | 9 | 2 | 5.5 | 25 | 42 | 19 | 19 | M $3 \times 0.5 \times 3$ | 3 | 32.2 | 6.6 | 7 | 14 | 5.2 |
| LE09BL LE09UL | 12 | 4 | 6 | 30 | 50.5 | 23 | 24 | $\begin{gathered} \text { M } 2.6 \times 0.45 \times 3 \\ \text { M } 3 \times 0.5 \times 3 \end{gathered}$ | 3.5 | 39 | $\begin{aligned} & 7.5 \\ & 7.5 \end{aligned}$ | 8 | 18 | 7.5 |
| LE12BL | 14 | 4 | 8 | 40 | 59 | 28 | 28 | M $3 \times 0.5 \times 4$ | 6 | 46 | 9 | 10 | 24 | 8.5 |
| LE15BL | 16 | 4 | 9 | 60 | 74.5 | 45 | 35 | M $4 \times 0.7 \times 4.5$ | 7.5 | 57.8 | 11.4 | 12 | 42 | 9.5 |



| Rail |  |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pitch | Mounting bolt hole$d \times D \times h$ | $B_{3}$ | $G$(recommended) | Max. length <br> $L_{\text {omax }}$ | Dynamic Static <br> $C$ $C_{0}$ <br> (N[kgf])  |  | Static moment |  |  | $D_{w}$ | Ball slide <br> (g) | Rail <br> (g/100mm) |
| $B_{2}$ |  |  |  |  |  |  |  | $\begin{gathered} M_{\text {RO }} \\ (N \cdot n \end{gathered}$ | $\begin{gathered} M_{P O} \\ n[k g f \cdot m \end{gathered}$ | $M_{y o}$ |  |  |  |
| - | 30 | $3.5 \times 6 \times 3.2$ | 7 | 10 | 600 | $\begin{aligned} & 1670 \\ & {[170]} \end{aligned}$ | $\begin{aligned} & 2940 \\ & {[300]} \end{aligned}$ | $\begin{gathered} 21 \\ {[2.1]} \end{gathered}$ | $\begin{gathered} 13 \\ {[1.3]} \end{gathered}$ | $\begin{gathered} 13 \\ {[1.3]} \end{gathered}$ | 1.587 | 39 | 55 |
| - | 30 | $3.5 \times 6 \times 4.5$ | 9 | 10 | 800 | $\begin{aligned} & 3140 \\ & {[320]} \end{aligned}$ | $\begin{aligned} & 5390 \\ & {[550]} \end{aligned}$ | $\begin{gathered} 43 \\ {[4.4]} \end{gathered}$ | $\begin{gathered} 30 \\ {[3.1]} \end{gathered}$ | $\begin{gathered} 30 \\ {[3.1]} \end{gathered}$ | 2 | 58 | 95 |
| - | 40 | $4.5 \times 8 \times 4.5$ | 12 | 15 | 1000 | $\begin{aligned} & 4610 \\ & {[470]} \end{aligned}$ | $\begin{aligned} & 7740 \\ & {[790]} \end{aligned}$ | $\begin{gathered} 85 \\ {[8.7]} \end{gathered}$ | $\begin{gathered} 52 \\ {[5.3]} \end{gathered}$ | $\begin{gathered} 52 \\ {[5.3]} \end{gathered}$ | 2.381 | 115 | 140 |
| 23 | 40 | $4.5 \times 8 \times 4.5$ | 9.5 | 15 | 1200 | $\begin{aligned} & 8230 \\ & \text { [840] } \end{aligned}$ | $\left\|\begin{array}{l} 13000 \\ {[1330]} \end{array}\right\|$ | $\begin{gathered} 259 \\ {[26.4]} \end{gathered}$ | $\underset{[11.4]}{112}$ | $\stackrel{112}{[11.4]}$ | 3.175 | 235 | 275 |

## LE-CL (Medium load type, wide rail, miniature)

## LE-SL (Medium load type, wide rail, miniature, large mounting tap hole)

| - Specification number <br> LE120130CL |  |  |  | II. refers to a set of 2 linear guides; no code refers to one |
| :---: | :---: | :---: | :---: | :---: |
| Model number |  |  |  |  |
| Rail length (mm) |  |  |  | Preload code |
| Ball slide shape |  |  |  | -Z0 fine clearance <br> - Z1 slight preload |
| Material/surface treatment |  |  | Acc | cy grade |
| Number of ball slides per rail |  |  |  | PN normal grade |
|  |  |  |  | P5 precision grade |



Table. I-5•28

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  | Width <br> $W_{1}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W_{2}$ | Width <br> W | Length <br> L | M ounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ |  |  |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |  |
| LE05CL | 6.5 | 1.4 | 3.5 | 17 | 20 | 13 | - | M $2.5 \times 0.45 \times 2$ | 2 | 13 | 6.5 | 5.1 | 10 | 4 |
| LE07SL | 9 | 2 | 5.5 | 25 | 22.5 | 19 | - | M $3 \times 0.5 \times 3$ | 3 | 12.6 | 6.3 | 7 | 14 | 5.2 |
| $\begin{aligned} & \hline \text { LE09CL } \\ & \text { LE09SL } \end{aligned}$ | 12 | 4 | 6 | 30 | 26.5 | 21 | - | $\begin{gathered} \text { M } 2.6 \times 0.45 \times 3 \\ \text { M } 3 \times 0.5 \times 3 \end{gathered}$ | 4.5 | 15 | 7.5 | 8 | 18 | 7.5 |
| LE12CL | 14 | 4 | 8 | 40 | 30.5 | 28 | - | M $3 \times 0.5 \times 4$ | 6 | 17.5 | 8.75 | 10 | 24 | 8.5 |
| LE15CL | 16 | 4 | 9 | 60 | 41.4 | 45 | - | M $4 \times 0.7 \times 4.5$ | 7.5 | 24.8 | 12.4 | 12 | 42 | 9.5 |

## Dimensions of LE Series (Interchangeable ball slide)

LAE-AR (miniature, with ball retainer)
LAE-TR (miniature, large mounting tap hole, with ball retainer)

- Standardized items in stock. See tables for "Standardized LE Series in stock" in Page A35.


Table. I-5-29

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W_{2}$ | Width w | Length <br> $L$ | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |
|  | 12 | 4 | 6 | 30 | 39.8 | 21 | 12 | $\text { M } 2.6 \times 0.45 \times 3$ <br> M $3 \times 0.5 \times 3$ | 4.5 | 27.6 | 7.8 | 8 |
| LAE12AR | 14 | 4 | 8 | 40 | 45 | 28 | 15 | M $3 \times 0.5 \times 4$ | 6 | 31 | 8 | 10 |
| LAE15AR | 16 | 4 | 9 | 60 | 56.6 | 45 | 20 | $\mathrm{M} 4 \times 0.7 \times 4.5$ | 7.5 | 38.4 | 9.2 | 12 |


| Basic load rating |  |  |  |  | Ball dia. | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dynamic | Static | Static moment |  |  | $D_{w}$ | Ball slide |
| C | $\mathrm{C}_{0}$ | $M_{\text {Ro }}$ | $\begin{gathered} M_{\mathrm{PO}} \\ \mathrm{~m}[\mathrm{kgf} . \end{gathered}$ | $M_{\mathrm{yo}}$ |  | (g) |
| $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{aligned} & 3750 \\ & {[380]} \end{aligned}$ | $\begin{gathered} 32 \\ {[3.3]} \end{gathered}$ | $\begin{aligned} & 17 \\ & {[1.7]} \end{aligned}$ | $\begin{aligned} & 17 \\ & {[1.7]} \end{aligned}$ | 2 | 40 |
| $\begin{aligned} & 3550 \\ & {[360]} \end{aligned}$ | $\begin{aligned} & 5300 \\ & {[540]} \end{aligned}$ | $\begin{gathered} 59 \\ {[6.0]} \end{gathered}$ | $\begin{gathered} 24 \\ {[2.4]} \end{gathered}$ | $\begin{gathered} 24 \\ {[2.4]} \end{gathered}$ | 2.381 | 75 |
| $\begin{aligned} & 6200 \\ & {[630]} \end{aligned}$ | $\begin{aligned} & 8750 \\ & \text { [890] } \end{aligned}$ | $\begin{gathered} 174 \\ {[17.7]} \end{gathered}$ | $[48$ | 48 $[4.9]$ | 3.175 | 150 |

## LE Series (Interchangeable parts)

## Table of rail size for LE Series (Interchangeable rail)

## Regular rail

## L1E (fine clearance)

-See Standardized LE Series in stock in Page A35 for reference number.


Table. I-5•30
Unit: mm

| Model No. | Rail |  |  |  |  |  |  |  | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Width <br> $W_{1}$ | Height <br> $H_{1}$ | F | $B_{2}$ | $B_{3}$ | Mounting bolt hole $d \times D \times h$ | G (recommended) | Max. length $L_{\text {omax }}$ | (g/100mm) |
| L1E09 | 18 | 7.5 | 30 | - | 9 | $3.5 \times 6 \times 4.5$ | 10 | 800 | 95 |
| L1E12 | 24 | 8.5 | 40 | - | 12 | $4.5 \times 8 \times 4.5$ | 15 | 1000 | 140 |
| L1E15 | 42 | 9.5 | 40 | 23 | 9.5 | $4.5 \times 8 \times 4.5$ | 15 | 1200 | 275 |

## A-I-5.7 LU Series (Miniature type)



## (1) Super-small type.

This compact guide owes its design to the single ball groove on both right and left sides (gothic-arch) .

## (2) Equal load carrying capacity in vertical

 and lateral directionsContact angle is set at 45 degrees, equally load carrying capacity in vertical and lateral directions. This also provides equal rigidity in both directions.
(3) Stainless steel is also standardized.

Items made of the martensitic stainless steel are available as standard.

## (4) Interchangeable rails and ball slides (short delivery time)

Randomly matching rails and ball slides are stocked as standardized items. This reduces delivery time.

## (5) Some series have a ball retainer.

Ball slide types AR and TR come with a ball retainer. Balls are retained in the retainer and do not fall out when the bearing is withdrawn from the rail. (Ball slides of interchangeable parts as well as LU15AL come with a ball cage.)


Fig. I-5•21 LU Series


Fig. I-5•22 Balls are in contact.

## LU-AL (Miniature)

LU-TL (Miniature, large mounting tap hole)
LU-AR (miniature, with a ball cage)

## LU-TR (Miniature, large mounting tap hole,

 with a ball retainer)
## - Specification number

LU12 O270 AL C 2 - PN ZO- II II refers to a set of 2 Model
number
Rail length (mm)
Ball slide shape
refers to one
Preload code
-Z0 fine clearance Z1 slight preload


Material/surface treatment (See A24)

- C: Standard material
(without a ball retainer 09-15)
Number of the ball slides per rail


## Accuracy grade

-PN Normal grade
-P6 Precision grade
-P6 Precision grade
-P5 High precision grad -P5 High precision grade
$\bullet$ P4 Super precision grade

- Standardized items in stock. See tables for
"Standardized LU Series in stock" in Page A36
Table. I-531

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  | Width <br> $W_{1}$ | Height <br> $H_{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W_{2}$ | Width <br> w | Length <br> L | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | $K$ |  |  |
|  |  |  |  |  |  | $B$ | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |  |
| LU05TL | 6 | 1 | 3.5 | 12 | 18 | 8 | - | M $2 \times 0.4 \times 1.5$ | 2 | 12 | 6 | 5 | 5 | 3.2 |
| LU07AL | 8 | 1.5 | 5 | 17 | 20.4 | 12 | 8 | M $2 \times 0.4 \times 2.4$ | 2.5 | 13.6 | 2.8 | 6.5 | 7 | 4.7 |
| LU09AL LU09TL | 10 | 2.2 | 5.5 | 20 | 27 | 15 | $\begin{aligned} & 13 \\ & 10 \end{aligned}$ | $\begin{aligned} & \text { M } 2 \times 0.4 \times 2.5 \\ & M 3 \times 0.5 \times 3 \end{aligned}$ | 2.5 | 18 | $\begin{gathered} 2.5 \\ 4 \end{gathered}$ | 7.8 | 9 | 5.5 |
| LU09AR <br> LU09TR | 10 | 2.2 | 5.5 | 20 | 30 | 15 | $\begin{aligned} & 13 \\ & 10 \end{aligned}$ | $\begin{aligned} & \text { M } 2 \times 0.4 \times 2.5 \\ & \text { M } 3 \times 0.5 \times 3 \end{aligned}$ | 2.5 | 20 | $\begin{gathered} 3.5 \\ 5 \end{gathered}$ | 7.8 | 9 | 5.5 |
| LU12AL LU12TL | 13 | 3 | 7.5 | 27 | 34 | 20 | 15 | $\begin{gathered} \text { M } 2.5 \times 0.45 \times 3 \\ \text { M } 3 \times 0.5 \times 3.5 \end{gathered}$ | 3.5 | 21.8 | 3.4 | 10 | 12 | 7.5 |
| LU12AR <br> LU12TR | 13 | 3 | 7.5 | 27 | 35.2 | 20 | 15 | $\begin{gathered} \text { M } 2.5 \times 0.45 \times 3 \\ \text { M } 3 \times 0.5 \times 3.5 \end{gathered}$ | 3.5 | 21.8 | 3.4 | 10 | 12 | 7.5 |
| LU15AL | 16 | 4 | 8.5 | 32 | 43.6 | 25 | 20 | M $3 \times 0.5 \times 4$ | 3.5 | 27 | 3.5 | 12 | 15 | 9.5 |

LU05TL, LU07AL, LU0-9TL come in stainless stee only
LU05TL has only two mounting tap holes in the center.


| Rail |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pitch <br> F | Mounting bolt hole $d \times D \times h$ | $B_{3}$ | (recomme <br> nded) | $\begin{gathered} \text { Max. } \\ \text { length } \\ \text { Lomax. } \\ \text { ( ) for } \\ \text { stainless } \end{gathered}$ | Dynamic <br> $C$ <br> $(N[k$ |  | Stal $M_{\text {Ro }}$ $(N$. | atic mom $M_{\text {Po }}$ $m[k g f ~ \cdot m]$ | ent <br> $M_{\text {Yo }}$ <br> ]) | $D_{\text {w }}$ | Ball slide (g) | Rail (g/100mm) |
| 15 | $2.3 \times 3.3 \times 1.5$ | 2.5 | 5 | $(210)$ | $\begin{aligned} & 430 \\ & {[44]} \end{aligned}$ | $\begin{aligned} & 620 \\ & \text { [63] } \end{aligned}$ | $\begin{gathered} 3 \\ {[0.3]} \end{gathered}$ | $\left[\begin{array}{c} 0.7 \\ {[0.07]} \end{array}\right.$ | $\begin{gathered} 0.7 \\ {[0.07]} \end{gathered}$ | 1.2 | 4 | 11 |
| 15 | $2.4 \times 4.2 \times 2.3$ | 3.5 | 5 | $(\overline{375})$ | $\begin{aligned} & 880 \\ & {[90]} \end{aligned}$ | $\begin{aligned} & 1180 \\ & {[120]} \end{aligned}$ | $\begin{gathered} 5 \\ {[0.5]} \end{gathered}$ | $\begin{gathered} 3 \\ {[0.3]} \end{gathered}$ | $\begin{gathered} 3 \\ {[0.3]} \end{gathered}$ | 1.587 | 10 | 23 |
| 20 | $\begin{aligned} & 2.6 \times 4.5 \times 3 \\ & 3.5 \times 6 \times 4.5 \end{aligned}$ | 4.5 | 7.5 | $\begin{aligned} & 1200 \\ & (600) \end{aligned}$ | $\begin{aligned} & 1470 \\ & {[150]} \end{aligned}$ | $\begin{aligned} & 1670 \\ & {[170]} \end{aligned}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | $\begin{gathered} 7 \\ {[0.7]} \end{gathered}$ | $\begin{gathered} 7 \\ {[0.7]} \end{gathered}$ | 2 | 17 | 35 |
| 20 | $\begin{aligned} & 2.6 \times 4.5 \times 3 \\ & 3.5 \times 6 \times 4.5 \end{aligned}$ | 4.5 | 7.5 | $(\overline{600})$ | $\begin{aligned} & 1180 \\ & {[120]} \end{aligned}$ | $\begin{aligned} & 1770 \\ & {[180]} \end{aligned}$ | $\begin{gathered} 9 \\ {[0.9]} \end{gathered}$ | $\begin{gathered} 5 \\ {[0.5]} \end{gathered}$ | $\begin{gathered} 5 \\ {[0.5]} \end{gathered}$ | 1.587 | 19 | 35 |
| 25 | $\begin{aligned} & 3 \times 5.5 \times 3.5 \\ & 3.5 \times 6 \times 4.5 \end{aligned}$ | 6 | 10 | $\begin{aligned} & 1800 \\ & (800) \end{aligned}$ | $\begin{aligned} & 2160 \\ & {[220]} \end{aligned}$ | $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{gathered} 22 \\ {[2.2]} \end{gathered}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | 2.381 | 38 | 65 |
| 25 | $\begin{aligned} & 3 \times 5.5 \times 3.5 \\ & 3.5 \times 6 \times 4.5 \end{aligned}$ | 6 | 10 | (800) | $\begin{aligned} & 2160 \\ & {[220]} \end{aligned}$ | $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{gathered} 22 \\ {[2.2]} \end{gathered}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | 2.381 | 38 | 65 |
| 40 | $3.5 \times 6 \times 4.5$ | 7.5 | 15 | $\begin{gathered} 2000 \\ (1000) \end{gathered}$ | $\begin{aligned} & 4300 \\ & {[440]} \end{aligned}$ | $\begin{aligned} & 4500 \\ & {[460]} \end{aligned}$ | $\begin{gathered} 42 \\ {[4.3]} \end{gathered}$ | $\begin{gathered} 22 \\ {[2.2]} \end{gathered}$ | $\begin{gathered} 22 \\ {[2.2]} \end{gathered}$ | 3.175 | 70 | 105 |

To fix rail of LUO5TL, use M2 $\times 0.4$ cross-recessed pan head machine screw for precision instrument. CIS 10-70 No. O pan head machine screw No.1.)
(J CIS : J apanese Camera Industrial Standard.)

## LU-BL (High load type, miniature)

## LU-UL (High load type, miniature, large mounting tap hole)

## - Specification number

LU 12 0270 BL_ $\mathbf{C}$ - PN Z은II II refers to a set of 2 Model
number
Rail length (mm)
Ball slide shape
Material/surface treatment (See A24)
Material/surface treatment (See A24)

- C : Standard material - K : Stainless steel

Number of the ball slides per rail
-PN Normal grade
-P6 Precision grade
-P5 High precision grade
•P4 Super precision grade


Table. I-5-32

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  | Width $W_{1}$ | Height <br> $H_{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $E$ | $W_{2}$ | Width <br> W | Length <br> L | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K |  |  |
|  |  |  |  |  |  | B | J | $M \times$ pitch $\times \ell$ |  |  |  |  |  |  |
| LU09BL <br> LU09UL | 10 | 2.2 | 5.5 | 20 | 41 | 15 | 16 | $\begin{gathered} M 2 \times 0.4 \times 2.5 \\ M 3 \times 0.5 \times 3 \end{gathered}$ | 2.5 | 31.2 | 7.6 | 7.8 | 9 | 5.5 |
| LU12BL <br> LU12UL | 13 | 3 | 7.5 | 27 | 47.5 | 20 | 20 | $\begin{aligned} & \text { M } 2.5 \times 0.45 \times 3 \\ & \text { M } 3 \times 0.5 \times 3.5 \end{aligned}$ | 3.5 | 35.3 | 7.65 | 10 | 12 | 7.5 |
| LU15BL | 16 | 4 | 8.5 | 32 | 61 | 25 | 25 | $\mathrm{M} 3 \times 0.5 \times 4$ | 3.5 | 44.4 | 9.7 | 12 | 15 | 9.5 |

## LU Series (Interchangeable parts)

Dimensions of LU Series (Interchangeable ball slide)
LAU-AR (Miniature, with a ball retainer)
LAU-TR (Miniature, large mounting tap hole, with a ball retainer)

- Standardized items in stock. See tables for "Standardized LU Series in stock" in Page A37.


Table. I-533

| Model No. | Assembly |  |  | Ball slide |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | E | W。 | Width w | Length <br> L | Mounting tap hole |  |  | $B_{1}$ | $L_{1}$ | $J_{1}$ | K |
|  |  |  |  |  |  | B | J | $M \times$ pitch $\times \ell$ |  |  |  |  |
| LAU09AR |  |  |  |  |  |  | 13 | $\mathrm{M} 2 \times 0.4 \times 2.5$ |  |  | 3.5 |  |
| LAU09TR |  |  |  |  |  |  | 10 | M $3 \times 0.5 \times 3$ |  |  | 5 |  |
| LAU12AR |  |  |  |  |  |  |  | M $2.5 \times 0.45 \times 3$ |  |  |  |  |
| LAU12TR |  |  |  |  |  |  |  | M $3 \times 0.5 \times 3.5$ |  |  |  |  |
| LAU15AL | 16 | 4 | 8.5 | 32 | 43.6 | 25 | 20 | $\mathrm{M} 3 \times 0.5 \times 4$ | 3.5 | 27 | 3.5 | 12 |

[^11]| Basic load rating |  |  |  |  | Ball dia. | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dynamic | Static | Static moment |  |  | D | Ball slide |
| $\left.C\right\|_{(\mathrm{N}[\mathrm{kgf}])} C_{0}$ |  | $M_{\text {¢ }}$ | $\begin{gathered} M_{\text {a }} \\ \mathbb{m}[k g f \end{gathered}$ | $\overline{M_{x n}}$ |  | (g) |
| $\begin{aligned} & 1180 \\ & {[120]} \end{aligned}$ | $\begin{aligned} & 1770 \\ & {[180]} \end{aligned}$ | $\begin{gathered} 9 \\ {[0.9]} \end{gathered}$ | $\begin{gathered} 5 \\ {[0.5]} \end{gathered}$ | $\begin{gathered} 5 \\ {[0.5]} \end{gathered}$ | 1.587 | 19 |
| $\begin{aligned} & 2160 \\ & {[220]} \end{aligned}$ | $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{gathered} 22 \\ {[2.2]} \end{gathered}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | $\begin{gathered} 12 \\ {[1.2]} \end{gathered}$ | 2.381 | 38 |
| $\begin{aligned} & 4300 \\ & {[440]} \end{aligned}$ | $\begin{aligned} & 4500 \\ & {[460]} \end{aligned}$ | $\begin{gathered} 42 \\ {[4.3]} \end{gathered}$ | $\begin{gathered} 22 \\ {[2.2]} \end{gathered}$ | 22 $[2.2]$ | 3.175 | 70 |

## LU Series (Interchangeable parts)

## Dimensions of LU Series (Interchangeable rail)

## Regular rail

## LIU (fine clearance)

- See Standardized LU Series in stock in Page A37 for reference codes of interchangeable items.


Table. I-5•34

| Model No. | Rail |  |  |  |  |  |  | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Width $W_{1}$ | Height $H_{1}$ | $F$ | $B_{3}$ | Mounting bolt hole $d \times D \times h$ | G <br> (recommended) | Max. length $L_{\text {omax. }}$ ( ) for stainless | (g/100mm) |
| $\begin{aligned} & \text { L1U09*S } \\ & \text { L1U09*TS } \end{aligned}$ | 9 | 5.5 | 20 | 4.5 | $\begin{aligned} & 2.6 \times 4.5 \times 3 \\ & 3.5 \times 6 \times 4.5 \end{aligned}$ | 7.5 | (600) | 35 |
| $\begin{aligned} & \text { L1U12*S } \\ & \text { L1U12*TS } \end{aligned}$ | 12 | 7.5 | 25 | 6 | $\begin{aligned} & 3 \times 5.5 \times 3.5 \\ & 3.5 \times 6 \times 4.5 \end{aligned}$ | 10 | (800) | 65 |
| L1U15 | 15 | 9.5 | 40 | 7.5 | $3.5 \times 6 \times 4.5$ | 15 | $\begin{gathered} 2000 \\ (1000) \end{gathered}$ | 105 |

The mark ( ${ }^{*}$ ) denotes the length of rail (unit: mm).

## A-I-5.8 LL Series



## (1) Super light-weight, and compact

This compact guide has a single ball groove on both right and left sides (gothic arch). Rails and ball slides are made of stainless steel plate, therefore they are lightweight.
Also, the ball groove is made outside the ball slide to reduce overall size and to obtain high speed.

## (2) Stainless steel is standard.

Rails and bearings are made of martensitic stainless steel.


Fig. I-5023 LL Series


Fig. I-5024 LL Series structure

NSK

## Dimensions of LL Series

LL (Miniature, light-weight)

## - Specification number <br> LL15 060 PL 1-PN ZO <br> number <br> Rail length (mm) <br> Ball slide shape <br> Number of ball slides per rail Accuracy grade: Only PN normal grade is available



Table. I-535

| Model No. | Assembly |  | Ball slide |  |  |  |  |  |  | Height <br> $H_{1}$ | Pitch <br> F | $N$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Height <br> H | $W_{1}$ | Width <br> w | Length <br> $\ell$ | Mounting tap hole |  | MT | $J_{1}$ | K |  |  |  |
|  |  |  |  |  | J | $M \times$ pitch |  |  |  |  |  |  |
| LL15 | 6.5 | 15 | 10.6 | 27 | 13 | M $3 \times 0.5$ | 1.2 | 7 | 1.5 | 5 | 30 40 30 40 50 | 1 1 2 2 2 |

Remarks:

1. LL Series does not have a ball retainer. Be aware that the balls fall out when a bearing is withdrawn from the rai
2. Seal Is not available. Please provide the dust-prevention measures on the equipment.
3. Do not use an installation screw on the ball slide which exceeds MT (maximum screw depth allowance) in the dimension table.


| Rail |  |  |  |  | Basic load rating |  |  |  |  | Ball dia. | Weight |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mounting bolt hole$d \times D \times h$ | $N \mathrm{H}$ | $B_{3}$ | G | Rail length <br> $L_{0}$ | Dynamic Static <br> $C$ $C_{o}$ <br> (N[kgf])  |  | Static moment |  |  | $D_{w}$ | Ball slide <br> (g) | Rail <br> (g) |
|  |  |  |  |  |  |  | $\begin{array}{r} M_{\text {RO }} \\ (N \end{array}$ | $M_{P O}$ <br> [ [kgf . | $\begin{aligned} & M_{y o} \\ & \text { 7]) } \end{aligned}$ |  |  |  |
| $2.4 \times 5 \times 0.4$ | 1.2 | 7.5 | $\begin{gathered} 5 \\ 10 \\ 7.5 \\ 5 \\ 10 \end{gathered}$ | $\begin{gathered} 40 \\ 60 \\ 75 \\ 90 \\ 120 \end{gathered}$ | $\begin{aligned} & 880 \\ & {[90]} \end{aligned}$ | $\begin{aligned} & 785 \\ & {[80]} \end{aligned}$ | $\begin{gathered} 7 \\ {[0.7]} \end{gathered}$ | $\begin{gathered} 3 \\ {[0.3]} \end{gathered}$ | $\begin{gathered} 3 \\ {[0.3]} \end{gathered}$ | 2 | 6 | 9 11 13 16 21 |

## A-I-6 Guide to Technical Services

## (1) CAD drawing data

NSK offers CAD data for linear guides. Data are available on magnetic tape (M/T) or floppy disk (FD).

| Available <br> format | Media |  |  |
| :---: | :---: | :---: | :---: |
|  | $\mathrm{M} / \mathrm{T}$ | $\operatorname{FD}\left(3.5^{\prime \prime}\right)$ | $\operatorname{FD}\left(5.25^{\prime \prime}\right)$ |
| CADAM | 0 |  |  |
| IGES | 0 |  |  |
| MICRO-CADAM |  | 0 | 0 |
| DXF |  | 0 | 0 |

- Data in drawings are filed in the actual size (some parts are simplified). You can use these data without processing.
- Drawings are three-views projection.
- Dimension lines are omitted to render the data as standard drawing for database.


## Data offered by CAD

NSK linear guides
LH Series
LS Series
LA Series
LY Series
LW Series
LE Series
LU Series

## (2) Technical support

For inquiries and advice, call the number below.
Linear Motion Engineering Department, Precision Machinery \& Parts

## Technology Center <br> Tel: 027-254-7718 (J apan) <br> Or call your local NSK representative.

## A-I -7 Linear Guide: Handling Precautions

NSK linear guides are of high quality and are easy to use. NSK places importance on safety in design. For maximum safety, please follow precautions as outlined below.

## (1) Lubrication



## Confirm lubrication

a. If your linear guide is of rust prevention specification, thoroughly wipe the rust prevention oil, and put lubricant inside of ball slide before using.
b. If you are using oil as lubricant, the oil may not reach the ball groove depending on how the ball slide is installed. Consult NSK in such case.

## (2) Handling


a. Interchangeable ball slides (randomly matching types between rail and ball slide) are installed to the provisional rail when they leave the factory. Handle the ball slide with care during installation to the rail.
b. Do not disassemble the guide unless absolutely necessary. Not only does it allow dust to enter, but it lessens precision.
c. Ball slide may move by simply leaning the rail. Make sure that the ball slide does not disengage from the rail.
d. Standard end cap is made of plastic. Beating it or hitting it against an object may cause damage.

## (3) Precautions in use



Prevent rust


Watch for hanging upside-down


## Temperature limitation

a. Make every effort to not allow dust and foreign objects to enter.
b. The temperature of the place where linear guides are used should not exceed 80 (excluding heatresistant type linear guides). A higher temperature may damage the plastic end cap.
c. If the user cuts the rail, thoroughly remove burrs and sharp edges on the cut surface.
d. When hanging upside-down (e.g. the rail is installed upside-down on the ceiling in which the ball slide faces downward), should the end cap be damaged, causing the balls to fall out, the ball slide may be detached from the rail and fall. For such use, take measures including installing a safety device.

## (4) Storage



Store in the correct position
a. Linear guide may bend if the rail is stored in inappropriate position. Place it on a suitable surface, and store it in a flat position.

# A- II Technical Description of NSK Linear Guides 

## A-II-1 Accuracy

## A-II-1.1 Accuracy Standard

-Table II-1•1, Figure II-1•1 and Figure II-1•2 show accuracy characteristics.
Table II-1•1 Definition of accuracy

| Characteristics | Definition (Figures II-1•1, II-1•2) |
| :--- | :--- |
| Mounting height $H$ | Distance from A (rail bottom datum face) to C (ball slide top face) |
| Variation of $H$ | Variation of $H$ between assembled ball slides installed in the rails <br> of a set of linear guide |
| Mounting width <br> $W_{2}$ or $W_{3}$ | Distance from B (rail side datum face) to D (ball slide side datum face). <br> Applicable only to the reference linear guide. |
| Variation of $W_{2}$ or $W_{3}$ | Difference of the width $\left(W_{2}\right.$ or $W_{3}$ ) between the assembled ball slides <br> which are installed in the same rail. Applicable only to the reference <br> linear guide. |
| Running parallelism of |  |
| ball slide, face $C$ to face $A$ |  | | Variation of C (ball slide top face) to A (rail bottom datum face) when |
| :--- |
| ball slide is moving. |



Fig. II-1.1 Assembled accuracy (Height and width)


Fig. II-1.2 Running parallelism of ball slide

## Mounting width: $\boldsymbol{W}_{\mathbf{2}} \boldsymbol{W}_{\mathbf{3}}$

- Mounting width differs depending on the arrangement of the datum faces of the rail and ball


Fig. II-1•3 Mounting width $W_{2}$

## A-II-1.2 Running Parallelism of Ball Slide

- Running parallelism of ball slide is common in all series. Specifications of all accuracy grades are shown in Table II-1•2.
slide on the reference linear guide (indicated as KL on the rail). (Fig. II-1•3 and Fig. II-1•4)


Fig. II-14 Mounting width $W_{3}$

However, applicable accuracy grades differ by series. Please refer to "Table I-3.1 Accuracy grade and applicable series" on page A20.

Table II-12 Running parallelism of ball slide
Unit: $\mu \mathrm{m}$

|  | Preloaded assembly (Non-interchangeable) |  |  |  |  | Interchangeable <br> type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rail over all <br> length (mm) | Ultra <br> precision P3 | Super <br> precision P4 | High <br> precision | Precision <br> grade | Normal grade <br> PN | Normal grade <br> PC |
| $\sim 50$ | 2 | 2 | 2 | 6 | 12 | 12 |
| $50 \sim 80$ | 2 | 2 | 3 | 7 | 13 | 13 |
| $80 \sim 125$ | 2 | 2 | 3.5 | 8 | 14 | 14 |
| $125 \sim 200$ | 2 | 2 | 4 | 9 | 15 | 15 |
| $200 \sim 250$ | 2 | 2.5 | 5 | 10 | 17 | 17 |
| $250 \sim 315$ | 2 | 2.5 | 5 | 11 | 17 | 17 |
| $315 \sim 400$ | 2 | 3 | 6 | 11 | 18 | 18 |
| $400 \sim 500$ | 2 | 3 | 6 | 12 | 19 | 19 |
| $500 \sim 630$ | 2 | 3.5 | 7 | 13 | 20 | 20 |
| $630 \sim 800$ | 2 | 4.5 | 8 | 14 | 22 | 22 |
| $800 \sim 1000$ | 2.5 | 5 | 9 | 16 | 23 | 23 |
| $1000 \sim 1250$ | 3 | 6 | 10 | 17 | 25 | 25 |
| $1250 \sim 1600$ | 4 | 7 | 11 | 19 | 27 | 27 |
| $1600 \sim 2000$ | 4.5 | 8 | 13 | 21 | 29 | 29 |
| $2000 \sim 2500$ | 5 | 10 | 15 | 22 | 31 | 31 |
| $2500 \sim 3150$ | 6 | 11 | 17 | 25 | 33 | 33 |
| $3150 \sim 4000$ | 9 | 16 | 23 | 30 | 38 | 38 |

## A-II-1.3 Accuracy Standard in Each Series

## LH, LS, LA, LY, LW Series

Table II-1.3 shows accuracy standards of the preloaded assembly in LH, LS, LA, LY and LW Series. Table II-1.4 shows accuracy standards of LH

Series interchangeable type. Table II-1•5 shows accuracy standards of LS and LW Series interchangeable type.

Table II-1•3 Tolerance of preloaded assembly in LH, LS, LA, LY and LW Series
Unit: $\mu \mathrm{m}$

| Characteristic Accuracy grade | $\underset{\text { P3 }}{ }$ Ultra precision | $\begin{array}{\|c\|} \hline \text { Super } \\ \text { precision P4 } \\ \hline \end{array}$ | $\left\lvert\, \begin{gathered}\text { High precision } \\ \text { P5 }\end{gathered}\right.$ | Precision grade P6 | Normal grade PN |
| :---: | :---: | :---: | :---: | :---: | :---: |
| M ounting height $H$ | $\pm 10$ | $\pm 10$ | $\pm 2$ | $\pm 40$ | $\pm 80$ |
| Variation of $H$ (all ball slides installed in rails for a set of linear guides) | 3 | 5 | 7 | 15 | 25 |
| M ounting width $\mathrm{W}_{2}$ or $\mathrm{W}_{3}$ | $\pm 15$ | $\pm 15$ | $\pm 25$ | $\pm 50$ | $\pm 100$ |
| Variation of $W_{2}$ or $W_{3}$ <br> (all ball slides on the reference linear guide) | 3 | 7 | 10 | 20 | 30 |

Running parallelism of ball slide, face C to face A
Refer to Table II-1•2, Figure II-1•5 and Figure II-1•6 Running parallelism of ball slide, face $D$ to face $B$

Table II-14 Tolerance of interchangeable type in LH Series •Normal grade (PC) Unit: $\mu \mathrm{m}$

| Characteristic Model No. |  | LH20 | LH25, 30, 35 | LH45, 55, 65 |
| :---: | :---: | :---: | :---: | :---: |
|  | Mounting height $H$ Variation of $H$ | $\begin{gathered} \pm 30 \\ 60 \end{gathered}$ | $\begin{gathered} \pm 35 \\ 70 \end{gathered}$ | $\begin{gathered} \pm 45 \\ 90 \end{gathered}$ |
|  | Mounting width $W_{2}$ or $W_{3}$ Variation of width $W_{2}$ or $W_{3}$ | $\begin{gathered} \pm 40 \\ \hline+40 \end{gathered}$ | $\begin{gathered} \pm 40 \\ \hline+0 \end{gathered}$ | $\begin{aligned} & \pm 50 \\ & 100 \end{aligned}$ |
|  | Running parallelism of ball slide, face C to face A Running parallelism of ball slide, face $D$ to face $B$ | Refer to Table I-1•2, Figure I-3•1, Figure I-3•2 |  |  |
|  | Mounting height $H$ Variation of $H$ | $\begin{aligned} & \pm 30 \\ & 60 \end{aligned}$ |  |  |
|  | Mounting width W/ 2 or W3 Variation of $W_{2}$ or $W_{3}$ (W/2 or $W_{3}$ ) |  | 40 | $\begin{aligned} & \pm 50 \\ & 100 \end{aligned}$ |
|  | Running parallelism of ball slide, face C to face A running parallelism, face C to face B | Refer to Table II-1•2, Figure II-1•5 and Figure II-1•6 |  |  |

Table II-1.5 Tolerance of interchangeable type in LS and LW Series $\bullet$ Normal grade (PC)
Unit: $\mu \mathrm{m}$

| Characteristic Model No. | $\begin{aligned} & \text { LS15, 20, 25, 30, } 35 \\ & \text { LW17, 21, 27, } 35,50 \\ & \hline \end{aligned}$ |
| :---: | :---: |
| Mounting height $H$ | $\pm 30$ |
| Variation of H | 60 |
| Mounting width W/ ${ }^{2}$ or W3 | $\pm 30$ |
| Variation of width W/ or W3 | 60 |
| Running parallelism of ball slide, face C to face A Running parallelism of ball slide, face $D$ to face $B$ | Refer to Table $\mathbb{I}-1 \cdot 2$, Figure $\mathbb{I}-1 \cdot 5$ and Figure II $1 \cdot 6$ |



Fig II-15 Mounting width ( $W_{2}$ )


Fig II-16 Mounting width ( $W_{3}$ )

## LE, LU Series

Table II-1•6 shows tolerance of preloaded assembly in LE and LU Series. Table II-1•7 shows tolerance of LE and LU Series intercahngeable type.

Table II-16 Tolerance of preloaded assembly in LE and LU Series
Unit: $\mu \mathrm{m}$ A

| Characteristic Accuracy grade | $\begin{aligned} & \hline \text { Super precision } \\ & \text { P4 } \end{aligned}$ | High precision P5 | $\begin{gathered} \hline \text { Precision grade } \\ \text { P6 } \end{gathered}$ | Normal grade PN |
| :---: | :---: | :---: | :---: | :---: |
| M ounting height $H$ <br> Variation of $H$ (all ball slides installed in rails for a set of linear guides) | $\frac{ \pm 10}{5}$ | $\frac{ \pm 15}{7}$ | $\frac{ \pm 20}{15}$ | $\begin{aligned} & \frac{+40}{25} \end{aligned}$ |
| M ounting width $W_{2}$ or $W_{3}$ <br> Variation of $W_{2}$ or $W_{3}$ <br> (all ball slides on the reference linear guide) | $\frac{ \pm 15}{7}$ | $\frac{+20}{10}$ | $\begin{aligned} & \pm 30 \\ & 20 \end{aligned}$ | $\begin{aligned} & \pm 50 \\ & 30 \end{aligned}$ |
| Running parallelism of ball slide, face C to face A Running parallelism of ball slide, face $D$ to face $B$ | Refer to Table II-1•2, Figure II-3•7 and Figure II-1•8 |  |  |  |

Table II-107 Tolerance of interchangeable type in LE and LU Series Normal grade (PC) Unit: $\mu \mathrm{m}$

| M odel $N o$ | LU09, 12,15 |
| :--- | :---: |
| Characteristic | LE09, 12,15 |
| Mounting height $H$ | $\pm 20$ |
| Variation of $H$ | 40 |
| Mounting width $W_{2}$ or $W_{3}$ | $\pm 20$ |
| Variation of width W Wr $W_{3}$ | 40 |
| Running parallelism of ball slide, face C to face A | Refer to Table I-1•2, |
| Running parallelism of ball slide, face to face B | Fig. II-3•7 and Fig. II-1•8 |

Indication of idatum face in LE and LU Series is different from other series. Refer to Table II-1•8.


Fig. II-1•7 Mounting width ( $W_{2}$ )


Fig. II-18 Mounting width ( $W_{3}$ )

Table II-1.8 Indication of rail datum face in LE and LU Series

| M odel No. | LU05,07, 09 <br> LE05, 07, 09, 12 | LU12, 15 | LE15 <br> Material |
| :--- | :---: | :---: | :---: |
| Special high <br> carbon steel |  |  |  |

## LL Series

Table II-1•9 shows tolerance of LL Series.
Table II-149 Tolerance of LL Series Normal grade (PN)

Unit: $\mu \mathrm{m}$

| M odel No. | LL15 |
| :--- | :---: |
| Characteristic | $\pm 20$ |
| M ounting height | 20 |
| Running parallelism, face C to face A <br> Running parallelism, face D to face B B | (See Fig. II -1-9) |

## A-II-2 Preload and Rigidity

## A-II-2.1 Preload and rigidity

- In NSK linear guides, slight size changes of balls, which are going to be inserted in the ball slide, controls clearance and amount of preload.
- In NSK linear guide, rigidity is further increased and elastic deformation is reduced by applying preload.
- In general, a load range in which the preload is effective becomes about 2.8 times of the preload (Fig. II-2•1).
- Fig. II-2•2 shows the relationship of ball slide deformation by external vertical load and preload. LY35 is used as a case.
- The following show the definition of linear guide rigidity.

1) Radial rigidity: Rigidity of vertical and lateral directions -- up/down and right/left (Fig. II-2•3).
2) Moment rigidity: Three moment directions -pitching, rolling, and yawing (Fig. II-2•4).


Fig. II -2•3 Radial rigidity

- Since two rails and four ball slides are used in general as a pair, considering only the radial rigidity is sufficient.


Fig. II-19 Standard LL


Fig. II-2•1 Elastic deformation


Fig. II-2.2 Rigidity of LY35, downward direction load (example)


Fig. II-24 Moment rigidity

- However, in cases as shown in Fig. II-2•5, Fig. II- $2 \cdot 6$ and Fig. $\mathbb{I I}-2 \cdot 7$, it is necessary to take into account the moment rigidity in addition to the radial rigidity.


Fig. II-2.5 Pitching direction


Fig. II-26 Rolling direction


Fig. II-2•7 All directions

## A-II-2.2 Preload and Rigidity of Each Series

## LH Series (Preloaded assembly)

Table II-2•1 shows preload and rigidity of preloaded assembly of LH Series.
Table II-2•1 Preload and rigidity of preloaded assembly of LH Series

|  | Model No. | Preload N [kgf] |  | Rigidity $\mathrm{N} / \mu \mathrm{m}$ [kgf/ $/ \mathrm{m}$ ] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Vertical directions |  | Lateral direction |  |
|  |  | $\begin{gathered} \text { Slight preload } \\ \text { Z1 } \end{gathered}$ | $\begin{array}{\|c} \hline \text { Medium preload } \\ Z 3 \end{array}$ | $\begin{gathered} \text { Slight preload } \\ \text { Z1 } \end{gathered}$ | Medium preload Z3 | $\begin{gathered} \text { Slight preload } \\ \text { Z1 } \end{gathered}$ | $\begin{array}{\|c} \hline \text { Medium preload } \\ Z 3 \end{array}$ |
|  | LH20 AN,EL,FL | $\begin{aligned} & 147 \\ & {[15]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 835 \\ {[85]} \\ \hline \end{array}$ | $\begin{aligned} & 186 \\ & {[19]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 335 \\ {[34]} \\ \hline \end{array}$ | $\begin{aligned} & 137 \\ & {[14]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 245 \\ {[25]} \\ \hline \end{array}$ |
|  | LH25 AN,EL,FL | $\begin{aligned} & 196 \\ & {[20]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1270 \\ & {[130]} \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \end{aligned}$ | $\begin{aligned} & 380 \\ & {[39]} \end{aligned}$ | $\begin{aligned} & 147 \\ & {[15]} \end{aligned}$ | $\begin{array}{r} 284 \\ \text { [29] } \\ \hline \end{array}$ |
|  | LH30 AN | $\begin{array}{r} 245 \\ {[25]} \end{array}$ | $\begin{aligned} & 1570 \\ & {[160]} \end{aligned}$ | $\begin{aligned} & 216 \\ & \text { [22] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 400 \\ & {[41]} \end{aligned}$ | $\begin{aligned} & 157 \\ & {[16]} \end{aligned}$ | $\begin{array}{r} 294 \\ \text { [30] } \\ \hline \end{array}$ |
|  | LH30 EL,FL | $\begin{aligned} & 294 \\ & \text { [30] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 1770 \\ & \text { [180] } \end{aligned}$ | $\begin{aligned} & 265 \\ & {[27]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 480 \\ \text { [49] } \\ \hline \end{array}$ | $\begin{aligned} & 186 \\ & \text { [19] } \end{aligned}$ | $\begin{array}{r} 355 \\ \text { [36] } \\ \hline \end{array}$ |
|  | LH35 AN,EL,FL | $\begin{aligned} & 390 \\ & {[40]} \end{aligned}$ | $\begin{aligned} & 2350 \\ & \text { [240] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 305 \\ & \text { [31] } \end{aligned}$ | $\begin{array}{r} 560 \\ \text { [57] } \end{array}$ | $\begin{aligned} & 216 \\ & \text { [22] } \end{aligned}$ | $\begin{array}{r} 390 \\ {[40]} \end{array}$ |
|  | LH45 AN,EL,FL | $\begin{aligned} & 635 \\ & {[65]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 3900 \\ & {[400]} \end{aligned}$ | $\begin{array}{r} 400 \\ {[41]} \end{array}$ | $\begin{array}{r} 745 \\ {[76]} \\ \hline \end{array}$ | $\begin{aligned} & 284 \\ & \text { [29] } \\ & \hline \end{aligned}$ | $\begin{array}{r} 540 \\ \text { [55] } \\ \hline \end{array}$ |
|  | LH55 AN,EL,FL | $\begin{gathered} 980 \\ {[100]} \end{gathered}$ | $\begin{aligned} & 5900 \\ & {[600]} \end{aligned}$ | $\begin{aligned} & 490 \\ & \text { [50] } \end{aligned}$ | $\begin{aligned} & 910 \\ & \text { [93] } \end{aligned}$ | $\begin{array}{r} 345 \\ \text { [35] } \end{array}$ | $\begin{array}{r} 645 \\ \text { [66] } \end{array}$ |
|  | LH65 AN,EL,FL | $\begin{aligned} & 1470 \\ & {[150]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8900 \\ & \text { [910] } \\ & \hline \end{aligned}$ | $\begin{array}{r} 580 \\ \text { [59] } \\ \hline \end{array}$ | $\begin{aligned} & 1070 \\ & {[109]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 400 \\ & {[41]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 755 \\ {[77]} \\ \hline \end{array}$ |
|  | LH20 BN,GL, HL | $\begin{array}{r} 196 \\ {[20]} \\ \hline \end{array}$ | $\begin{aligned} & 1080 \\ & {[110]} \end{aligned}$ | $\begin{aligned} & 265 \\ & \text { [27] } \end{aligned}$ | $\begin{aligned} & 480 \\ & \text { [49] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 196 \\ & {[20]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 355 \\ & {[36]} \\ & \hline \end{aligned}$ |
|  | LH25 BN,GL, HL | $\begin{aligned} & 245 \\ & {[25]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1570 \\ & {[160]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 294 \\ & \text { [30] } \\ & \hline \end{aligned}$ | $\begin{array}{r} 560 \\ \text { [57] } \\ \hline \end{array}$ | $\begin{aligned} & 216 \\ & \text { [22] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 400 \\ & {[41]} \\ & \hline \end{aligned}$ |
|  | LH30 BN,GL,HL | $\begin{aligned} & 390 \\ & {[40]} \end{aligned}$ | $\begin{aligned} & 2260 \\ & {[230]} \end{aligned}$ | $\begin{array}{r} 360 \\ \text { [37] } \end{array}$ | $\begin{aligned} & 665 \\ & {[68]} \end{aligned}$ | $\begin{aligned} & 265 \\ & \text { [27] } \end{aligned}$ | $\begin{aligned} & 480 \\ & \text { [49] } \end{aligned}$ |
|  | LH35 BN,GL,HL | $\begin{aligned} & 490 \\ & {[50]} \end{aligned}$ | $\begin{gathered} 2940 \\ {[300]} \end{gathered}$ | $\begin{aligned} & 430 \\ & {[44]} \end{aligned}$ | $\begin{aligned} & 795 \\ & \text { [81] } \end{aligned}$ | $\begin{aligned} & 305 \\ & {[31]} \end{aligned}$ | $\begin{aligned} & 570 \\ & {[58]} \end{aligned}$ |
|  | LH45 BN,GL, HL | $\begin{array}{r} 785 \\ {[80]} \\ \hline \end{array}$ | $\begin{aligned} & 4800 \\ & {[490]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 520 \\ \text { [53] } \\ \hline \end{array}$ | $\begin{array}{r} 960 \\ {[98]} \\ \hline \end{array}$ | $\begin{array}{r} 370 \\ {[38]} \\ \hline \end{array}$ | $\begin{array}{r} 695 \\ {[71]} \\ \hline \end{array}$ |
|  | LH55 BN,GL,HL | $\begin{aligned} & 1180 \\ & {[120]} \end{aligned}$ | $\begin{aligned} & 7050 \\ & {[720]} \end{aligned}$ | $\begin{aligned} & 635 \\ & {[65]} \end{aligned}$ | $\begin{aligned} & 1170 \\ & {[119]} \end{aligned}$ | $\begin{aligned} & 440 \\ & {[45]} \end{aligned}$ | $\begin{aligned} & 835 \\ & {[85]} \end{aligned}$ |
|  | LH65 BN,GL,HL | $\begin{aligned} & 1860 \\ & {[190]} \end{aligned}$ | $\begin{aligned} & 11300 \\ & {[1150]} \end{aligned}$ | $\begin{aligned} & 805 \\ & \text { [82] } \end{aligned}$ | $\begin{aligned} & 1480 \\ & {[151]} \end{aligned}$ | $\begin{array}{r} 550 \\ \text { [56] } \end{array}$ | $\begin{aligned} & 1040 \\ & \text { [106] } \end{aligned}$ |
|  | LH85 BN,GL,HL | $\begin{aligned} & 2840 \\ & \text { [290] } \end{aligned}$ | $\begin{aligned} & 16800 \\ & {[1710]} \end{aligned}$ | $\begin{aligned} & 1020 \\ & {[104]} \end{aligned}$ | $\begin{aligned} & 1870 \\ & \text { [191] } \end{aligned}$ | $\begin{aligned} & 695 \\ & {[71]} \end{aligned}$ | $\begin{aligned} & 1300 \\ & \text { [133] } \end{aligned}$ |

Clearance for fine clearance $Z 0$ is $0 \sim 3 \mu \mathrm{~m}$. Therefore, preload is zero.

## LH Series (interchangeable type)

Table II- $2 \cdot 2$ shows clearance and preload of interchangeable in LH Series.
Table II-2•2 Clearance and preload of interchangeable type in LH Series

Unit: $\mu \mathrm{m}$

| Model No. | Fine clearance | Slight preload |
| :---: | :---: | :---: |
|  | ZT | ZZ |
| LH20 | $-5 \sim 15$ | -5~0 |
| LH25 |  | -5~0 |
| LH30 |  | -7~0 |
| LH35 |  | $-7 \sim 0$ |
| LH45 |  | -7~0 |
| LH55 |  | -9~0 |
| LH65 |  | -9~0 |

Negative sign indicates preload volume.

## LS Series (Preloaded assembly)

Table II- $2 \cdot 3$ shows preload and rigidity o of LS Series.
Table II-2•3 Preload and rigidity of preloaded assembly in LS Series

|  | Model No. | Preload <br> N [kgf] |  | Rigidity $\mathrm{N} / \mu \mathrm{m}[\mathrm{kgf} / \mu \mathrm{m}]$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Vertical directions |  | Lateral direction |  |
|  |  | $\begin{gathered} \hline \text { Slight preload } \\ \text { Z1 } \end{gathered}$ | $\begin{array}{\|c} \hline \text { Medium preload } \\ Z 3 \end{array}$ | $\begin{array}{\|c} \hline \begin{array}{c} \text { Slight preload } \\ \text { Z1 } \end{array} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \text { M edium preload } \\ \text { Z3 } \end{array}$ | Slight preload Z1 | Medium preload Z3 |
| $\begin{aligned} & 0 \\ & 0 \\ & \frac{0}{7} \\ & \frac{0}{0} \\ & \frac{0}{5} \\ & \hline \bar{i} \end{aligned}$ | LS15 AL,EL,FL | $\begin{gathered} 69 \\ {[7]} \end{gathered}$ | $\begin{array}{r} 390 \\ {[40]} \\ \hline \end{array}$ | $\begin{aligned} & 127 \\ & {[13]} \end{aligned}$ | $\begin{array}{r} 226 \\ {[23]} \\ \hline \end{array}$ | $\begin{aligned} & 88 \\ & {[9]} \end{aligned}$ | $\begin{aligned} & 167 \\ & {[17]} \\ & \hline \end{aligned}$ |
|  | LS20 AL,EL,FL | $\begin{aligned} & 88 \\ & {[9]} \end{aligned}$ | $\begin{aligned} & 540 \\ & \text { [55] } \end{aligned}$ | $\begin{aligned} & 147 \\ & {[15]} \end{aligned}$ | $\begin{aligned} & 284 \\ & \text { [29] } \end{aligned}$ | $\begin{aligned} & 108 \\ & \text { [11] } \end{aligned}$ | $\begin{aligned} & 206 \\ & {[21]} \end{aligned}$ |
|  | LS25 AL,EL,FL | $\begin{aligned} & 147 \\ & {[15]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 880 \\ & {[90]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 206 \\ \text { [21] } \\ \hline \end{array}$ | $\begin{array}{r} 370 \\ \text { [38] } \\ \hline \end{array}$ | $\begin{aligned} & 147 \\ & {[15]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 275 \\ & {[28]} \\ & \hline \end{aligned}$ |
|  | LS30 AL,EL,FL | $\begin{aligned} & 245 \\ & \text { [25] } \end{aligned}$ | $\begin{aligned} & 1370 \\ & {[140]} \end{aligned}$ | $\begin{aligned} & 255 \\ & {[26]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 460 \\ \text { [47] } \\ \hline \end{array}$ | $\begin{aligned} & 186 \\ & {[19]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 345 \\ & \text { [35] } \end{aligned}$ |
|  | LS35 AL,EL,FL | $\begin{array}{r} 345 \\ \text { [35] } \\ \hline \end{array}$ | $\begin{aligned} & 1960 \\ & {[200]} \end{aligned}$ | $\begin{array}{r} 305 \\ {[31]} \\ \hline \end{array}$ | $\begin{array}{r} 550 \\ {[56]} \\ \hline \end{array}$ | $\begin{array}{r} 216 \\ \text { [22] } \\ \hline \end{array}$ | $\begin{array}{r} 400 \\ \text { [41] } \\ \hline \end{array}$ |
|  | LS15 CL,J L,KL | $\begin{aligned} & 49 \\ & {[5]} \end{aligned}$ | $\begin{aligned} & 294 \\ & {[30]} \\ & \hline \end{aligned}$ | $\begin{gathered} 78 \\ \text { [8] } \end{gathered}$ | $\begin{aligned} & 147 \\ & {[15]} \end{aligned}$ | $\begin{aligned} & 59 \\ & {[6]} \end{aligned}$ | $\begin{aligned} & 108 \\ & {[11]} \end{aligned}$ |
|  | LS20 CL,J L,KL | $\begin{aligned} & 69 \\ & \text { [7] } \\ & \hline \end{aligned}$ | $\begin{array}{r} 390 \\ {[40]} \\ \hline \end{array}$ | $\begin{array}{r} 108 \\ \text { [11] } \\ \hline \end{array}$ | $\begin{array}{r} 186 \\ \text { [19] } \\ \hline \end{array}$ | $\begin{aligned} & 78 \\ & \text { [8] } \\ & \hline \end{aligned}$ | $\begin{array}{r} 137 \\ {[14]} \\ \hline \end{array}$ |
|  | LS25 CL,J L,KL | $\begin{gathered} 98 \\ {[10]} \end{gathered}$ | $\begin{aligned} & 635 \\ & {[65]} \end{aligned}$ | $\begin{aligned} & 127 \\ & {[13]} \end{aligned}$ | $\begin{aligned} & 235 \\ & {[24]} \\ & \hline \end{aligned}$ | $\begin{gathered} 88 \\ {[9]} \\ \hline \end{gathered}$ | $\begin{array}{r} 177 \\ {[18]} \\ \hline \end{array}$ |
|  | LS30 CL,J L,KL | $\begin{aligned} & 147 \\ & {[15]} \\ & \hline \end{aligned}$ | $\begin{gathered} 980 \\ {[100]} \\ \hline \end{gathered}$ | $\begin{array}{r} 147 \\ {[15]} \\ \hline \end{array}$ | $\begin{aligned} & 275 \\ & {[28]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 108 \\ & \text { [11] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 206 \\ & \text { [21] } \\ & \hline \end{aligned}$ |
|  | LS35 CL,J L,KL | $\begin{aligned} & 245 \\ & {[25]} \end{aligned}$ | $\begin{aligned} & 1370 \\ & {[140]} \end{aligned}$ | $\begin{aligned} & 186 \\ & {[19]} \end{aligned}$ | $\begin{aligned} & 335 \\ & {[34]} \end{aligned}$ | $\begin{aligned} & 137 \\ & {[14]} \end{aligned}$ | $\begin{aligned} & 245 \\ & {[25]} \end{aligned}$ |

Clearance for fine clearance ZO is $0 \sim 3 \mu \mathrm{~m}$. Therefore, preload is zero.
However, ZO of PN grade is $0 \sim 15 \mu \mathrm{~m}$.

## LS Series (Interchangeable type)

Table II-2•4 shows clearance of interchangeable type of LS Series.


| Model No. | Fine clearance | Slight preload |
| :---: | :---: | :---: |
|  | ZT | ZZ |
| LS15 | $-4 \sim 15$ | $-4 \sim 0$ |
| LS20 | $-4 \sim 15$ | $-4 \sim 0$ |
| LS25 | $-5 \sim 15$ | $-5 \sim 0$ |
| LS30 | $-5 \sim 15$ | $-5 \sim 0$ |
| LS35 | $-5 \sim 15$ | $-6 \sim 0$ |

Negative sign indicates preload volume.

## LA Series

Table II- $2 \cdot 5$ shows preload and rigidity of LA Series.
LA Series has two types of preload Z3 (medium preload) and Z4 (heavy preload).
Table II-25 Preload and rigidity of LA Series

|  | Model No. | Preload <br> N [kgf] |  | Rigidity $\mathrm{N} / \mu \mathrm{m}[\mathrm{kgf} / \mu \mathrm{m}]$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Medium preload Z3 | Heavy preload Z4 | $\begin{aligned} & \text { Medium preload } \\ & \text { Z3 } \end{aligned}$ | Heavy preload Z4 |
|  | LA30 AN, EL, FL | $\begin{array}{r} 2450 \\ {[250]} \\ \hline \end{array}$ | $\begin{aligned} & 3140 \\ & {[320]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 705 \\ {[72]} \\ \hline \end{array}$ | $\begin{array}{r} 835 \\ {[85]} \\ \hline \end{array}$ |
|  | LA35 AL, AN, EL, FL | $\begin{aligned} & 3450 \\ & {[350]} \end{aligned}$ | $\begin{aligned} & 4300 \\ & {[440]} \end{aligned}$ | $\begin{aligned} & 825 \\ & {[84]} \end{aligned}$ | $\begin{aligned} & 970 \\ & {[99]} \end{aligned}$ |
|  | LA45 AL, AN, EL, FL | $\begin{aligned} & 5050 \\ & {[515]} \end{aligned}$ | $\begin{aligned} & 6350 \\ & {[650]} \end{aligned}$ | $\begin{aligned} & 1100 \\ & {[112]} \end{aligned}$ | $\begin{aligned} & 1240 \\ & {[126]} \end{aligned}$ |
|  | LA55 AL, AN, EL, FL | $\begin{aligned} & 8100 \\ & {[825]} \end{aligned}$ | $\begin{aligned} & 10200 \\ & {[1040]} \end{aligned}$ | $\begin{aligned} & 1400 \\ & {[143]} \end{aligned}$ | $\begin{aligned} & 1540 \\ & {[157]} \end{aligned}$ |
|  | LA65 AN, EL, FL | $\begin{aligned} & 13800 \\ & {[1410]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 18800 \\ & {[1920]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1730 \\ & {[176]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 2030 \\ & {[207]} \end{aligned}$ |
|  | LA30 BN, GL, HL | $\begin{aligned} & 3250 \\ & {[330]} \end{aligned}$ | $\begin{aligned} & 4050 \\ & {[415]} \end{aligned}$ | $\begin{aligned} & 1000 \\ & {[102]} \end{aligned}$ | $\begin{aligned} & 1180 \\ & {[120]} \end{aligned}$ |
|  | LA35 BL, BN, GL, HL | $\begin{aligned} & 4450 \\ & {[455]} \end{aligned}$ | $\begin{aligned} & 5650 \\ & {[575]} \end{aligned}$ | $\begin{aligned} & 1200 \\ & {[122]} \end{aligned}$ | $\begin{aligned} & 1400 \\ & {[143]} \end{aligned}$ |
|  | LA45 BL, BN, GL, HL | $\begin{aligned} & 6150 \\ & {[630]} \end{aligned}$ | $\begin{aligned} & 7750 \\ & {[790]} \end{aligned}$ | $\begin{aligned} & 1450 \\ & {[148]} \end{aligned}$ | $\begin{aligned} & 1640 \\ & {[167]} \end{aligned}$ |
|  | LA55 BL, BN, GL, HL | $\begin{aligned} & 9550 \\ & \text { [975] } \end{aligned}$ | $\begin{aligned} & 12100 \\ & {[1230]} \end{aligned}$ | $\begin{aligned} & 1840 \\ & {[188]} \end{aligned}$ | $\begin{aligned} & 2020 \\ & {[206]} \\ & \hline \end{aligned}$ |
|  | LA65 BN, GL, HL | $\begin{aligned} & 18000 \\ & {[1840]} \end{aligned}$ | $\begin{aligned} & 24400 \\ & {[2490]} \end{aligned}$ | $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{aligned} & 2840 \\ & {[290]} \end{aligned}$ |

## LY Series

Table II $-2 \cdot 6$ shows preload and rigidity of LY Series.
Table II -26 Preload and rigidity of LY Series

|  | Model No. | Preload <br> N [kgf] |  |  |  | Rigidity $\mathrm{N} / \mu \mathrm{m}[\mathrm{kgf} / \mu \mathrm{m}]$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \hline \text { Slight preload } \\ \text { Z1 } \end{gathered}$ | Light preload <br> Z2 | $\begin{gathered} \text { Medium preload } \\ \text { Z3 } \end{gathered}$ | Heavy preload Z4 | Slight preload Z1 | Light preload Z2 | $\begin{gathered} \text { Medium preload } \\ \mathrm{Z3} \end{gathered}$ | Heavy preload Z4 |
|  | LY15 AL,AN,EL,FL | $\begin{gathered} 59 \\ {[6]} \\ \hline \end{gathered}$ | $\begin{array}{r} 147 \\ {[15]} \\ \hline \end{array}$ | $\begin{array}{r} 294 \\ {[30]} \\ \hline \end{array}$ |  | $\begin{array}{r} 98 \\ {[10]} \\ \hline \end{array}$ | $\begin{array}{r} 137 \\ {[14]} \\ \hline \end{array}$ | $\begin{array}{r} 167 \\ {[17]} \\ \hline \end{array}$ |  |
|  | LY20 AL, EL,FL | $\begin{gathered} 98 \\ {[10]} \end{gathered}$ | $\begin{aligned} & 245 \\ & {[25]} \end{aligned}$ | $\begin{aligned} & 490 \\ & {[50]} \end{aligned}$ |  | $\begin{aligned} & 127 \\ & \text { [13] } \end{aligned}$ | $\begin{aligned} & 167 \\ & {[17]} \end{aligned}$ | $\begin{aligned} & 216 \\ & \text { [22] } \end{aligned}$ |  |
|  | LY25 AL,AN,EL,FL | $\begin{array}{r} 147 \\ {[15]} \\ \hline \end{array}$ | $\begin{array}{r} 440 \\ \text { [45] } \\ \hline \end{array}$ | $\begin{array}{r} 835 \\ {[85]} \\ \hline \end{array}$ | $\begin{aligned} & 1180 \\ & {[120]} \end{aligned}$ | $\begin{aligned} & 167 \\ & {[17]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 284 \\ \text { [29] } \\ \hline \end{array}$ | $\begin{array}{r} 390 \\ {[40]} \\ \hline \end{array}$ | $\begin{array}{r} 460 \\ {[47]} \\ \hline \end{array}$ |
|  | LY30 AL,AN,EL,FL | $\begin{aligned} & 245 \\ & {[25]} \end{aligned}$ | $\begin{aligned} & 635 \\ & {[65]} \end{aligned}$ | $\begin{aligned} & 1270 \\ & {[130]} \end{aligned}$ | $\begin{aligned} & 1770 \\ & {[180]} \end{aligned}$ | $\begin{aligned} & 196 \\ & {[20]} \end{aligned}$ | $\begin{aligned} & 325 \\ & \text { [33] } \end{aligned}$ | $\begin{aligned} & 480 \\ & {[49]} \end{aligned}$ | $\begin{aligned} & 580 \\ & {[59]} \end{aligned}$ |
|  | LY35 AL,AN,EL,FL | $\begin{array}{r} 345 \\ \text { [35] } \\ \hline \end{array}$ | $\begin{aligned} & 880 \\ & {[90]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1770 \\ & {[180]} \end{aligned}$ | $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{array}{r} 245 \\ {[25]} \\ \hline \end{array}$ | $\begin{array}{r} 360 \\ \text { [37] } \\ \hline \end{array}$ | $\begin{array}{r} 580 \\ {[59]} \end{array}$ | $\begin{array}{r} 655 \\ {[67]} \\ \hline \end{array}$ |
|  | LY45 AL,AN,EL,FL | $\begin{aligned} & 490 \\ & {[50]} \end{aligned}$ | $\begin{aligned} & 1270 \\ & {[130]} \end{aligned}$ | $\begin{aligned} & 2550 \\ & {[260]} \end{aligned}$ | $\begin{aligned} & 3600 \\ & {[370]} \end{aligned}$ | $\begin{aligned} & 315 \\ & \text { [32] } \end{aligned}$ | $\begin{aligned} & 500 \\ & {[51]} \end{aligned}$ | $\begin{array}{r} 735 \\ {[75]} \\ \hline \end{array}$ | $\begin{aligned} & 860 \\ & \text { [88] } \end{aligned}$ |
|  | LY55 AL,AN,EL,FL | $\begin{aligned} & 785 \\ & {[80]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1960 \\ & {[200]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 3900 \\ & {[400]} \end{aligned}$ | $\begin{aligned} & 5600 \\ & {[570]} \end{aligned}$ | $\begin{array}{r} 370 \\ {[38]} \\ \hline \end{array}$ | $\begin{array}{r} 600 \\ {[61]} \\ \hline \end{array}$ | $\begin{aligned} & 880 \\ & {[90]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1020 \\ & {[104]} \end{aligned}$ |
|  | LY65 AN,EL,FL | $\begin{aligned} & 1670 \\ & {[170]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 4200 \\ & {[430]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8450 \\ & {[860]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 11800 \\ & {[1200]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 560 \\ & {[57]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 910 \\ & \text { [93] } \\ & \hline \end{aligned}$ | $\begin{aligned} & 1340 \\ & {[137]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1560 \\ & {[159]} \\ & \hline \end{aligned}$ |
|  | LY20 BL, GL,HL | $\begin{gathered} 98 \\ {[10]} \end{gathered}$ | $\begin{aligned} & 294 \\ & \text { [30] } \end{aligned}$ | $\begin{aligned} & 590 \\ & {[60]} \end{aligned}$ | - - | $\begin{aligned} & 147 \\ & \text { [15] } \end{aligned}$ | $\begin{aligned} & 216 \\ & \text { [22] } \end{aligned}$ | $\begin{aligned} & 275 \\ & {[28]} \end{aligned}$ |  |
|  | LY25 BL,BN,GL,HL | $\begin{array}{r} 196 \\ {[20]} \\ \hline \end{array}$ | $\begin{array}{r} 540 \\ {[55]} \\ \hline \end{array}$ | $\begin{aligned} & 1080 \\ & {[110]} \end{aligned}$ | $\begin{gathered} 1570 \\ {[160]} \end{gathered}$ | $\begin{array}{r} 226 \\ \text { [23] } \end{array}$ | $\begin{array}{r} 360 \\ \text { [37] } \\ \hline \end{array}$ | $\begin{array}{r} 540 \\ \text { [55] } \\ \hline \end{array}$ | $\begin{array}{r} 645 \\ {[66]} \\ \hline \end{array}$ |
|  | LY30 BL,BN,GL,HL | $\begin{aligned} & 294 \\ & {[30]} \end{aligned}$ | $\begin{aligned} & 785 \\ & {[80]} \end{aligned}$ | $\begin{aligned} & 1570 \\ & {[160]} \end{aligned}$ | $\begin{aligned} & 2160 \\ & {[220]} \end{aligned}$ | $\begin{aligned} & 245 \\ & {[25]} \end{aligned}$ | $\begin{array}{r} 400 \\ {[41]} \\ \hline \end{array}$ | $\begin{aligned} & 610 \\ & {[62]} \end{aligned}$ | $\begin{aligned} & 695 \\ & {[71]} \end{aligned}$ |
|  | LY35 BL,BN,GL,HL | $\begin{array}{r} 440 \\ \text { [45] } \end{array}$ | $\begin{aligned} & 1080 \\ & {[110]} \end{aligned}$ | $\begin{aligned} & 2160 \\ & {[220]} \end{aligned}$ | $\begin{aligned} & 2940 \\ & {[300]} \end{aligned}$ | $\begin{aligned} & 305 \\ & \text { [31] } \end{aligned}$ | $\begin{array}{r} 450 \\ {[46]} \\ \hline \end{array}$ | $\begin{aligned} & 685 \\ & {[70]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 805 \\ & {[82]} \\ & \hline \end{aligned}$ |
|  | LY45 BL,BN,GL,HL | $\begin{array}{r} 635 \\ {[65]} \\ \hline \end{array}$ | $\begin{aligned} & 1570 \\ & {[160]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 3150 \\ {[320]} \\ \hline \end{array}$ | $\begin{aligned} & 4400 \\ & {[450]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 400 \\ \text { [41] } \\ \hline \end{array}$ | $\begin{aligned} & 625 \\ & \text { [64] } \\ & \hline \end{aligned}$ | $\begin{array}{r} 940 \\ {[96]} \\ \hline \end{array}$ | $\begin{aligned} & 1100 \\ & {[112]} \\ & \hline \end{aligned}$ |
|  | LY55 BL,BN,GL,HL | $\begin{gathered} 980 \\ {[100]} \end{gathered}$ | $\begin{aligned} & 2450 \\ & {[250]} \end{aligned}$ | $\begin{aligned} & 5000 \\ & {[510]} \end{aligned}$ | $\begin{aligned} & 6950 \\ & {[710]} \end{aligned}$ | $\begin{aligned} & 470 \\ & {[48]} \end{aligned}$ | $\begin{aligned} & 755 \\ & {[77]} \end{aligned}$ | $\begin{aligned} & 1140 \\ & {[116]} \end{aligned}$ | $\begin{aligned} & 1340 \\ & {[137]} \end{aligned}$ |
|  | LY65 BN,GL,HL | $\begin{aligned} & 2260 \\ & {[230]} \end{aligned}$ | $\begin{aligned} & 5600 \\ & {[570]} \end{aligned}$ | $\begin{aligned} & 11300 \\ & {[1150]} \end{aligned}$ | $\begin{aligned} & 15700 \\ & {[1600]} \end{aligned}$ | $\begin{aligned} & 805 \\ & {[82]} \end{aligned}$ | $\begin{aligned} & 1280 \\ & {[131]} \end{aligned}$ | $\begin{aligned} & 1920 \\ & {[196]} \end{aligned}$ | $\begin{aligned} & 2230 \\ & {[227]} \end{aligned}$ |

Clearance for fine clearance ZO is $0 \sim 3 \mu \mathrm{~m}$. Therefore, preload is zero.

## LW Series (Preloaded assembly)

Table II- $2 \cdot 7$ shows preload and rigidity of preloaded assembly of LW Series.
Rigidities are for the median of the preload range.

Table II-2.7 Preload and rigidity of LW Series

| Model No. | Preload <br> $\mathrm{N}[\mathrm{kgf}]$ |  | Rigidity <br> $\mathrm{N} / \mu \mathrm{m}[\mathrm{kgf} / \mu \mathrm{m}]$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Slight preload | Medium preload | Slight preload | Medium preload |
|  | Z1 | Z3 | Z1 | Z3 |
| LW17 EL | $0 \sim 245$ | - | 156 | - |
|  | $0 \sim 25]$ | - | $[16]$ | - |
| LW27 EL | $[0 \sim 30]$ | - | 181 | - |
|  | $0 \sim 390$ | - | $[18]$ | - |
| LW35 EL | $0 \sim 40]$ | - | 226 | - |
|  | $[0 \sim 50]$ | - | $[23]$ | - |
| LW50 EL | $0 \sim 590$ | $[80]$ | $[30$ | 440 |
|  | $[0 \sim 60]$ | 1470 | $[150]$ | $[35]$ |

Clearance of fine clearance ZO is $0 \sim 3 \mu \mathrm{~m}$. Therefore, preload is zero.
However, ZO of PN Grade is $3 \sim 15 \mu \mathrm{~m}$.

## LW Series (Interchangeable type)

Table II-2•8 shows in LW Series.
Table II-2\& Clearance of interchangeable type in LW Series

Unit: $\mu \mathrm{m}$

| Model No. | Fine clearance |
| :---: | :---: |
|  | $\mathbf{Z T}$ |
| LW17 | $-3 \sim 15$ |
| LW21 | $-3 \sim 15$ |
| LW27 | $-4 \sim 15$ |
| LW35 | $-5 \sim 15$ |
| LW50 | $-5 \sim 15$ |

## LE Series (Preloaded assembly)

Table II-2•9 shows preload and rigidity of preloaded assembly of LE Series. Rigidities are for the median of the preload range.

Table II-209 Preload and rigidity of LE Series

|  | Model No. | Preload <br> N [kgf] | $\begin{gathered} \text { Rigidity } \\ \mathrm{N} / \mu \mathrm{m}[\mathrm{kgf} / \mu \mathrm{m}] \end{gathered}$ |
| :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { Slight preload } \\ \text { Z1 } \end{gathered}$ | $\begin{gathered} \text { Slight preload } \\ \text { Z1 } \end{gathered}$ |
|  | LE05 AL | $\begin{gathered} 0 \sim 22 \\ {[0 \sim 2.3]} \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ {[3.5]} \\ \hline \end{gathered}$ |
|  | LE07 TL | $\begin{gathered} 0 \sim 29 \\ {[0 \sim 3]} \end{gathered}$ | $\begin{gathered} 46 \\ {[4.5]} \\ \hline \end{gathered}$ |
|  | LE09 AL, TL LE09 AR,TR | $\begin{gathered} 0 \sim 37 \\ {[0 \sim 3.8]} \end{gathered}$ | $\begin{aligned} & 61 \\ & {[6]} \end{aligned}$ |
|  | LE12 AL LE12 AR | $\begin{gathered} 0 \sim 40 \\ {[0 \sim 4.1]} \end{gathered}$ | $\begin{gathered} 63 \\ {[6.5]} \\ \hline \end{gathered}$ |
|  | LE15 AL,AR | $\begin{gathered} 0 \sim 49 \\ {[0 \sim 5]} \end{gathered}$ | $\begin{gathered} 66 \\ {[6.5]} \\ \hline \end{gathered}$ |
|  | LE05 CL | $\begin{gathered} 0 \sim 19 \\ {[0 \sim 1.9]} \end{gathered}$ | $\begin{aligned} & 29 \\ & \text { [3] } \\ & \hline \end{aligned}$ |
|  | LE07 SL | $\begin{gathered} 0 \sim 20 \\ {[0 \sim 2]} \\ \hline \end{gathered}$ | $\begin{aligned} & 28 \\ & \text { [3] } \end{aligned}$ |
|  | LE09 CL,SL | $\begin{gathered} 0 \sim 20 \\ {[0 \sim 2]} \\ \hline \end{gathered}$ | $\begin{gathered} 33 \\ {[3.5]} \\ \hline \end{gathered}$ |
|  | LE12 CL | $\begin{gathered} 0 \sim 23 \\ {[0 \sim 2.3]} \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ {[3.5]} \\ \hline \end{gathered}$ |
|  | LE15 CL | $0 \sim 29$ | $\begin{gathered} 44 \\ {[4.5]} \end{gathered}$ |
|  | LE07 UL | $\begin{gathered} 0 \sim 43 \\ {[0 \sim 4.4]} \\ \hline \end{gathered}$ | $\begin{aligned} & 71 \\ & {[7]} \end{aligned}$ |
|  | LE09 BL,UL | $\begin{gathered} 0 \sim 49 \\ {[0 \sim 5]} \end{gathered}$ | $\begin{aligned} & 17 \\ & \hline 86 \\ & {[9]} \end{aligned}$ |
|  | LE12 BL | $\begin{gathered} 0 \sim 59 \\ {[0 \sim 6]} \\ \hline \end{gathered}$ | $\begin{gathered} 97 \\ {[10]} \\ \hline \end{gathered}$ |
|  | LE15 BL | $\begin{aligned} & 0 \sim 78 \\ & {[0 \sim 8]} \end{aligned}$ | ${ }^{114}$ [12] |

Clearance of fine clearance ZO is $0 \sim 3 \mu \mathrm{~m}$. Therefore, preload is zero.
However, ZO of PN grade is $3 \sim 10 \mu \mathrm{~m}$.

## LE Series (Interchangeable type)

Table II- $2 \cdot 10$ shows clearance of interchangeable type of LE Series.
Table II-2-10 Clearance of interchangeable type of LE Series

Unit: $\mu \mathrm{m}$

| Model No. | Fine clearance |
| :---: | :---: |
|  | $\mathbf{Z T}$ |
| LE09 | $0 \sim 15$ |
| LE12 |  |
| LE15 |  |

## LU Series (Preloaded assembly)

Table II-2•11 shows preload and rigidity of preloaded assembly of LU Series. Rigidities are for the median of the preload range.

Table II-2•11 Preload and rigidity of LU Series

|  | Model No. | Preload <br> N [kgf] | Rigidity $\mathrm{N} / \mu \mathrm{m}[\mathrm{kgf} / \mu \mathrm{m}]$ |
| :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Slight preload } \\ & \text { Z1 } \end{aligned}$ | $\begin{aligned} & \text { Slight preload } \\ & \text { Z1 } \end{aligned}$ |
| $\begin{aligned} & \mathbb{O} \\ & \stackrel{\rightharpoonup}{\lambda} \\ & \stackrel{0}{0} \\ & \frac{0}{C} \\ & \frac{\bar{O}}{\bar{I}} \end{aligned}$ | LU05 TL | $\begin{gathered} 0 \sim 3.5 \\ {[0 \sim 0.34]} \end{gathered}$ | $\begin{gathered} 15 \\ {[1.5]} \end{gathered}$ |
|  | LU07 AL | $\begin{gathered} 0 \sim 8 \\ {[0 \sim 0.8]} \end{gathered}$ | $\begin{aligned} & 22 \\ & {[2]} \\ & \hline \end{aligned}$ |
|  | LU09 AL, TL | $\begin{gathered} 0 \sim 12 \\ {[0 \sim 1.2]} \end{gathered}$ | $\begin{gathered} 26 \\ {[2.5]} \end{gathered}$ |
|  | LU09 AR,TR | $\begin{gathered} 0 \sim 10 \\ {[0 \sim 1.0]} \end{gathered}$ | $\begin{gathered} 30 \\ {[3.5]} \end{gathered}$ |
|  | LU12 AL,TL | $\begin{gathered} 0 \sim 17 \\ {[0 \sim 1.7]} \end{gathered}$ | $\begin{gathered} 33 \\ {[3.5]} \end{gathered}$ |
|  | LU12 AR,TR | $\begin{gathered} 0 \sim 17 \\ {[0 \sim 1.7]} \end{gathered}$ | $\begin{gathered} 33 \\ {[3.5]} \end{gathered}$ |
|  | LU15 AL | $\begin{gathered} 0 \sim 33 \\ {[0 \sim 3.4]} \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ {[4.5]} \\ \hline \end{gathered}$ |
|  | LU09 BL,UL | $\begin{gathered} 0 \sim 17 \\ {[0 \sim 1.7]} \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ {[4.5]} \\ \hline \end{gathered}$ |
|  | LU12 BL,UL | $\begin{gathered} 0 \sim 25 \\ {[0 \sim 2.5]} \end{gathered}$ | $\begin{gathered} 52 \\ {[5]} \end{gathered}$ |
|  | LU15 BL | $\begin{gathered} 0 \sim 51 \\ {[0 \sim 5.2]} \end{gathered}$ | $\begin{gathered} 75 \\ {[7.5]} \end{gathered}$ |

Clearance of fine clearance $Z 0$ is $0 \sim 3 \mu \mathrm{~m}$. Therefore, preload is zero.
However, ZO of PN grade is $3 \sim 10 \mu \mathrm{~m}$.

## LU Series (Interchangeable type)

Table II-2•12 shows clearance of interchangeable type of LU Series
Table II -2•12 Clearance of interchangeable type of LU Series

Unit: $\mu \mathrm{m}$

| Model No. | Fine clearance |
| :---: | :---: |
|  | $\mathbf{Z T}$ |
| LU09 |  |
| LU12 | $0 \sim 15$ |
| LU15 |  |

## LL Series

Table II- $2 \cdot 13$ shows clearance of LL Series
Table II-2•13 Radial clearance
Unit: $\mu \mathrm{m}$

| Model No. | Clearance |
| :---: | :---: |
| LL15 | $0 \sim 10$ |

$\square$

## A-II-2.3 Calculating Friction Force by Preload

- Dynamic friction force per one ball slide of the linear guide can be calculated from preload vlue.
- The followings is a simple calculation to obtain the criterion of dynamic friction force.
For slight preload ZZ of interchangeable type with preload, use preload volume of slight preload Z1 of preloaded assembly.
$F=i P$
F: Dynamic friction force( $\mathbf{N}$ )
P: Preload ( N )
i: Contact coefficient

Use the following contact coefficient values (i).
LH/LS, LW Series: 0.004
LA Series : 0.012
LY, LE, LU Series : 0.026
-The starting friction force when the ball slide begins to move depends on lubrication condition. Roughly estimate it at 1.5 to 2 times of the dynamic friction obtained by the above method.

## Calculation example

In case of LH35AN - Z3

$$
\begin{aligned}
i & =0.004 \\
P & =2350(\mathrm{~N})(\text { from Table II-2•1) } \\
F & =i P \\
& =0.004 \times 2350=9.4(\mathrm{~N})
\end{aligned}
$$

Therefore, the criteria of the dynamic friction force of LH35AN - Z3 is 9.4 N .
For seal friction, refer to "A-II-5 Dust Proof of Linear

## Guide."

## A-II-3 Rating Life

## A-II-3.1 Rating Life and Basic Load Rating

## (1) Life

Although used in appropriate conditions, the linear guide deteriorates after a certain period of operation, and eventually becomes unusable. In broad definition, the period until the linear guide becomes unusable is called "life." There are "fatigue life " caused by flaking, and "life of accuracy deterioration" which is caused by wear.

## (2) Rating fatigue life

When the linear guide runs under load, the balls and the rolling contact surface of the grooves are exposed to repetitive load. This brings about fatigue to the material, and generates flaking. Flaking is scale-like damage to the surface of the ball groove.
Total running distance until first appearance of flaking is called "fatigue life." This is "life" in the narrow sense. Fatigue life varies significantly even in linear guides produced in the same lot, and even when they are operated under the same conditions. This is attributable to the inherent variation of the fatigue of the material itself.
"Rating fatigue life" is the total running distance which allows $90 \%$ of the group of linear guides of the same reference number to run without causing flaking when they are independently run under the same conditions. Rating fatigue life is sometimes indicated by total operating hours when the linear guides run at a certain speed.

## (3) Basic dynamic load rating

- Basic dynamic load rating, which indicates load carrying capacity of the linear guide, is a load whose direction and volume do not change, and which furnishes 50 km of rating fatigue life.
- In case of linear guide, it is a constant load applied to downward direction to the center of the ball slide.
- Value of basic dynamic load rating C is shown in
"Selection Guide to Linear Guides A-I-5 Model Number and Dimension Table."


## (4) Calculation of rating fatigue life

In general, rating fatigue life "L" can be calculated from basic dynamic load rating "C" and the load "F" to ball slide using the following formula.
For balls as rolling element $L=50 \times\left(\frac{C}{F}\right)^{3}$
For rollers as rolling element $L=50 \times\left(\frac{C}{F}\right)^{\frac{10}{3}}$
L: Rating fatigue life (km)
C: Basic dynamic load rating (N)
F: Load to a ball slide (N)
(dynamic equivalent load)

## (5) Dynamic equivalent load

- Load applied to the linear guide (ball slide load) comes from various directions up/down and right/left directions and/or as moment load. Sometimes more than one type of load is applied simultaneously. Sometimes volume and direction of the load may change.
Varying load cannot be used as it is to calculate life of linear guide. Therefore, it is necessary to use a hypothetical load to ball slide with a constant volume which would generate a value equivalent to an actual fatigue life. This is called "dynamic equivalent load." For actual calculation, refer to "A-II-3.2 (4) How to calculate dynamic equivalent load."


## (6) Basic static load rating

- When an excessive load or a momentary large impact is applied to the linear guide, local permanent deformation takes place to the balls and 128 to the rolling contact surface. After exceeding a certain level, the deformation hampers smooth linear guide operation.
- Basic static load rating is a static load when: [Permanent deformation of the balls] + [permanent deformation of the rolling contact surfaces] becomes 0.0001 times of the ball diameter.
- In case of linear guide, it is a load which is applied downward direction to the center of the ball slide.
- Values of basic static load rating C0 are shown in "Selection Guide to Linear Guide A-I-5 Model Number and Dimension Table."


## (7) Basic static moment load rating

- Generally, NSK linear guide uses a set of two rails and four ball slides for the guide way of one axis. Under some operating condition, static moment load should be taken into account.
"M0," which is the limit of static moment load in such use is shown in "Selection Guide to Linear Guide A-I-5 Model Number and Dimension Table."


## A-II-3.2 How to Calculate Life

## (1) Flow chart to calculate life



Set operating conditions such as volume of load to the linear guide, installation method, set up of axes, number of ball slide, etc.

Calculating load which applies to each bearing Refer to Section (3) Page A130

Calculate up/down, right/left direction loads and moment load of the linear guide.

Calculating dynamic equivalent load Refer to Section (4)

Calculate dynamic equivalent load based on the load from each direction which are applied to each linear guide.

Calculating mean effective load Refer to Section (5)............................................................................. 136

Calculate mean effective load based on the dynamic equivalent load which changes by the stroke position.


Confirm that static load is within permissible range.

Completion

## (2) Setting operating condition of linear guide

- First, set operating conditions to determine whether the temporarily selected model satisfies the required life.
- Major operating conditions are as follows. Set all values to calculate applied loads to each ball slide (Refer to Table II-3•1).

| Axis set up | : Horizontal, vertical <br> Rail combination <br>  <br> Applying loads <br> rail |
| :--- | :--- |
| Ball slide span | $: F_{x}, F_{y}$ and $F_{z}(\mathrm{~N})$ |
| Rail span | $: I(\mathrm{~mm})$ |
| Point of load action point | $: L(\mathrm{~mm})$ |
| Center of driving mechanism | $: X, Y, Z(\mathrm{~mm})$ |
| Operating speed | $: X_{b}, Y_{b}, Z_{b}(\mathrm{~mm})$ |
| Time in acceleration | $: t(\mathrm{~mm} / \mathrm{sec})$ |
| Operating frequency (duty cycle) |  |

## (3) Calculating load to a ball slide

-Table II-31 shows a formula to calculate loads that are going to be applied to each assembled ball slide into a machine.
The Table shows six typical patterns of linear guide installing structure.

- In the Tables, directions indicated by arrows denote "plus" for the applied loads ( $F_{x}, F_{y}, F_{z}$ ) and the loads which is applied to the ball slide. ( $F_{\mathrm{r}}, F_{\mathrm{s}}, M_{\mathrm{r}}, M_{\mathrm{p}}, M_{\mathrm{y}}$ ).
- Codes in the Tables are as follows:
$\mathrm{Fr}_{\mathrm{r}}$ : Vertical loads to the ball slide (N)
$F_{s}$ : Lateral loads to the ball slide ( N )
$M_{r}$ : Rolling moment to the ball slide ( $\mathrm{N} \cdot \mathrm{mm}$ )


Fig. II-302
$M_{\mathrm{p}}$ : Pitching moment the ball slide ( $\mathrm{N} \cdot \mathrm{mm}$ )
$M_{y}$ : Yawing moment the ball slide $(\mathrm{N} \cdot \mathrm{mm})$
Suffixes ( $1,2, \ldots$ ) to the above $F_{r} \sim M_{y}$ : Ball slide number
$F_{\text {xi }}$ : Load applied in $X$ direction ( $\mathrm{i}=1 \sim \mathrm{n}$; n is the number of loads applied in $X$ direction) (N)
$F_{\mathrm{yj}}$ : Load applied in $Y$ direction ( $\mathrm{j}=1 \sim \mathrm{n}$; n is the number of loads applied in $Y$ direction) ( N )
$F_{\text {zk }}$ : Load applied in $Z$ direction ( $k=1 \sim n ; n$ is the number of loads applied in $Z$ direction) (N)
Coordinates ( $X_{\mathrm{xi}}, Y_{\mathrm{xi}}, Z_{\mathrm{xx}}$ ): Point where load $F_{\mathrm{xi}}(\mathrm{mm})$ is applied.
Coordinates ( $X_{y j}, Y_{y j}, Z_{j j}$ ): Point where load $F_{y j}(\mathrm{~mm})$ is applied.
Coordinates ( $X_{z k}, Y_{z k}, Z_{z k}$ ): Point where load $F_{z k}(\mathrm{~mm})$ is applied.
I: Ball slide span (mm)
L: Rail span (mm)
Coordinates ( $X_{\mathrm{b}}, Y_{\mathrm{b}}, Z_{\mathrm{b}}$ ): Center of driving mechanism

Table II-3• Loads applied to the ball slides

| Pattem |
| :--- | :--- | :--- |



| Arrangement of ball slides |
| :---: | :---: | :---: |

## (4) Calculation of dynamic equivalent load

- For calculation of dynamic equivalent load, use the load in Table II-3•2 which matches the intended use of the linear guide.


Fig. II-3e3
Table II-302 Loads in the arrangement of linear guides

| Pattern | Arrangement of linear guide | Loads necessary to calculate dynamic equivalent load |  |  |  |  | Dynamic equivalent load |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Load |  | Moment load |  |  |  |
|  |  | Up/down (vertical) | Right/left (lateral) | Rolling | Pitching | Yawing |  |
| 1 |  | $F_{\mathrm{r}}$ | $F_{\text {s }}$ | $M_{\text {r }}$ | $M_{\text {p }}$ | $M_{y}$ |  |
| 2 |  | $F_{\mathrm{r}}$ | $F_{\text {s }}$ | $M_{r}$ |  |  | $\begin{aligned} & F_{\mathrm{re}}=\mathcal{E}_{\mathrm{r}} \cdot M_{\mathrm{r}} \\ & F_{\mathrm{pe}}=\mathcal{E}_{\mathrm{p}} \cdot M_{\mathrm{p}} \\ & F_{\mathrm{ye}}=\boldsymbol{\varepsilon}_{\mathrm{y}} \cdot M_{\mathrm{y}} \end{aligned}$ |
| 3 |  | $F_{\text {r }}$ | $F_{\text {s }}$ |  | $M_{\text {p }}$ | $M_{y}$ | $\alpha$ :Contact angle <br> LH, LS, LW Series $\alpha=50^{\circ}$ |
| 4 |  | $F_{\text {r }}$ | $F_{\text {s }}$ |  |  |  |  |

- Use dynamic equivalent coefficient $\varepsilon$ in the table below for easy conversion of moment load to dynamic equivalent load.
- Coefficient of each moment direction is as follows.
$\varepsilon_{r}$ : Rolling direction
$\varepsilon_{\mathrm{p}}$ : Pitching direction
$\varepsilon_{y}$ : Yawing direction

Table II-3•3 Dynamic equivalent coefficients
Unit:1/m

| Model number | $\varepsilon_{\mathrm{r}}$ | $\varepsilon_{\text {p }}$ | $\varepsilon_{\text {y }}$ | Model number | $\mathcal{E}_{\mathrm{r}}$ | $\mathcal{E}^{\text {p }}$ | $\varepsilon_{y}$ | Model number | $\mathcal{E}_{\text {r }}$ | $\mathcal{E}^{\text {p }}$ | $\varepsilon_{\text {y }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LH20 | 142 | 81 | 97 |  |  |  |  | LW17 | 66 | 125 | 149 |
| LH20L | 142 | 57 | 68 |  |  |  |  | LW21 | 59 | 108 | 129 |
| LH25 | 123 | 68 | 81 | LA30 | 105 | 63 | 63 | LW27 | 53 | 76 | 91 |
| LH25L | 123 | 51 | 61 | LA30L | 105 | 43 | 43 | LW35 | 32 | 51 | 61 |
| LH30A | 98 | 70 | 83 | LA35 | 84 | 54 | 54 | LW50 | 25 | 38 | 46 |
| LH30EF | 98 | 58 | 69 | LA35L | 84 | 37 | 37 |  |  |  |  |
| LH30L | 98 | 44 | 52 | LA45 | 60 | 41 | 41 | LE05 | 196 | 248 | 248 |
| LH35 | 78 | 51 | 61 | LA45L | 60 | 31 | 31 | LE05S | 196 | 323 | 323 |
| LH35L | 78 | 36 | 43 | LA55 | 51 | 33 | 33 | LE07 | 141 | 188 | 188 |
| LH45 | 60 | 38 | 45 | LA55L | 51 | 26 | 26 | LE07S | 141 | 349 | 349 |
| LH45L | 60 | 30 | 36 | LA65 | 43 | 29 | 29 | LE07L | 141 | 122 | 122 |
| LH55 | 51 | 31 | 37 | LA65L | 43 | 20 | 20 | LE09 | 123 | 149 | 149 |
| LH55L | 51 | 25 | 30 |  |  |  |  | LE09S | 123 | 277 | 277 |
| LH65 | 43 | 27 | 32 |  |  |  |  | LE09L | 123 | 102 | 102 |
| LH65L | 43 | 20 | 24 |  |  |  |  | LE12 | 90 | 125 | 125 |
| LH85L | 33 | 17 | 20 | LY15 | 133 | 111 | 111 | LE12S | 90 | 233 | 233 |
|  |  |  |  | LY20 | 100 | 89 | 89 | LE12L | 90 | 86 | 86 |
|  |  |  |  | LY20L | 100 | 65 | 65 | LE15 | 50 | 102 | 102 |
|  |  |  |  | LY25 | 90 | 75 | 75 | LE15S | 50 | 174 | 174 |
|  |  |  |  | LY25L | 90 | 51 | 51 | LE15L | 50 | 68 | 68 |
| LS15 | 177 | 116 | 138 | LY30 | 74 | 63 | 63 |  |  |  |  |
| LS15S | 177 | 174 | 208 | LY30L | 74 | 48 | 48 | LU05 | 385 | 359 | 359 |
| LS20 | 127 | 94 | 112 | LY35 | 61 | 54 | 54 | LU07 | 286 | 305 | 305 |
| LS20S | 127 | 136 | 162 | LY35L | 61 | 41 | 41 | LU09 | 217 | 242 | 242 |
| LS25 | 111 | 70 | 83 | LY45 | 46 | 41 | 41 | LU09L | 217 | 138 | 138 |
| LS25S | 111 | 108 | 129 | LY45L | 46 | 30 | 30 | LU09R | 217 | 203 | 203 |
| LS30 | 94 | 63 | 75 | LY55 | 39 | 35 | 35 | LU12 | 167 | 204 | 204 |
| LS30S | 94 | 102 | 121 | LY55L | 39 | 26 | 26 | LU12L | 167 | 116 | 116 |
| LS35 | 76 | 54 | 64 | LY65 | 33 | 31 | 31 | LU15 | 133 | 174 | 174 |
| LS35S | 76 | 87 | 104 | LY65L | 33 | 21 | 21 | LU15L | 133 | 94 | 94 |

Definitions of codes appearing at the end of the model number in Table II-3•3:

| L | : Super-high load type | LH45L |
| :--- | :--- | :--- |
| $S$ | : Medium load type | LS25S |
| No code | : High load type | LY45_- |
| $A$ | : Ball slide shape is square | LH30A (only LH30) |
| $E F$ | : Ball slide shape is flanged type | LH30EF (only LH30) |
| $R$ | : Miniature Series with ball retainer | LU09 |

- Formula is determined by the relationship of loads in terms of volume. Full dynamic equivalent load can be easily obtained by using each coefficient.
After obtaining the dynamic equivalent load of the necessary load directions from Table II-3•3, use the formulas below to calculate full dynamic equivalent loads.
- When $F r$ is the largest load: $F e=F r+0.5 F s e+0.5 F r e+0.5 F p e+0.5 F y e$
- When Fse is the largest load : $\mathrm{Fe}=0.5 \mathrm{Fr}+F$ se+0.5Fre+0.5Fpe+0.5Fye
- When Fre is the largest load : $\mathrm{Fe}=0.5 \mathrm{Fr}+0.5 F \mathrm{se}+F \mathrm{re}+0.5 \mathrm{Fpe}+0.5 F \mathrm{Fye}$
- When Fpe is the largest load : $F \mathrm{e}=0.5 \mathrm{Fr}+0.5 F \mathrm{se}+0.5 F \mathrm{re}+F \mathrm{pe}+0.5 F \mathrm{Fye}$
- When Fye is the largest load : $\mathrm{Fe}=0.5 \mathrm{Fr}+0.5 \mathrm{Fse}+0.5 \mathrm{Fr}++0.5 \mathrm{Fpe}+F \mathrm{Fye}$

For the values of each dynamic equivalent load in the formulas above, disregard load directions and take the absolute value.

## (5) Calculation of mean effective load

When the load to the ball slide deviates, obtain a mean effective load which becomes equal to the life of ball slide under variable load conditions. If the load does not vary, use the dynamic equivalent load as it is.
(1) When load and running distance vary by phase (Fig. II-34)


Fig. II -34 Variable load by phase
Running distance while dynamic equivalent load $F_{1}$ is applied: $L_{1}$
Running distance while dynamic equivalent load $F_{2}$ is applied: $L_{2}$
Running distance while dynamic equivalent load $F_{3}$ is applied: $L_{3}$
Running distancewhile dynamic equivalent load Fn is applied: Ln

From the above, mean effective load Fm can be obtained by the following formula.
$F m \sqrt[3]{\frac{1}{L}\left(F_{1}^{3} L_{1}+F_{2}^{3} L_{2}+\ldots \ldots .+F_{n}^{3} L_{n}\right)}$
$F \mathrm{~m}$ : Mean effective load of the deviating load ( N )
$L$ : Running distance ( $\Sigma L n$ )

## When load changes almost lineally (Fig. II-35)

Approximate mean effective load Fm can be obtained by the following formula.

$$
\begin{aligned}
& \text { Fm } \div \frac{1}{3}(\text { Fmin }+2 F m a x) \\
& \text { Fmin :Minimum value of dynamic } \\
& \quad \text { equivalent load (N) } \\
& \text { Fmax: Maximum value of dynamic } \\
& \quad \text { equivalent load (N) }
\end{aligned}
$$

(3) When load changes similar to a sine curve (Fig. I-36)
At time of (a): $F m=0.65$ Fmax
At time of (b): Fm $=0.75 \mathrm{Fmax}$

(a)



Fig. II-3*5 Simple variable load

## (2) Hardness coefficient

- For linear guides, in order to function optimally, both the balls and the rolling contact surface must have a hardness of HRC58 to 62 to an appropriate depth
- The hardness of NSK linear guide fully satisfies HRC58 to 62. Therefore, in most cases it is not necessary to consider hardness. If the linear guide is made of a special material by a customer's request, as the material hardness is lower than HRC58, use the following formula for adjustment.
$C_{H}=f_{H} \cdot C$
Сон $=\mathrm{f}_{\mathrm{H}}{ }^{\prime} \cdot \mathrm{C}_{\text {o }}$
$C_{H}$ : Basic dynamic load rating adjusted by hardness coefficient
$f_{H}$ : Hardness coefficient (Refer to Fig. II-3.7)
Сон : Basic static load rating adjusted by hardness coefficient
$f_{H^{\prime}}$ : Static hardness coefficient (Refer to Fig. II-3.7)


Fig. II-3.7 Hardness coefficient

## (3) Reliability coefficient

- In general, a reliability of $90 \%$ is customary. In this case, reliability coefficient is 1 . Therefore, the reliability coefficient does not have to be included in calculation.


## (7) Calculation of rating life

Life calculating formula in the stroke movement with normal lubrication, the following relationships exist between ball slide mean effective load $F m(N)$, basic dynamic load rating to load application direction $C$ $(\mathrm{N})$, and rating fatigue life $L(\mathrm{Km})$.

$$
L=50 \times\left(\frac{\boldsymbol{f}_{\mathrm{H}} \cdot \boldsymbol{C}}{\boldsymbol{f} \boldsymbol{w} \cdot \boldsymbol{F} \boldsymbol{m}}\right)^{\mathrm{n}}(\mathrm{Km})
$$

Ball linear guide bearing which uses balls $n=3$
Roller linear guide bearing which uses rollers $n=10 / 3$
$f_{H}$ : Hardness coefficient
$f$ : Load factor
Fm : Mean effective load
Use basic dynamic load rating $C$ to calculate the life.
Note: Do not use basic static load rating $C_{0}$, basic static moment rating $M_{\text {Ro, }} M_{\text {PO }}$ or Myo.

## Life as an entire guide way system

In those cases when several ball slides comprise a single guide way system (such as a single-axis table), the life of the ball slide to which the most strenuous condition is applied is considered to be the life of the entire system. For example, in Fig. II-3•8, if "Ball slide A" is the ball slide which receives the largest


Fig. II-38 Life of a system mean effective load, or if "Ball slide A" is the one which has the shortest life, the life of the system is considered to be the life of "Ball slide A."

## (8) Examination of static load

## (1) Examine from basic static load rating

- Examine static permissible load $P_{0}$, which is applied to the ball slide, from basic static load rating $C_{0}$ and static permissible load factor $f s$.

$$
P_{0}=\frac{C_{0}}{\boldsymbol{f}}
$$

When static equivalent load $P_{0}$ is a combination of vertical loads Fr and lateral load Fs, calculate using formulas below.

## For LH, LS, LW Series:

If compressed load and lateral load are combined $P_{0}=F r+1.59 F s$

If tensile load and lateral load are combined

$$
P_{0}=1.34 \mathrm{Fr}+1.59 \mathrm{Fs}
$$

## For LA, LY, LU, LE Series:

$$
P_{0}=F r+F s
$$

- The table below shows guidelines of fs for general industrial use.

Table II -35

| Use conditions | $f s$ |
| :---: | :---: |
| Under normal operating conditions | $1 \sim 2$ |
| Operating under vibration/impact | $1.5 \sim 3$ |

- Basic static load rating is not a destructive force to the balls, rails, or ball slide. The balls can withstand a load more than seven times larger than the basic static load rating . It is sufficient as a safety factor to the destruction load designed for general machines.
- However, when the linear guide is mounted upside down, the strength of the bolt which secures rail and ball slide affects the strength of the entire system. Strength of the bolt and its material should be considered.


## (2) Examining from static moment load rating

- Also examine static permissible load $M_{0}$ from basic static moment load $M_{\text {po }}$ and static permissible load factor $f s$.

$$
M_{0}=\frac{\boldsymbol{M}_{\mathrm{P}}}{\boldsymbol{f}_{5}}
$$

If more than one moment load in any direction is combined, please consult NSK.


Fig. II-399 Moment load directions

## (9) Precautions for the design in examining

 the lifeThe following points must be heeded in examining the life.


## In case of oscillating stroke

- If the balls do not rotate all the way, but only halfway, and if this minute stroke is repeated, lubricant disappears from the contact surface of balls and grooves. This generates "fretting," a premature wear. Fretting cannot be entirely prevented, but it can be mitigated.
- A grease which prevents fretting is recommended for oscillating stroke operations. Using a standard grease, life can be markedly prolonged by adding a normal stroke travel (about the ball slide length) once every several thousand cycles.


When applying pitching or yawing moment

- Load applied to the ball rows inside the ball slide is inconsistent if pitching or yawing moment load is applied. Loads are heavy on the balls on each end of the row.
- In such case, a heavy load lubricant grease or oil are recommended. Another countermeasure is using one size larger model of linear guide to reduce the load per ball.
- Moment load is insignificant for 2-rail, 4-ball slides combination which is commonly used.


When an extraordinary large load is applied during stroke

- If an extraordinary large load is applied at certain position of the stroke, calculate not only the life based on the mean effective load, but also the life based on the load in this range.



## When calculated life is extraordinarily short (Less than 3000 km in calculated life, or the load exceeds $10 \%$ of the basic dynamic load rating.)

- In such case, the contact pressure to the balls and the rolling contact surface is extraordinarily high.
- Operated under such state continually, the life is significantly affected by the loss of lubrication and the presence of dust, and the actual life becomes shorter than calculated.
- It is necessary to reconsider arrangement, the number of ball slide, and the type of model in order to reduce the load to the ball slide.


## A-II-4 Lubrication

- Refer to Page D13 for linear guide lubrication.


## A-II-4.3 Lubrication Accessories

## (1) Types of lubrication accessories

- Fig. $\mathbb{I}-4 \cdot 1$ and $\mathbb{I}-4 \cdot 2$ show linear guide grease fittings and tube fittings.
- For standard specifications, the grease fitting is installed at the end of the ball slide. It can be installed on the side of the ball slide as an option. Refer to Fig. II-4•3, Fig. II-4•4, and Table II-4•1.
- When using a piping accessory with M6 x1 screw, which is a piping standard screw, a connector is required to connect to the grease fitting hole on the ball slide, whose installation hole is $\mathrm{M} 6 \times 0.75$. The connector is available from NSK.

Table II-4•1 Location of the grease fitting

| Rail width code | Low type | Hightype | Tap | Depth |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $T_{2}$ | $T_{2}$ | $S$ | $L$ |  |
| 15 | 4.5 | 8.5 | $\mathrm{M} 6 \times 0.75$ | 8 |  |
| 20 | 5 | - | $\mathrm{M} 6 \times 0.75$ | 8 |  |
| 25 | 6 | 10 | $\mathrm{M} 6 \times 0.75$ | 8 |  |
| 30 | 7 | 10 | $\mathrm{M} 6 \times 0.75$ | 8 |  |
| 35 | 8 | 15 | $\mathrm{M} 6 \times 0.75$ | 8 |  |
| 45 | 10 | 20 | PS1/8 | 11 |  |
| 55 | 11 | 21 | PS1/8 | 11 |  |
| 65 | 19 | 19 | PS1/8 | 11 |  |
| Unit: |  |  |  |  |  |



Fig. II-44 Optional position in LY Series


Fig. II-4•1 Shapes of grease fitting


Fig. II-4•2 Linear guide tube fitting


Fig. II-4•3 Location of grease fitting

## (2) Changing assembly direction of the lubrication accessory

(1) Changing direction of the grease fitting or tube fitting
Follow the procedures below.
Remove the grease fitting with a spanner.
Wrap the fitting screw section with some sealing tape, flax yarn, or the like.
Put the grease fitting back into the opening, and tighten it. If the torque becomes too large before the grease fitting turns to the desired direction, pull it out. Adjust the thickness of sealing tape, flax yarn or the like, then try again.

Note: The component where the grease fitting is inserted is made of plastic. Excessive tightening of the grease fitting damages the plastic.
(2) Move the grease fitting to the other side of ball slide
Follow the procedures below.
Illustration at right: Using a spanner, remove the blind plug in the grease fitting installation hole on Face B.
Remove the grease fitting on Face A. Insert the grease fitting in the installation hole on Face $B$. Take the same steps as the above (1) for adjusting. Insert the blind plug in the grease fitting installation hole on Face A.

## (3) Switching the grease fitting to the side of ball slide

Consult NSK to install the grease fitting to the side of the end cap or the ball slide. This is optional service.


Fig. II-45 Grease fitting installation

## A-II-5 Dust Proof of Linear Guide

## A-II-5.1 Standard Specification

- To keep foreign matters from entering inside the ball slide, NSK linear guide has an end seal on both ends, and an bottom seal at the bottom.
- Table II-5•1 shows seals for standard specification for each series.

Table II-5^1 Standard seals

|  |  | End <br> seal | Bottom seal |
| :---: | :---: | :---: | :---: |
| LH Series |  | 0 | 0 |
| LS Series |  | 0 | 0 |
| LA Series |  | 0 | 0 |
| LY Series |  | 0 | 0 |
| LW Series |  | 0 | 0 |
| LE Series |  | 0 | $\Delta$ |
| LU | LU12,15 | 0 | $\Delta$ |
| Series | LU05,07,09 | $\Delta$ | - |

O: Installed as standard
$\Delta$ : Installed on request

- Seal friction per standard ball slide is shown in Table II-5•2.


Fig. II -5•1

Table II -502 Seal friction per ball slide (maximum value)
Unit: N

| Series | 15 | 20 | 25 | 30 | 35 | 45 | 55 | 65 | 85 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LH Series | - | 6 | 8 | 8 | 10 | 12 | 18 | 20 | 30 |
| LS Series | 4 | 6 | 8 | 8 | 10 | - | - | - | - |
| LA Series | - | - | - | 8 | 8 | 9 | 9 | 12 | - |
| LY Series | 2 | 2 | 3 | 8 | 10 | 12 | 12 | 13 | - |


| Series | 17 | 21 | 27 | 35 | 50 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LW Series | 6 | 8 | 12 | 16 | 20 |


| Series | 05 | 07 | 09 | 12 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LU Series | 0.3 | 0.3 | 0.5 | 0.5 | 0.5 |
| LE Series | - | 0.4 | 0.8 | 1.0 | 1.2 |

## A-II-5.2 NSK K1 Lubrication Unit

## (1) What is K1 Lubrication Unit

- This is a lubrication unit made of porous plastic (polyurethane) which contains a large volume of lubrication oil, and is formed into seal.
- K1 Lubrication Unit is not a simple dust prevention seal. This remarkable seal also serves as a lubrication unit by discharging oil from the plastic.
- Along with the protection plate, a K1 Lubrication Unit is installed between the end cap and the end seal at both ends of the linear guide (Fig. II-5•2). KI Lubrication Unit is already equipped at the time of delivery.


Fig. II-5•2

## (2) Functions of NSK K1 Lubrication Unit

This Unit is markedly effective as a lubrication oil cup and a highly functional seal in the following occasions.

- Use it when sealed lubricant runs out ........ For production line system (maintenance-free)
-When only a small amount of oil is allowed ... For clean facility, medical equipment
-When oil is washed away .................... For food processing machines
-When oil-absorbing dust is present ......... For woodworking machines

Refer to Page D23 for details.

## A-II-5.3 Dust proof components

NSK has the following items. Select a suitable type for the operating environment.

Table II-5^3 Optional dust proof components

| Name | Purpose |
| :---: | :--- |
| NSK K1 <br> lubrication unit | Made of plastic which contains oil. Enhances dust prevention and <br> lubricating functions. |
| Double seal | Combines two end seals, enhancing sealing function. |
| Protector | Prevents high-temperature, hard dusts from entering. |
| Rail cap | Prevents foreign matters such as swarf generated in cutting operation <br> from clogging the rail-mounting hole. |
| Inner seal | Installed inside the ball slide, and prevents foreign matters from entering <br> the rolling contact surface. |
| Bellows | Covers the linear guide and feed screw. |

## (1) Double seal

- A combination of two end seals to enhance seal function.
-When a double seal is installed, the end seal section becomes thicker than the standard item by the size shown in Table II-5•4. Take this thickness into consideration in determining the stroke and the size of section in which a ball slide is going to be installed.
- Double-seal set: Can be installed to a completed standard item later on request. It comprises two end seals, a collar, and a small screw for installation (Fig. II-5•4).
- Double-seal set for LY Series also has a spacer which is installed between end seals (Fig. II-5•5).
- For LA Series, double-seal set can be installed only before shipping from the factory.


Fig. II -53

Table II-54 Thickness of double-seal set (one side)
Unit: mm

| Model No. | Double-seal set <br> reference No. | Increased <br> thickness |
| :---: | :---: | :---: |
| LH20 | LH20WS-01 | 2.5 |
| LH25 | LH25WS-01 | 2.8 |
| LH30 | LH30WS-01 | 3.6 |
| LH35 | LH35WS-01 | 3.6 |
| LH45 | LH45WS-01 | 4.3 |
| LH55 | LH55WS-01 | 4.3 |
| LH65 | LH65WS-01 | 4.9 |
| LH85 | LH85WS-01 | 6.2 |
| LS15 | LS15WS-01 | 2.8 |
| LS20 | LS20WS-01 | 2.5 |
| LS25 | LS25WS-01 | 2.8 |
| LS30 | LS30WS-01 | 3.6 |
| LS35 | LS35WS-01 | 3.6 |


| Model No. | Double-seal set <br> reference No. | Increased <br> thickness ${ }_{2}$ |
| :---: | :---: | :---: |
| LY15 | LY15WS-01 | 3.3 |
| LY20 | LY20WS-01 | 3.3 |
| LY25 | LY25WS-01 | 5.3 |
| LY30 | LY30WS-02 $*$ | 6.0 |
| LY35 | LY35WS-03 $* *$ | 7.0 |
| LY45 | LY45WS-03 $* *$ | 8.0 |
| LY55 | LY55WS-02 $*$ | 8.0 |
| LY65 | LY65WS-03 $* *$ | 8.0 |
| LW17 | LW17WS-01 | 2.6 |
| LW21 | LW21WS-01 | 2.8 |
| LW27 | LW27WS-01 | 2.5 |
| LW35 | LW35WS-01 | 3.0 |
| LW50 | LW50WS-01 | 3.6 |

*) Can be used with a new type of seal. (seal flat type, installed on the stepped rail top face)
**) Can be used with a new type of seal. (seal flat type, flat top face)
Please consult NSK when installing an old type seal.


Fig. II -54

## (2) Protector

- A protector is usually installed outside the end seal to prevent high-temperature fine particles such as welding spatter and other hard foreign matters from entering the ball slide.
- Same as the case with a double seal, when a


Fig. II -5٪
protector is installed, the ball slide becomes longer by the size shown in Table II-5.5. Protector is available as a set.

- For LA Series, protector can be installed only before shipping from the factory.

Table II -5\% Thickness of protector set (one side)
Unit: mm

| Model No. | Double-seal set <br> reference No. | Increased <br> thicknessV |
| :---: | :---: | :---: |
| LH20 | LH2OPT-01 | 2.9 |
| LH25 | LH25PT-01 | 3.2 |
| LH30 | LH3OPT-01 | 4.2 |
| LH35 | LH35PT-01 | 4.2 |
| LH45 | LH45PT-01 | 4.9 |
| LH55 | LH55PT-01 | 4.9 |
| LH65 | LH65PT-01 | 5.5 |
| LH85 | LH85PT-01 | 6.8 |
| LS15 | LS15PT-01 | 3.0 |
| LS20 | LS2OPT-01 | 2.7 |
| LS25 | LS25PT-01 | 3.2 |
| LS30 | LS30PT-01 | 4.2 |
| LS35 | LS35PT-01 | 4.2 |


| Model No. | Double-seal set <br> reference No. | Increased <br> thickness ${ }_{1}$ |
| :---: | :---: | :---: |
| LY15 | LY15PT-01 | 4.1 |
| LY20 | LY20PT-01 | 4.1 |
| LY25 | LY25PT-01 | 6.1 |
| LY30 | LY30PT-02 $\quad *$ | 6.6 |
| LY35 | LY35PT-03 $\quad * *$ | 7.6 |
| LY45 | LY45PT-03 $\quad * *$ | 8.6 |
| LY55 | LY55PT-02 $\quad *$ | 8.6 |
| LY65 | LY65PT-03 $\quad * *$ | 8.6 |
| LW17 | - |  |
| LW21 | - | - |
| LW27 | LW27PT-01 | - |
| LW35 | LW35PT-01 | 2.9 |
| LW50 | LW50PT-01 | 4.2 |

*) Can be used with a new type of seal. (seal flat type, installed on the stepped rail top face)
**) Can be used with a new type of seal. (seal flat type, installed on the stepped rail top face)
Please consult NSK when installing old type seal.
-A connector (Fig. II-5•6) is necessary to install a grease fitting to the end cap after a double seal or protector are assembled. Specify a double seal set with a connector when ordering.


Fig. II-5 $\mathbf{- 5}$ Connector
Reference number examples with connector
(a) Double seal plus connector for LH25: LH25WSC-0*
(b) Protector plus connector for LS30: LS30PTC-0*

## (3) Cap to cover the bolt hole for rail mounting

- After the rail is mounted to the machine base, a cap is used to cover the bolt hole to prevent foreign matters from clogging up the hole or from entering into the ball slide (Fig. II-5•7).
- The cap for the bolt hole is made of synthetic resin which is superb in its resistance to oil and wear.
- Table II $-5 \times 6$ shows sizes of the bolts for the each model number as well as reference number of the cap.
- To insert a cap into the rail bolt hole, use a flat tool (Fig. II-5 ${ }^{\circ}$ ). Pound the cap gradually until its height becomes flush with the rail top face.


Fig. II-5.7


Fig. II -5.8
Table II -5.6 Caps to cover rail bolt hole

| Model No. | Bolt to <br> secure rail | Cap <br> reference number |
| :---: | :---: | :---: |
| LS15 | M3 | L45800003-003 |
| LY15, LW27 | M4 | L45800004-003 |
| LH20, LS20, LY20 | M5 | L45800005-003 |
| LH25, LS25, LY25, LS30, LW35 | M6 | L45800006-003 |
| LH30, LA30, LY30, LH35, LS35, LY35, LW50 | M8 | L45800008-003 |
| LH45, LA45, LY45 | M12 | L45800012-003 |
| LH55, LA55, LY55 | M14 | L45800014-003 |
| LH65, LA65, LY65 | M16 | L45800016-003 |
| LH85 | M22 | L45800022-003 |

## (4) Inner seal

- The end seal installed on both ends of the ball slide cannot arrest entire foreign matters, though the missed amount is negligible. An inner seal protects the ball contact surface from such foreign matters which entered inside the ball slide (Fig. II-5.9).
- Inner seal is installed inside the ball slide. Therefore, the appearance in size and the shape are the same as standard ball slide. (Inner seal is already installed before shipped from the factory.)pping.
- It is strongly recommended to use a bellows and a double seal, along with an inner seal, to maintain precision of the linear guide.


Fig. II -5-9 Inner seal when installed

## Linear guide which can use inner seal

Inner seal can be manufactured for linear guides shown in Table II-5•7.

## (5) Bellows

- Bellows covers entire linear guide and ball screw. It has been used widely as a way of protection in an environment where foreign matters are prevalent.
- NSK has bellows exclusively for LH, LS, LA, LY and LW Series. They have a middle bellows and a 148 bellows at both ends. For LY and LH Series, there are low and high type bellows which are in compliance with their ball slide types.
- The high type is used for AN and BN types. The low type is used for FL, EL, HL, GL, AL, BL Types. By combining, the top of the bellows is slightly lower than the top face of the ball slide.
- When a high type bellows is installed to the ball slide with the height code L (such as FL), the top of the bellows becomes higher than the ball slide. But it is advantageous for stroke because the pitch of the bellows becomes larger.

Table II -5•7

| Series | Model No. |
| :---: | :---: |
| LH Series | LH20, LH25, LH30, LH35, LH45, LH55, LH65, LH85 |
| LS Series | LS20, LS25, LS30, LS35 |
| LA Series | LA30, LA35, LA45, LA55, LA65 |
| LY Series | LY30, LY35, LY45, LY55 |

## (1) LH and LS Series

* Installation in the ball slide (Fig. II -5-10)
- Remove two machine screws (M2) which secure the end seals to the end of the ball slide (Fig. II-5.10).
- Then place a spacer to the hole for securing end seal. Fasten the mounting plate at the end of the bellows to the ball slide with a slightly longer machine screws (provided with the bellows).


## * Installation in the rail

- To install bellows for LH Series and LS Series, lightly knock a fastener exclusively for bellows to the end of the rail (Fig. II-5.10). Then secure the mounting plate at the end of the bellows through the tap hole of the fastener.
- As described above, a bellows can be easily installed in the end of the rail without creating a tap hole on the end of the rail. (This method cannot be used for LH85.)


Fig. II -5•10

## (2) LY Series

* Installation in the ball slide (Fig. II-5011)
- Remove only two machine screws which secure the end seal. (Remove top two screws when four screws are used.) Then, to secure the bellows, drive a slightly longer machine screw (provided with the bellows) into the smaller hole of the mounting plate into the holes from which two machine screws were removed.


## * Installation in the rail

- Put tap holes to the rail end face. Install the bellows mounting plate to the rail through the tap hole. Use a machine screw. NSK processes the tap holes to the rail end face when ordered with a linear guide.


Fig. II-5•11

## (3) LA and LW Series

* Installation to the ball slide (Fig. II -5•12 and Fig. II -5•13)
- Remove two machine screws which secure the end seal. (For LW17 and 21, hold the end cap by hand. Otherwise, the end cap is detached from the ball
slide, and the balls inside may spill out.)
- Place a spacer in the securing hole of the end seal, fasten the mounting plate on the end of the bellows using a slightly longer machine screw (provided with the bellows).


## ＊Installation in the rail

－Same as the case for LY Series，make tap holes to the rail end face．Fix the bellows mounting plate to the rail end face through these tap holes．Use a
machine screw．NSK processes a tap hole to the rail end face when ordered with a linear guide．


Fig．II－5•12


Fig．II－5•13

## Calculating length of bellows

－Formula is as follows．
－A bellows forms one block（BL）with six folds as shown in Fig． $\mathbb{I}-5 \cdot 14$ ．Stroke is determined by multiplying by an integer of this BL．
－Length when stretched to maximum size ：
Lmax $=7 \times$ P x Number of BL
－Length when contracted to minimum size ：
Lmin＝ $\mathbf{1 7} \mathbf{x}$ Number of BL
－Stroke ：
St＝Lmax－Lmin


Fig．II－5•14

## Dimension tables of bellows LH Series



Bellows refemce number

|  |
| :--- | :--- | :--- | :--- |
| Bellows <br> A: Bellows for the ends <br> B: Middle bellows |
| Bellows for LH series |

Fig. II-5-15 Dimensions of bellows
Table II -5\& Dimensions of bellows
Unit: mm

| Model No. | H | $h_{1}$ | E | W | $P$ | a | $b$ | BL minimum length | $M_{1}$ Tap $\times$ depth | M2Tap x depth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J AH20N | 29.5 | 24.5 | 5 | 48 | 10 | 13 | 22 | 17 | M $3 \times 5$ | M $2.5 \times 16$ |
| J AH25L | 35 | 28 | 7 | 51 | 10 | 16 | 26 | 17 | M $3 \times 5$ | M $3 \times 18$ |
| J AH25N | 39 | 32 |  | 61 | 15 |  |  |  |  |  |
| J AH30L | 41 | 32 | 9 | 60 | 12 | 18 | 31 | 17 | M $4 \times 6$ | M $4 \times 22$ |
| J AH30N | 44 | 35 |  | 66 | 15 |  |  |  |  |  |
| J AH35L | 47 | 37.5 | 9.5 | 72 | 15 | 24 | 34 | 17 | M $4 \times 6$ | M $4 \times 23$ |
| J AH35N | 54 | 44.5 |  | 82 | 20 |  |  |  |  |  |
| J AH45L | 59 | 45 | 14 | 83 | 15 | 32 | 44.5 | 17 | M5 x 8 | M $5 \times 28$ |
| J AH45N | 69 | 55 |  | 103 | 25 |  |  |  |  |  |
| J AH55L | 69 | 54 | 15 | 101 | 20 | 40 | 50.5 | 17 | M5 x 8 | M5 x 30 |
| J AH55N | 79 | 64 |  | 121 | 30 |  |  |  |  |  |
| J AH65N | 89 | 73 | 16 | 131 | 30 | 48 | 61 | 17 | M6x 8 | M6x 35 |
| J AH85N* | 108 | 90 | 18 | 173 | 40 | $54 *$ | 51* | 17 | M6x8 | M8x 40 |

*Bellows is fixed to the tap hole at the rail end for LH85.
Table II-5^9 Numbers of folds (BL) and lengths of bellows
Unit: mm

| Model No. | Number of BL | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lmin | 34 | 68 | 102 | 136 | 170 | 204 | 238 | 272 | 306 | 340 |
| J AH2ON | Stroke | 106 | 212 | 318 | 424 | 530 | 636 | 742 | 848 | 954 | 1060 |
|  | $L$ max | 140 | 280 | 420 | 560 | 700 | 840 | 980 | 1120 | 1260 | 1400 |
| J AH25L | Stroke | 106 | 212 | 318 | 424 | 530 | 636 | 742 | 848 | 954 | 1060 |
|  | $L_{\text {max }}$ | 140 | 280 | 420 | 560 | 700 | 840 | 980 | 1120 | 1260 | 1400 |
| J AH25N | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  | $L_{\text {max }}$ | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| J AH30L | Stroke | 134 | 268 | 402 | 536 | 670 | 804 | 938 | 1072 | 1206 | 1340 |
|  | $L_{\text {max }}$ | 168 | 336 | 504 | 672 | 840 | 1008 | 1176 | 1344 | 1512 | 1680 |
| J AH3ON | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  | $L_{\text {max }}$ | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| J AH35L | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  | Lmax | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| J AH35N | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  | Lmax | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| J AH45L | Stroke | 176 | 352 | 528 | 704 | 880 | 1058 | 1232 | 1408 | 1584 | 1760 |
|  | Lmax | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| J AH45N | Stroke | 316 | 632 | 948 | 1264 | 1580 | 1896 | 2212 | 2528 | 2844 | 3160 |
|  | Lmax | 350 | 700 | 1050 | 1400 | 1750 | 2100 | 2450 | 2800 | 3150 | 3500 |
| J AH55L | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  | $L$ max | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| J AH55N | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  | $L_{\text {max }}$ | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |
| J AH65N | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  | Lmax | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |
| JAH85N f | Stroke | 526 | 1052 | 1578 | 2104 | 2630 | 3156 | 3682 | 4208 | 4734 | 5260 |
|  | $L_{\text {max }}$ | 560 | 1120 | 1680 | 2240 | 2800 | 3360 | 3920 | 4480 | 5040 | 5600 |

Remarks: Values of odd numbers BL ( $3,5,7, \ldots$ ) can be obtained by adding two values of even number BLs on both sides, then dividing the sum by two.

## LS Series



Bellows refence number

| Bellows |
| :--- |
| B: Bellows for the ends <br> B: Middle bellows |
| Bellows for LS series |

Fig. II-516 Dimension of bellows
Table II -5-10 Dimensions of bellows
Unit: mm

| Model No. | $H$ | $h_{1}$ | $E$ | $W$ | $P$ | $a$ | $b$ | BL minimum length | $M_{1}$ Tap $\times$ depth | $M_{2}$ Tap $\times$ depth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J AS15L | 23.5 | 18.9 | 4.6 | 43 | 10 | 8 | 16.5 | 17 | $\mathrm{M} 3 \times 5$ | $\mathrm{M} 3 \times 14$ |
| J AS20L | 27 | 21 | 6 | 48 | 10 | 13 | 19.7 | 17 | $\mathrm{M} 3 \times 5$ | $\mathrm{M} 2.5 \times 14$ |
| J AS25L | 32 | 25 | 7 | 51 | 10 | 15 | 23.2 | 17 | $\mathrm{M} 3 \times 5$ | $\mathrm{M} 3 \times 18$ |
| J AS30L | 41 | 32 | 9 | 66 | 15 | 16 | 29 | 17 | $\mathrm{M} 4 \times 6$ | $\mathrm{M} 4 \times 19$ |
| JAS35L | 47 | 36.5 | 10.5 | 72 | 15 | 22 | 33.5 | 17 | $\mathrm{M} 4 \times 6$ | $\mathrm{M} 4 \times 22$ |

Table II -5•11 Numbers of folds (BL) and lengths of bellows
Unit: mm

| Model No. | Number of BL | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $L$ min | 34 | 68 | 102 | 136 | 170 | 204 | 238 | 272 | 306 | 340 |
| J AS15L | Stroke | 106 | 212 | 318 | 424 | 530 | 636 | 742 | 848 | 954 | 1060 |
|  | $L_{\text {max }}$ | 140 | 280 | 420 | 560 | 700 | 840 | 980 | 1120 | 1260 | 1400 |
| J AS20L | Stroke | 106 | 212 | 318 | 424 | 530 | 636 | 742 | 848 | 954 | 1060 |
|  | $L$ max | 140 | 280 | 420 | 560 | 700 | 840 | 980 | 1120 | 1260 | 1400 |
| J AS25L | Stroke | 106 | 212 | 318 | 424 | 530 | 636 | 742 | 848 | 954 | 1060 |
|  | $L$ max | 140 | 280 | 420 | 560 | 700 | 840 | 980 | 1120 | 1260 | 1400 |
| J AS30L | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  | $L_{\text {max }}$ | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| J AS35L | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  | $L$ max | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |

Remarks: Values of odd number BL (3, 5, 7, ...) can be obtained by adding two values of even number BLs on both side, then dividing the sum by two.

## LA Series



Bellows refence number


Fig. II-5•17 An installed bellows

Table II -512 Dimensions of bellow
Unit: mm

| Model number <br> of bellows | $H$ | $h_{1}$ | $E$ | $W$ | $P$ | $a$ | $b$ | Length <br> of BL | Tap <br> $(M)$ xdepth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J AA30L | 41 | 33.5 | 7.5 | 60 | 12 | 14 | 17.5 | 17 | $\mathrm{M} 4 \times 6$ |
| JAA30N | 44 | 36.5 | 7.5 | 66 | 15 | 14 | 17.5 | 17 | $\mathrm{M} 4 \times 6$ |
| JAA35L | 47 | 39.5 | 7.5 | 72 | 15 | 15 | 18.8 | 17 | $\mathrm{M} 4 \times 6$ |
| JAA35N | 54 | 46.5 | 7.5 | 82 | 20 | 15 | 18.8 | 17 | $\mathrm{M} 4 \times 6$ |
| JAA45L | 59 | 49 | 10 | 93 | 20 | 25 | 22.5 | 17 | $\mathrm{M} 5 \times 8$ |
| JAA45N | 69 | 59 | 10 | 113 | 30 | 25 | 22.5 | 17 | $\mathrm{M} 5 \times 8$ |
| JAA55L | 69 | 57 | 12 | 101 | 20 | 35 | 27.1 | 17 | $\mathrm{M} 5 \times 8$ |
| JAA55N | 79 | 67 | 12 | 121 | 30 | 35 | 27.1 | 17 | $\mathrm{M} 5 \times 8$ |
| JAA65N | 89 | 75 | 14 | 131 | 30 | 40 | 33.3 | 17 | $\mathrm{M} 5 \times 8$ |

Table II-5•13 Numbers of folds (BL) and length of bellows
Unit: mm

| Type | Model number of bellows | Length of BL | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Lmin | 34 | 68 | 102 | 136 | 170 | 204 | 238 | 272 | 306 | 340 |
| Low type | J AA30L | Stroke | 134 | 268 | 402 | 536 | 670 | 804 | 938 | 1072 | 1206 | 1340 |
|  |  | Lmax | 168 | 336 | 504 | 672 | 840 | 1008 | 1176 | 1344 | 1512 | 1680 |
| High type | J AA30N | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  |  | $L_{\text {max }}$ | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| Low type | J AA35L | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  |  | $L_{\text {max }}$ | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| High type | J AA35N | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  |  | Lmax | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| Low type | J AA45L | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  |  | $L_{\text {max }}$ | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| High type | J AA45N | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  |  | Lmax | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |
| Low type | J AA55L | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  |  | $L_{\text {max }}$ | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| High type | J AA55N | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  |  | Lmax | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |
| Low/high type | J AA65L | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  |  | $L_{\text {max }}$ | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |

Note ${ }^{(2)} \quad$ Bellows for LY65 is for both low and high types.
Remarks :Values of odd number Bls are obtained by adding values of the even number BLs on both sides, then dividing the sum by two.

## LY Series



Fig. II-5-18 An installed bellows

Bellows refernce number


Table II-5-14 Dimensions of bellows
Unit: mm

| Model number of bellows | H | $h_{1}$ | E | W | P | a | $b$ | Length of BL | Tap <br> (M) xdepth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J AY25L, J BY25L | 35 | 28 | 7 | 51 | 10 | 12 | 15.25 | 17 | M3x6 |
| JAY25N,J BY25N | 39 | 32 |  | 61 | 15 |  |  |  |  |
| J AY30L, J BY30L | 41 | 32 | 9 | 60 | 12 | 14 | 19 | 17 | M4×8 |
| J AY30N,J BY30N | 44 | 35 |  | 66 | 15 |  |  |  |  |
| J AY35L,J BY35L | 47 | 37.5 | 9.5 | 72 | 15 | 15 | 21 | 17 | M4×8 |
| JAY35N,J BY35N | 54 | 44.5 |  | 82 | 20 |  |  |  |  |
| J AY45L,J BY45L | 59 | 47 | 12 | 93 | 20 | 25 | 25 | 17 | M5 x 8 |
| J AY45N,J BY45N | 69 | 57 |  | 113 | 30 |  |  |  |  |
| J AY55L, J BY55L | 69 | 54 | 15 | 101 | 20 | 35 | 30.5 | 17 | M5 $\times 8$ |
| J AY55N,J BY55N | 79 | 64 |  | 121 | 30 |  |  |  |  |
| J AY65N,J BY65N | 89 | 75 | 14 | 141 | 35 | 40 | 34.25 | 17 | M6x12 |

Table II-5-15 Numbers of folds (BL) and length of bellows
Unit: mm

| Type | Model number of bellows | Length of BL | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Lmin | 34 | 68 | 102 | 136 | 170 | 204 | 238 | 272 | 306 | 340 |
| Low type | $\begin{aligned} & \text { JAY25L } \\ & \text { JBY25L } \end{aligned}$ | Stroke | 106 | 212 | 318 | 424 | 530 | 636 | 742 | 848 | 954 | 1060 |
|  |  | Lmax | 140 | 280 | 420 | 560 | 700 | 840 | 980 | 1120 | 1260 | 1400 |
| High type | $\begin{aligned} & \text { JAY25N } \\ & \text { JBY25N } \end{aligned}$ | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 123 | 1408 | 1584 | 1760 |
|  |  | Lmax | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| Low type | $\begin{aligned} & \text { JAY30L } \\ & \text { JBY30L } \end{aligned}$ | Stroke | 134 | 268 | 402 | 536 | 670 | 804 | 938 | 1072 | 1206 | 1340 |
|  |  | $L_{\text {max }}$ | 168 | 336 | 504 | 672 | 840 | 1008 | 1176 | 1344 | 1512 | 1680 |
| igh type | JAY3ONJBY3ON | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  |  | Lmax | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| Low type | $\begin{aligned} & \text { J AY35L } \\ & \text { J BY35L } \end{aligned}$ | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  |  | Lmax | 210 | 420 | 630 | 840 | 1050 | 1260 | 147 | 1680 | 189 | 2100 |
| High type | JAY35NJBY35N | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  |  | Lmax | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| Low type | $\begin{aligned} & \text { JAY45L } \\ & \text { JBY45L } \end{aligned}$ | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 172 | 1968 | 221 | 2460 |
|  |  | Lmax | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| High type | $\begin{aligned} & \text { JAY45N } \\ & \text { JBY45N } \end{aligned}$ | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  |  | $L_{\text {max }}$ | 420 | 840 | 1260 | 1680 | 2100 | 252 | 2940 | 3360 | 3780 | 4200 |
| Low type | JAY55L JBY55L | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  |  | Lmax | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| High type | $\begin{aligned} & \text { JAY55N } \\ & \text { JBY55N } \end{aligned}$ | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  |  | $L_{\text {max }}$ | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |
| Low/high type ${ }^{1}$ | $\begin{aligned} & \text { JAY65N } \\ & \text { JBY65N } \end{aligned}$ | Stroke | 456 | 912 | 1368 | 1824 | 2280 | 2736 | 3192 | 3648 | 4104 | 4560 |
|  |  | $L_{\text {max }}$ | 490 | 980 | 1470 | 1960 | 2450 | 2940 | 3430 | 3920 | 4410 | 4900 |

Note ${ }^{(2)} \quad$ Bellows for LY65 is for both low and high types.
Remarks :Values of odd number Bls are obtained by adding values of the even number BLs on both sides, then dividing the sum by two.

## LW Series



Bellows refence number

| 」 A | 08 |
| :---: | :---: |
| Bellows | Number of N (fold number) |
| B: Middle bellows | N: High type L: Low type |
| Bellows for LW series | Size number of linear guide |

Fig. II -5•19

Table II-5-16 Dimensions of bellows
Unit: mm

| Model number of bellows | H | $h_{1}$ | E | W | P | $a$ | b | Length of BL | Tap (M) xdepth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J AW17N | 25.5 | 23 | 2.5 | 68 | 15 | 22 | 6 | 17 | M3x6 |
| J AW21N | 29 | 26 | 3 | 75 | 17 | 26 | 7 | 17 | M $3 \times 6$ |
| J AW27N | 37 | 33 | 4 | 85 | 20 | 28 | 10 | 17 | M $3 \times 6$ |
| J AW35L | 34 | 30 | 4 | 100 | 14 | 48 | 12 | 17 | M $4 \times 8$ |
| J AW35N | 41 | 37 |  | 115 | 20 |  |  |  |  |
| J AW50L | 46.5 | 42 | 4.5 | 135 | 20 | 70 | 14 | 17 | M 4 x 8 |
| J AW50N | 56.5 | 52 |  | 160 | 30 |  |  |  |  |

Table II -517 Numbers of folds (BL) and length of bellows

| Model No. | Number of BL | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lmin | 34 | 68 | 102 | 136 | 170 | 204 | 238 | 272 | 306 | 340 |
| J AW17N | Stroke | 176 | 352 | 528 | 704 | 880 | 1056 | 1232 | 1408 | 1584 | 1760 |
|  | Lmin | 210 | 420 | 630 | 840 | 1050 | 1260 | 1470 | 1680 | 1890 | 2100 |
| J AW21N | Stroke | 204 | 408 | 612 | 816 | 1020 | 1224 | 1428 | 1632 | 1836 | 2040 |
|  | Lmin | 238 | 476 | 714 | 952 | 1190 | 1428 | 1666 | 1904 | 2142 | 2380 |
| J AW27N | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  | Lmin | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| J AW35L | Stroke | 162 | 324 | 486 | 648 | 810 | 972 | 1134 | 1296 | 1458 | 1620 |
|  | Lmin | 196 | 392 | 588 | 784 | 980 | 1176 | 1372 | 1568 | 1764 | 1960 |
| J AW35N | Stroke | 218 | 436 | 654 | 872 | 1090 | 1308 | 1526 | 1744 | 1962 | 2180 |
|  | $L$ min | 252 | 504 | 756 | 1008 | 1260 | 1512 | 1764 | 2016 | 2268 | 2520 |
| J AW50L | Stroke | 246 | 492 | 738 | 984 | 1230 | 1476 | 1722 | 1968 | 2214 | 2460 |
|  | Lmin | 280 | 560 | 840 | 1120 | 1400 | 1680 | 1960 | 2240 | 2520 | 2800 |
| J AW50N | Stroke | 386 | 772 | 1158 | 1544 | 1930 | 2316 | 2702 | 3088 | 3474 | 3860 |
|  | Lmin | 420 | 840 | 1260 | 1680 | 2100 | 2520 | 2940 | 3360 | 3780 | 4200 |

Remarks: Values of odd numbers BL (3,5,7, ...) can be obtained by adding two values of even number BLs on both sides, then dividing the sum by two.

## A-II-6 Rust Prevention and Surface Treatment

## A-II-6.1 Rust Prevention (Stainless steel)

NSK linear guide is available in stainless steel standard series.

OStainless steel standard series
LH Series
LS Series
LE Series
LU Series
LL Series

Select from the above when using in the environment which invites rust.

## A-II-6.2 Surface Treatment

## (1) Types of surface treatment

The following are common types of treatment.
OElectrolytic rust prevention black film treatment (low temperature chrome plating)

- Used to prevent corrosion and light reflection, and for cosmetic purpose.


## OFluoride low temperature chrome plating

- Fluoroplastic coating is provided following the electrolytic rust prevention black film treatment.
- Resistance to corrosion is higher than electrolytic rust prevention film treatment.
OChrome plating for industrial use (Hard chrome plating)
- Has high hardness. Increases resistance to both wear and corrosion.


## OElectroless nickel plating

- Creates a film of consistent thickness on complex shaped items.
- For corrosion prevention.

OPhosphate coating

- For corrosion prevention: usually applied prior to painting because this treatment creates porous surface.
OBlack oxide treatment (Irontetraxcide film
- Creates irontetraxide film on the surface. For
cosmetic purposes.


## treatment)

## (2) Recommended surface treatment

From among the surface treatments above, NSK recommend "electrolytic rust prevention black film treatment" and "fluoride low temperature chrome plating," because of its better results in humidity cabinet test, and cost-effectiveness.
Please refer to Page D5 for the details of humidity cabinet test results.

## A-II-7 Linear Guides for Special Environments

## A-II-7.1 Heat-resistant Specifications

- Standard linear guides use plastic for ball recirculation component. The environmental temperature of standard linear guides at maximum is $80^{\circ} \mathrm{C}$.

Table II-7•1 Comparison of materials: Standard and heat-resistant specifications

| Component | Standard specification | Heat-resistant specification |
| :---: | :---: | :---: |
| Rail | Special high carbon steel (equivalent to SUS440C/J IS) | Special high carbon steel (equivalent to SUS440C/J IS) |
| Ball slide | Special high carbon steel (equivalent to SUS440C/J IS) | Special high carbon steel (equivalent to SUS440C/J IS) |
| Balls | SUJ 2, SUS440C | SUJ 2, SUS440C |
| Ball retainer | Polyacetals | SUS304 |
| Ball retaining wire | SUS304 | SUS304 |
| End cap | Polyacetals | SUS316L |
| Return guide | Polyacetals | SUS316L |
| End seal | Acrylonitril-butadiene rubber | Fluorine rubber |
| Bottom seal | Acrylonitril-butadiene rubber | Fluorine rubber |

## Heat resistant linear guides

## LH Series

LS Series
LW Series
LE Series
LU Series


Fig. II -7•1

## A-II-7.2 Vacuum and Clean Specifications

- Due to its abundant experience and technology, NSK manufactures linear guides that can be used in a vacuum or in clean environments. Please consult NSK.
- Linear guide specifications vary for environmental conditions.
For example, "all stainless steel plus special grease, or solid film lubricant" for vacuum environments.
- NSK has low-dust generating grease "LG2" which is ideal for clean environments.
Refer to Page D1 for details.


## A-II-8 Noise

- Appropriate design and highly accurate processing technology contribute to reducing noise of NSK linear guides.
- Fig. II- $8 \cdot 1$ is a noise-level data plot. The product of $D_{\mathrm{w}}(\mathrm{mm})$ ball diameter of linear guide and travel speed $V(\mathrm{~m} / \mathrm{min})$ is shown on the abscissa. The noise level is shown on the ordinate.
- The plot indicates that the noise levels remain within a narrow straight belt irrespective of the linear guide type (LH25 through LH65 are plotted here).
- Noise level can be estimated; find the ball diameter from the linear guide model number, then 158 incorporate a travel speed.


Fig. II -81 Noise levels of linear guides

## Example of estimate

LS30, and the travel speed is $100 \mathrm{~m} / \mathrm{min}$.
$D_{w}=4.762 ; V=100 \mathrm{~m} / \mathrm{min}$
Therefore,
$D_{w} \cdot V=4.762 \times 100=476.2$
Therefore, from Fig. II $-8 \bullet 1$, the noise level is $66 \sim 72 \mathrm{~dB}$ (A).

## A-II-9 Arrangement and Mounting of Linear Guide

## A-II-9.1 Arrangement

- For NSK linear guide, the datum face of the rail and of the ball sldie are marked with either an "datum face groove" or with an "arrow."
- In case that two or more linear guides are used together, one linear guise is designated as a reference side guide, and the rest is adjusting side guide(s). The reference side rail has its reference number, serial number, and "KL" mark on the opposite side of the datum face (Fig. II-9•1).
- When the reference side rail is pressed against the mounting faces of machine as well as the ball slide datum face, the variation of mounting width W2 (or W2) must be minimal.
The variations are standardized as accuracy standards (Fig. II-9•2, II-9•3)
- The ways to indicate the datum faces of LE and LU Series are shown in Table II-9•1.


Fig. II -9•1

## Example of arrangement

- Arrangement of the linear guide must be determined taking into account the table position, its direction (horizontal, vertical, inclined, hanging from the ceiling), stroke, the size of bed and the table in the equipment as a whole. Table II-9.2 shows a common arrangement examples, and features/precautions for each case.


Fig. II-9•2 Most common setting of the reference side rail


Fig. II-9॰3 Setting of the refemce side rail in certain occasions

Table II-9.1 Marks on the rail datum faces in LE, LU Series

| Model No. | LU05, 07, 09 <br> LE05, 07, 09, 12 | LU12, 15 | LE15 |
| :--- | :---: | :---: | :---: |
| LE09, 12 (with a ball retainer) |  |  |  |

Table II-9॰2 Arrangement example

| Arrangement | Features/Precautions |
| :---: | :---: |
|  | - Easy in highly-accurate installation (recommended arrangement) |
|  | -Easy in highly-accurate installation <br> - Lubricant oil may not be supplied to ball slide. Precaution is required in the oil supply design. |
|  | - Slightly difficult for highly-accurate installation <br> - Life of linear guide is affected by mounting accuracy. <br> - When oil lubricant is used, precaution is required in oil supply design. |
|  | - Difficult for highly-accurate installation <br> - For a linear guide mounted in sideways, precaution is required in oil supply design if oil lubricant is used. |
|  | - Rather easy in highly-accurate installation <br> - When oil lubricant is used, precaution is required in oil supply design. |
|  | - Easy in highly-accurate installation if the linear guide is installed to the machine base first, then hang up-side-down along with the machine base. <br> - Ball slide may detach from the rail and fall down if the linear guide is damaged and all the balls in the ball slide fall out. It is necessary to take preventive measures against the falling of the ball slide. |

## A-II-9.2 Mounting Accuracy

## (1) Accuracy of the mounting base of machine

- Mounting accuracy of linear guide usually copies the accuracy of the machine base.
- However, when two or more ball slides are assembled to each rail, the table stroke becomes shorter than the mounting surface. This, along with the fact that the mounting error is evenly spread, contributes to a higher table accuracy than the mounting face accuracy, reducing the error to about 1/3 in average (Fig. II-9•4).


## (2) Installation error

- Mounting error affects mainly three factors: life, friction and accuracy (Table II-9•3).


Fig. II -9^4

Table II-9•3 Influence of mounting error

| Factor |  | Influence |
| :---: | :---: | :---: |
| $\stackrel{\text { U }}{\substack{3}}$ |  | - Large mounting error generates a force which twists the ball slide and reduces its life. <br> - It also distorts the contact point of the ball and the groove and changes contact angle, lowering rigidity. |
| 은 |  | - LH and LS Series are affected very little by mounting error thanks to their small friction. (self alignment) <br> - However, being off-set gothic arch grooves, their friction suddenly soars once the mounting error exceeds a certain level. <br> - Mounting error severely affects friction for LY Series with heavy preload. |
|  |  | - When rigidity of four ball slides are equal, the theoretical straightness becomes $1 / 2$ of the installation error $\mathrm{e}_{1}$. <br> - However, this value becomes slightly larger due to deformation of the rail and the machine base. |

## (3) Permissible values of mounting error

- Of the three major factors which are affected by the mounting error, NSK focuses on life. By the NSK standard, permissible values of mounting error are the values which allows 5000 km or longer life under the following conditions.
- Load volume per ball slide is $10 \%$ of the basic dynamic load rating C.
- Rigidity of the machine base is infinite.
- Fig. II-9•5 and II-9•6 are representing the mounting errors. Their permissible values of mounting error 162 are shown in Table II-9•4 to II-9•7.


Fig. II -9‘6
Table II-9^4 Permissible values of parallelism for LH Series
Unit: $\mu \mathrm{m}$

| Value | Preload | Model No. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LH20 | LH25 | LH30 | LH35 | LH45 | LH55 | LH65 | LH85 |
| Permissible values of parallelism in two rails $\mathrm{e}_{1}$ | Z0, ZT | 30 | 40 | 45 | 55 | 65 | 80 | 110 | 120 |
|  | Z1, ZZ | 20 | 25 | 30 | 35 | 45 | 55 | 70 | 90 |
|  | Z3 | 15 | 20 | 25 | 30 | 40 | 45 | 60 | 70 |
| Permissible values ofparallelism (height) in two rails $\mathrm{e}_{2}$ | Z0, Z1 | $375 \mu \mathrm{~m} / 500 \mathrm{~mm}$ |  |  |  |  |  |  |  |
|  | Z1, ZZ, Z3 | $150 \mu \mathrm{~m} / 500 \mathrm{~mm}$ |  |  |  |  |  |  |  |

Table II-9^5 Permissible values of parallelism for LS Series

Unit: $\mu \mathrm{m}$

| Value | Preload | Model No. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LS15 | LS20 | LS25 | LS30 | LS35 |
| Permissible values of parallelism in two rails $\mathrm{e}_{1}$ | Z0, Z | 20 | 22 | 30 | 35 | 40 |
|  | z1, zz | 15 | 17 | 20 | 25 | 30 |
|  | Z3 | 12 | 15 | 15 | 20 | 25 |
| Permissible values of | Z0, T | $375 \mu \mathrm{~m} / 500 \mathrm{~mm}$ |  |  |  |  |
| parallelism (height) in two rails $e_{2}$ | z1, 1,73 | $150 \mu \mathrm{~m} / 500 \mathrm{~mm}$ |  |  |  |  |

Table II -9* Permissible values of parallelism for LA Series

Unit: $\mu \mathrm{m}$

| Value |  | Model No. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Preload | LA30 | LA35 | LA45 | LA55 | LA65 |
| Permissible values of parallelism in two rails $\mathrm{e}_{1}$ | Z3 | 17 | 20 | 25 | 30 | 40 |
|  | Z4 | 15 | 17 | 20 | 25 | 30 |
| Permissible values of parallelism (height) in two rails $e_{2}$ |  | $185 \mu \mathrm{~m} / 500 \mathrm{~mm}$ |  |  |  |  |

Table II-9•7 Permissible values of parallelism for LY Series
Unit: $\mu \mathrm{m}$

| Value | Preload | Model No. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LY15 | LY20 | LY25 | LY30 | LY35 | LY45 | LY55 | LY65 |
| Permissible values of parallelism in two rails $\mathrm{e}_{1}$ | Z0 | 20 | 25 | 25 | 25 | 30 | 40 | 50 | 60 |
|  | Z1 | 20 | 25 | 20 | 25 | 30 | 35 | 45 | 50 |
|  | Z2 | 15 | 20 | 20 | 20 | 25 | 30 | 40 | 45 |
|  | Z3 | 15 | 20 | 15 | 20 | 20 | 25 | 35 | 40 |
|  | Z4 | - | - | 15 | 15 | 20 | 25 | 30 | 35 |
| Permissible values of parallelism (height) in two rails | $185 \mu \mathrm{~m} / 500 \mathrm{~mm}$ |  |  |  |  |  |  |  |  |

## (4) Running accuracy and the influence of even-off effect

- When installed in a machine base, the linear guide is affected by the flatness of the mounting face of the machine base. However, in the case of two-rails/four-ball slides specification, which is most widely used, the straightness as a table as a whole unit is generally less than the straightness as a single component. This is due to the even-off effect


Fig. II -9•7
generated by the shorter stroke, compared to rail length, as well as by interaction between the rails, and ball slides.

- Fig. II-9•9 shows an actually measured straightness of the table which uses NSK linear guide. In this case, the final straightness of the table is about $1 / 5$ of the straightness of the mounting face.


Fig. II-9•8

Fig. II -9ه9 Straightness of the table equipped with linear guide

|  | Straightness in yawing direction | Straightness in pitching direction |
| :---: | :---: | :---: |
| Datum side, mounting surface |  |  |
| Adjusting side, mounting surface |  | $\left.\begin{array}{c}(\mu \mathrm{m}) \\ 0 \\ -2 \\ -4 \\ -6\end{array}\right)$ |
| Datum side, Linear guide |  | $(\mu \mathrm{m})$ |
| Adjusting side, Linear guide |  |  |
| Table accuracy (assembled result) |  |  |

## A-I-9.3 Installation

## (1) Shoulder height of the mounting face of the machine base and comer radius r

- Fig. II-9•10, II-9•11, and Table II-9•9 show shoulder height of the mounting face of the machine base and the size of corner $r$. These figures are relevant when the linear guide is pressed to the shoulder of the bed or table (the raised section from where the mounting face begins), and horizontally secured to it.
- The shoulder should be thick (wide) enough, so it is not deformed by the pressing force.


## (2) Tightening torque of the bolt

- Table II-9•8 shows tightening torque of the bolt when the rail is secured to the fixture of ball groove grinding machine.
- Apply same torque in this table when securing the rail to the machine base. Equal accuracy at the time of grinding can be obtained.

Table II -9\& Bolt tightening torque (Bolt material: High carbon chromium steel)

Unit: $\mathrm{N} \cdot \mathrm{m}(\mathrm{kgf} \cdot \mathrm{cm})$

| Bolt size | Tightening torque | Bolt size | Tightening torque |
| :---: | :---: | :---: | :---: |
| M2.3 | $0.38(3.9)$ | M10 | $43(440)$ |
| M2.5 | $0.58(5.9)$ | M12 | $76(770)$ |
| M3 | $1.06(10.8)$ | M14 | $122(1240)$ |
| M4 | $2.5(25)$ | M16 | $196(2000)$ |
| M5 | $5.1(52)$ | M18 | $265(2700)$ |
| M6 | $8.6(88)$ | M22 | $520(5300)$ |
| M8 | $22(220)$ | - | - |

## (3) Installation procedures

- There are two installation ways depending on the accuracy requirement.
a. Installation with high accuracy
b. Accuracy is not high, but easy to install
- For both methods, wipe off the rust preventive oil applied to the linear guide. Remove burrs and small bumps on the bed and table mounting face with an oilstone (Fig. II-9•12).
Apply machine oil or similar oil with low viscosity to the mounting face to increase the rust preventive effect.
- Linear guide is a precision product. Handle with care.


Fig. II -9•10 Shoulder for the rail datum face


Fig. II-9•11 Shoulder for the ball slide datum face

Table II -9^9 Height of the shoulder and comer radius of the mounting face

Unit: mm

| Rail width | Corner radius <br> $r_{\mathrm{n}}($ maximum $)$ | Shoulder height <br> for the rail $H^{\prime}$ | Shoulder height for <br> the ball slide $H^{\prime \prime}$ |
| :---: | :---: | :---: | :---: |
| 15 | 0.5 | 4 | 4 |
| 20 | 0.5 | 4.5 | 5 |
| 25 | 0.5 | 5 | 5 |
| 30 | 0.5 | 6 | 6 |
| 35 | 0.5 | 6 | 6 |
| 45 | 0.7 | 8 | 8 |
| 55 | 0.7 | 10 | 10 |
| 65 | 1.0 | 11 | 11 |



Fig. II -9•12
(A) Highly accurate installation
(a) Rail installation procedures
(a)-1) Machine base has a shoulder on the side where the reference side rail is installed.
(1) Confirm that the rail is reference side rail, and the datum face of the rail comes to face to face with the shoulder of the bed. Keep the ball slides on the rail, and carefully place the rail on the bed on its mounting face. Temporarily tighten the bolts.
At this time, press the rail from sideways to make the rail tightly contact to the shoulder of the bed. Apply tightening torque to the bolt in Table $\mathbb{I I}-9 \bullet 7$ when tightening a shoulder plate (Fig. II-9•13).
Refer to "(4) Various methods to press linear guide sideways."
(2) For final tightening of the bolts to secure the rail, tighten the bolt on either end of the rail, then proceed to other end.
If the datum face is on the left side as shown in Fig. II-9•14, tighten the bolt at the farthest end first, then proceed to near end.
This way, a bolt rotating force presses the rail against the shoulder. (Therefore, the rail is attached sufficiently tightly against the shoulder by merely pressing the rail by hand. But if there is a danger of applying a lateral impact load, it is necessary to use a shoulder plate to prevent the rail from slipping.)
(3) If the mounting face of the bed where the adjusting side rail is installed also has a shoulder, repeat the steps (1) - (2).
(4) If there is no shoulder on the mounting face of the bed for the adjusting side rail: Secure a measuring table to the ball slides of the reference side rail (Fig. II-9•15). Use this to adjust the parallelism of the adjusting side rail. Check parallelism of the adjusting side rail with a dial gauge from one end of the rail, tightening the bolts one by one.
The measuring table is more stable if secured to two bearings, but one bearing is sufficient.
Parallelism between two rails can also be checked by the same method in Fig. $\mathbb{I I}-9 \cdot 15$ when there is a shoulder on the face where the adjusting side rail is installed.


Fig. II -9•13 Pressing the rail from sideways


Fig. II-9•14 Rail installation


Fig. II-9•15 Measuring parallelism
(a-2) When machine base does not have a shoulder on the side where the reference side rail is installed
(1) Carefully place the reference side rail on the bed on its mounting face. Temporarily tighten the bolts. Do not tighten the bolts all the way, but stop tightening when the bolt enters halfway into the bolt hole. This makes the proceeding steps easier.
(2) Place the straight edge almost parallel to the reference side rail which is temporarily secured by bolts. (At the both ends of the rail and straight edge, the distance between them shall be almost same.)
(3) Once the position of the straight edge is determined, use it as the reference. With a dial gauge, check parallelism with the rail, and adjust the rail if necessary. Then tighten the bolts.
Ensure that the straight edge does not move while the bolts are being tightened.
This procedure should be carried out starting from one end of the rail to the other end. (Fig. II-9•16).
(4) Finally tighten all bolts with specifieds torque.
(5) There are two ways for installation of adjusting side rail:

1. Based on the straight edge which is used for reference side rail installation
2. Based on the reference side rail which is installed prior to the adjusting side rail.
In both way, use a dial gauge to measure parallelism.
Other procedures are the same as (1)~4), and the (4) for case where there is a shoulder on the machine base.

## (b) Procedures of ball slide installation

## (b-1) When table has a shoulder

(1) Arrange the ball slides so that locations match to their mounting section of the table. Carefully place the table on the ball slides. Temporarily tighten all bolts.
(2) While pressing the table from sideways, further tighten the bolts which secure the ball slides on the reference side, so the table shoulder and the ball slide's mounting datum face are sufficiently tightly attached.
If a shoulder plate is provided, first tighten the bolts of the plate, then further tighten the bolts to the ball slides (Fig. II-9•17).


Fig. II -9•16


Fig. II -9•17 Pressing ball slide from sideways
(3) Then, further tighten the bolts for ball slides on the adjusting side rail.
Move the table by hand to confirm that there is no abnormality such as excessive friction force during stroking. (This confirms that the correct installation steps were taken.)
(4) Finally, tighten all bolts with standard torque.
(b)-2) When table does not have a shoulder
(1) Arrange the ball slides so that locations match to their mounting section of the table. Carefully place the table on the ball slides. Temporarily tighten bolts to secure ball slides.
(2) Since the table does not have a shoulder, immediately tighten the bolts further to secure ball slides.
(3) Move the table by hand to confirm that there is no abnormality. Finally, tighten all bolts with standard torque.

## (B) Easy installation

(1) Carefully place the reference side rail on the bed. Then tighten the bolts for installation with specified torque.
(2) Temporarily tighten the bolts on the adjusting side rail.
(3) Tighten the ball slides on the reference side rail and one ball slide on the adjustment side rail with specified torque. Leave the rest of the ball slide on the adjusting side rail temporarily tightened (Fig. II-9•18).
(4) While moving the table with each pitch of the bolt for rail: With specified torque, tighten the rail mounting bolt which is located immediately adjacent to the ball slide on the adjusting side rail that had been finally tightened.
Take this procedure from one end to the other.
(5) Return the table to the original position once. Then with standard torque, tighten the rest of the ball slides on the adjusting side. Then, by the same procedure as in (4), tighten the rest of the rail mounting bolts with standard torque. Move the table to check any abnormality such as large friction force.


Fig. II-9•18 Easy installation

## (4) Various methods to press linear guide sideways



Fig. II -9•19 Recommended method


Fig. II-9020 Installation that requires caution


Fig. II -9•21


Fig. II -9•22

- This method is most widely used, and generally recommended. The ball slide and the rail should stick out slightly from the sides of table and bed. The shoulder plate should have a recess, so the 168 corners of the rail and ball slide do not touch the shoulder plate.
- A tapered block is squeezed in. But the slightest tightening of the bolt generates a large pressing force to the side. Too much tightening may cause the rail to deform, or the land (shown in the figure left) to warp to the right. This method requires caution.
- The bolt that presses rail must be thin due to limited space.
- Press a needle-shape roller with a taper section of the head of a slotted pan head screw. Watch out for the position of the screw.


## A-II-9.4 Assemble the Interchangeable Linear Guide

- Interchangeable ball slide is assembled on a provisinal rail (an inserting tool) when it is delivered (Fig. II-9•23).
- NSK standard grease is packed into the ball slide, allowing immediate use.


## Assembly procedures of interchangeable linear guide

Follow steps as described below.
(1) Wipe off the rust preventive oil from the rail and ball slide.
(2) Match the datum face of rail and the ball slide (groove for installation) as shown in (Fig. II-9•24).
(3) Align the provisional rail to the rail in the bottom and side faces. Press the provisional rail lightly against the rail, and move the ball slide over the rail (Fig. II-9•23).


Fig. II -9023 Inserting interchangeable ball slide into the rail


Fig. II -9•24

## A-II-9.5 Mark for Butting Rails

- A rail which requires the length that exceeds manufactured maximum length comes in butting specification.
- The rail with butting specification are marked with alphabet (A, B, C ...) and an arrow on the opposite side of the mounting datum face. Use the alphabets and arrows for assembly order and direction of the rail (Fig. II-9•25).
- The pitch of the rail mounting hole on the butting section should be as F in Fig. II-9•26. When two rails are used in parallel, the butted sections should not align. This is to avoid change in the running accuracy of the table at the butted sections.


Fig. II -9•25


Fig. II -9•26

## A-II-9.6 Handling Preloaded Assembly

- In case of the preloaded assembly (non interchangeable), do not remove ball slides from the rail as a general rule.
- If it is unavoidable to remove ball slide from the rail, make certain to use a provisional rail (a tool used to insert a ball slide to the rail) as shown in Fig. II$9 \cdot 27$.
- Provisional rail for each model is in stock.
- Pay due attention to the assembly mark when returning the ball slide back to the rail. Follow the cautions described below.


## Mark for assembling ball slide and rail

- Rails of preloaded assembly (not interchangeable) are marked with a reference number and a serial number on the opposite of the datum face.
- Ball slide to be combined are also marked with the same serial number (reference number is not marked).
- Furthermore, ball slides are marked with an arrow. Ball slides should be positioned with their arrows facing each other.
- In case that the ball slides had to be removed from the rail, confirm their serial numbers and the directions of arrows for re-assembly (Fig. II-9•28).
- When two or more rails are used in a single set, serial numbers are in sequence if their reference numbers are the same. The linear guide with smallest serial number has the "KL" mark (Fig. II9•29).
- When two or more rails of different refernce number are used in a single set, the rails and ball slides have the same serial number. In this case, when ball slide is removed from the rail, it is confusing which rail each ball slide was previously installed. When removing ball slides from the rail for an unavoidable reason (Fig. II-9•30), sufficient precaution is required.


Fig. II -9•27


Fig. II -9•28


Fig. II-9029 When two rails have the same reference number


Fig. II-9॰30 When two rails have different refemce number

## A-II-10 Drills to Select Linear Guide

## A-II-10.1 Single Axis Material Handling System

This section explains linear guide selection, life calculation, and deformation at load acting point for a single axis material handling system equipped with linear guide.


Fig. II-10• Single axis material handling system
The work load is applied only to one way of stroke. Assume that the load is acting in full stroke as the condition of acting load is unknown.

Specification of Single axis material handling system

Table weight
Weight of the work
Acting load

Ball slide span
$L_{b}: 100(\mathrm{~mm})$
Rail span

Load point coordinates from the table center ( mm )

| Load | X coordinate | Y coordinate | $Z$ coordinate |
| :---: | :---: | :---: | :---: |
| W1 | 30 | -20 | 20 |
| W2 | 80 | -90 | 120 |
| $F$ | -50 | -135 | 30 |

Stroke: 1000 mm
(1 cycle: 2000 mm )

| Environment | $: 10-30\left({ }^{\circ} \mathrm{C}\right)$ |
| :--- | :---: |
| Travel speed | $: 12(\mathrm{~m} / \mathrm{min})$ |
| Time to reach travel speed | $: 0.25(\mathrm{sec})$ |
| Operating hour | $: 16(\mathrm{hr} /$ day $)$ |

## (1) Selection of linear guide model

Select a type of linear guide from "A-I-2.1 Types
and Characteristics of Linear Guide." Since this
material handling system has 2 rails and 4 ball slides, LH, LS, and LU Series are suitable.

## (2) Selection of size (model number)

Select a size (model number) from "A-II-3.2
Calculation of Life Expectancy (3) Calculating loads to a ball slide."
Calculating load $P$ per ball slide
Find out potential coefficients $\mathbf{K p 1}$ (for vertical load W1), Kp2 (for vertical load W2) and $\mathbf{K p 3}$ (load F right angle direction to the axis).
From load point coefficients, the potential coefficient $\mathbf{K p 1}$ of vertical direction load $\mathbf{W} \mathbf{1}$ is:

$$
K p 1=\left|\frac{X_{1}}{L_{b}}\right|+\left|\frac{Y_{1}}{L_{r}}\right|=\frac{30}{100}+\frac{20}{90}=0.52
$$

From load point coefficients, the potential coefficient Kp2 of vertical load W2 is:

$$
K p 2=\left|\frac{X_{2}}{L_{\mathrm{b}}}\right|+\left|\frac{Y_{2}}{L_{\mathrm{r}}}\right|=\frac{80}{100}+\frac{90}{90}=1.80
$$

From load point coefficients, the potential coefficient $F$ of lateral load is:

$$
K p 3=\left|\frac{X_{3}}{L_{\mathrm{b}}}\right|+\left|\frac{Z_{3}}{L_{\mathrm{r}}}\right|=\frac{50}{100}+\frac{30}{90}=0.83
$$

Therefore, load $\boldsymbol{P}$ per ball slide is:

$$
\begin{aligned}
P= & \sum \frac{F}{4}+\sum \frac{K \mathrm{p} \cdot F}{2} \\
= & \frac{\mathrm{W} 1+\mathrm{W} 2+F}{4}+\frac{K \mathrm{pl} 1 \cdot \mathrm{~W} 1+K \mathrm{p} 2 \cdot \mathrm{~W} 2+K \mathrm{p} 3 \cdot F}{2} \\
= & \frac{150+200+200}{4} \\
& +\frac{0.52 \times 150+1.8 \times 200+0.83 \times 200}{2} \\
= & 439.5(\mathrm{~N})
\end{aligned}
$$

Based on this, select LU15AL from "Fig. I-3•4

## Selection based on the load "

## (3) Calculating life

Calculate life of the selected LU15AL based on "A-

## II-3.2 Calculation of Life Expectancy."

## Linear guide LU15AL

Basic dynamic load rating : $\mathbf{4 3 0 0}$ ( N )
Basic static load rating : 4500 (N)
Load conditions of the linear guide
Table weight W1:150(N)
Weight of the work W2:200(N)
Applied load
F : 200 (N)
Rail span
Lr : $90(\mathrm{~mm})$
Ball slide span
Lb : 100 (mm)

From the time to reach travel speed and the travel speed, the table acceleration is $0.8 \mathrm{~m} / \mathrm{sec}^{2}$. Therefore, it is not necessary to take into account inertial force brought about by table mass.

## Calculation of the load applied to ball slide

Calculate two occasions:

1. There is the work mounted on the table.
2. No work mounted on the table.

## From Pattem 4 in Table II-3•1

## There is a work mounted on the table Vertical direction loads

$$
\begin{aligned}
M 1 & =\sum_{j=1}^{n}\left(F_{y j} \cdot Z_{y j}\right)+\sum_{k=1}^{n}\left(F_{z k} \cdot Y_{z k}\right) \\
& =F \cdot Z_{3}+W 1 \cdot Y_{1}+W 2 \cdot Y_{2} \\
& =-200 \times 30+150 \times(-20)+200 \times(-90) \\
& =-27000(\mathrm{~N} \cdot \mathrm{~mm}) \\
M 2 & =\sum_{i=1}^{n}\left\{F_{x i} \cdot\left(Z_{x i}-Z_{b}\right)\right\}+\sum_{k=1}^{n}\left(F_{z k} \cdot X_{z k}\right) \\
& =W 1 \cdot X_{1}+W 2 \cdot X_{2} \\
& =150 \times 30+200 \times 80 \\
& =20500(\mathrm{~N} \cdot \mathrm{~mm}) \\
F_{r 1} & =\frac{\sum_{k=1}^{n} F_{z k}}{4}+\frac{M 1}{2 \cdot L}+\frac{M 2}{2 \cdot \ell} \\
& =\frac{W 1+W 2}{4}+\frac{M 1}{2 \cdot L_{r}}+\frac{M 2}{2 \cdot L_{b}} \\
& =\frac{150+200}{4}+\frac{-27000}{2 \times 90}+\frac{20500}{2 \times 100} \\
& =40(\mathrm{~N})
\end{aligned}
$$

Similarly

$$
\begin{aligned}
& F_{\mathrm{r} 2}=-165(\mathrm{~N}) \\
& F_{\mathrm{r} 3}=340(\mathrm{~N}) \\
& F_{\mathrm{r} 4}=135(\mathrm{~N})
\end{aligned}
$$

## Lateral direction loads

$$
\begin{aligned}
M 3 & =-\sum_{i=1}^{n}\left\{F_{x i} \cdot\left(Y_{x i}-Y_{b}\right)\right\}+\sum_{j=1}^{n}\left(F_{y j} \cdot X_{y j}\right) \\
& =F \cdot X_{3} \\
& =-200 \times(-50) \\
& =10000(\mathrm{~N} \cdot \mathrm{~mm})
\end{aligned}
$$

$$
\begin{aligned}
F_{s 1}=F_{s 3} & =\frac{\sum_{j=1}^{n} F_{y j}}{4}+\frac{M 3}{2 \cdot \ell} \\
& =\frac{F}{4}+\frac{M 3}{2 L_{b}} \\
& =\frac{-200}{4}+\frac{10000}{2 \times 100} \\
& =0(\mathrm{~N})
\end{aligned}
$$

## Lateral direction loads

$$
\begin{aligned}
M 3 & =-\sum_{i=1}^{n}\left\{F_{x i} \cdot\left(Y_{x i}-Y_{b}\right)\right\}+\sum_{j=1}^{n}\left(F_{y j} \cdot X_{y j}\right) \\
& =F \cdot X_{3} \\
& =-200 \times(-50) \\
& =10000(\mathrm{~N} \cdot \mathrm{~mm})
\end{aligned}
$$

Similarly

$$
F_{\mathrm{s} 2}=F_{54}=-100(\mathrm{~N})
$$

## No work mounted on the table

Vertical direction load

$$
\begin{aligned}
M 1 & =\sum_{j=1}^{n}\left(F_{y j} \cdot Z_{y j}\right)+\sum_{k=1}^{n}\left(F_{z k} \cdot Y_{z k}\right) \\
& =F \cdot Z_{3}+W 1 \cdot Y_{1} \\
& =-200 \times 30+150 \times(-20) \\
& =-9000(\mathrm{~N} \cdot \mathrm{~mm})
\end{aligned}
$$

$$
\begin{aligned}
M 2 & =\sum_{i=1}^{n}\left\{F_{x i}\left(Z_{x i}-Z_{b}\right)\right\}+\sum_{k=1}^{n}\left(F_{z k} \cdot X_{z k}\right) \\
& =W 1 \cdot X_{1} \\
& =150 \times 30 \\
& =4500(\mathrm{~N} \cdot \mathrm{~mm})
\end{aligned}
$$

$$
\begin{aligned}
F_{r 1} & =\frac{\sum_{k=1}^{n} F_{z k}}{4}+\frac{M 1}{2 \cdot L}+\frac{M 2}{2 \cdot \ell} \\
& =\frac{W 1}{4}+\frac{M 1}{2 \cdot L_{r}}+\frac{M 2}{2 \cdot L_{b}} \\
& =\frac{150}{4}+\frac{-9000}{2 \times 90}+\frac{4500}{2 \times 100} \\
& =10(\mathrm{~N})
\end{aligned}
$$

## Similarly

$$
\begin{aligned}
& F_{\mathrm{r} 2}=-35(\mathrm{~N}) \\
& F_{\mathrm{r} 3}=110(\mathrm{~N}) \\
& F_{\mathrm{r} 4}=65(\mathrm{~N})
\end{aligned}
$$

$$
\begin{aligned}
F_{s 1}=F_{s 3} & =\frac{\sum_{j=1}^{n} F_{y j}}{4}+\frac{M 3}{2 \cdot \ell} \\
& =\frac{F}{4}+\frac{M 3}{2 \cdot L_{b}} \\
& =\frac{-200}{4}+\frac{10000}{2 \times 100} \\
& =0(\mathrm{~N})
\end{aligned}
$$

Similarly

$$
F_{\mathrm{s} 2}=F_{\mathrm{s} 4}=-100(\mathrm{~N})
$$

For calculation, take into consideration the positive or negative signs (+, -) for load point coordinate.

## Calculation of dynamic equivalent load

Use "A-II-3.2 (4) Calculation of dynamic equivalent load."
It matches Position 4 in "Table II-3•2 Loads in the arrangement of linear guides." Ball slide loads that must be considered are vertical and lateral direction loads.

In case of LU15AL,
Vertical direction dynamic equivalent load

$$
F r=F r
$$

Lateral direction dynamic equivalent load

$$
\boldsymbol{F}_{\mathrm{se}}=\boldsymbol{F}_{5} \tan \alpha=\boldsymbol{F}_{5}
$$

Use the formula for full dynamic equivalent load 174 (Page A136) to calculate $F_{\text {e }}$.
Results are shown in the table below.

Unit: N

| Work mounted | Brg1 | Brg2 | Brg3 | Brg4 |  |
| :--- | ---: | :--- | :--- | ---: | ---: |
| $F_{\mathrm{r}}\left(F_{\mathrm{r} 1} \sim F_{\mathrm{r} 4}\right)$ | 40 | -165 | 340 | 135 |  |
| $F_{\mathrm{se}}\left(F_{\mathrm{s} 1} \sim F_{\mathrm{s} 4}\right)$ | 0 | -100 | 0 | -100 |  |
| $F_{\mathrm{e}}$ |  | 40 | 215 |  | 340 |
| No work mounted | Brg1 |  | Brg2 |  | Brg3 |
| $F_{\mathrm{r}}\left(F_{\mathrm{r} 1} \sim F_{\mathrm{r} 4}\right)$ | 10 |  | -35 | Brg4 | 185 |
| $F_{\mathrm{se}}\left(F_{\mathrm{s} 1} \sim F_{\mathrm{s} 4}\right)$ | 0 | 110 | 65 |  |  |
| $F_{\mathrm{e}}$ |  | 10 | -100 | 0 | -100 |

From these results, use the largest full dynamic equivalent loads for the calculations hereafter.
Therefore, the results are:
Work mounted $F_{\mathrm{e} 1}=340(\mathrm{~N})$
No work mounted $F_{\mathrm{e} 2}=133(\mathrm{~N})$
Therefore, the results are:

## Calculation of mean effective load

Based on "A-II-3.2 (5) Calculation of mean effective load," calculate from the largest full dynamic equivalent loads.


Cycle patterns of full dynamic equivalent load

From the cycle pattern, the mean effective load matches " ${ }^{(1)}$ When load and running distance vary by phase." Therefore, use the following formula. Assuming that $L$ is: $L=L_{1}+L_{2}$.

$$
\begin{aligned}
F m & =\sqrt[3]{\frac{1}{L}\left(F_{e 1}^{3} L_{1}+F_{e 2}^{3} L_{2}\right)} \\
& =\sqrt[3]{\frac{1}{2000}\left(340^{3} \times 1000+133^{3} \times 1000\right)} \\
& =275(\mathrm{~N})
\end{aligned}
$$

## Determine various coefficients

Determine coefficients to use from "A-II-3.2 (6)
Various coefficients."

## Load factors

Use conditions are: Travel speed -- $12 \mathrm{~m} / \mathrm{min}$; Acceleration -- $0.8 \mathrm{~m} / \mathrm{sec}^{2}(0.082 \mathrm{G})$. As the load factor $f_{w}$ is in the range of $1.0 \sim 1.5$, use common value $\boldsymbol{f}_{\mathbf{w}}=\mathbf{1 . 2}$.

## Hardness coefficient

The hardness of NSK linear guides is HRC58~62. Use a hardness coefficient $f_{H}=\mathbf{1}$ and take the value of basic dynamic load rating as it is.

## Calculate rating life

Use "A-II-3.2 (7) Calculation of rating life."
Linear guide LU15AL's basic dynamic load rating $C$

$$
\text { : } 4300 \text { (N) }
$$

Mean effective load $F_{\mathrm{m}}: 275(\mathrm{~N})$
Load factor $f_{\mathrm{w}} \quad: 1.2$
Hardness coefficient $f_{\mathrm{H}}: 1$

Rating fatigue life $L=50 \times\left(\frac{f_{\mathrm{H}} \cdot C}{f_{\mathrm{W}} \cdot F_{\mathrm{M}}}\right)^{3}$

$$
\begin{aligned}
& 50 \times\left(\frac{1}{1.2 \times 2300}\right)^{3} \\
& \text { about } 110620(\mathrm{Km})
\end{aligned}
$$

Travel speed: $12 \mathrm{~m} / \mathrm{min}$; Operating hours: 16hr/Day. Convert the above rating fatigue life into hours:

$$
\frac{110620 \times 1000}{12 \times 60 \times 16}
$$

about 9600(Day)

## Examine static load

Based on "A-II-3.2 (8) Examination of static load,"
find out on which ball slide the static equivalent load $P_{0}$ becomes largest.
Linear guide LU15AL's basic static load rating $C_{0}$ : 4500 (N)
Ball slide No. 3 receives the largest load.
$P_{0}$ at this time:

$$
P_{0}=F_{\mathrm{r}}+F_{\mathrm{s}}=340
$$

Therefore, static permissible load coefficient $f_{\mathrm{s}}$ is:

$$
f_{\mathrm{s}}=\frac{C_{0}}{P_{0}}=\frac{4500}{340}=13.2
$$

There is no problem at this value.

## (4) Selection of accuracy grade and preload

Based on "A-I-3.4 (2) Application examples of accuracy grade and preload," select accuracy grade PN and preload $\mathrm{Z1}$ for material handling system.

## (5) Calculation of deformation

Calculate deformation by the weight of the mounted work W2. From "Table II-2•11" in "A-II-2 Preload and Rigidity," the rigidity of linear guide LU15AL, Z1 pre-load is:

$$
K_{s}=K_{r}=45(\mathrm{~N} / \mathrm{mm})=45000(\mathrm{~N} / \mathrm{mm})
$$

Deformation by the weight of the mounted work $W_{2}$ can be obtained: Difference in deformation when $W_{2}$ applies or does not apply.

## From Pattem 4 in Table II-3•1 (Paqe A132)

Work mounted:

$$
\begin{aligned}
& \begin{aligned}
\delta_{x 1} & =Y_{d} \cdot \frac{F_{s 2}-F_{s 1}}{L_{b} \cdot K_{s}}+Z_{d} \cdot \frac{F_{r 1}-F_{r 2}}{L_{b} \cdot K_{r}} \\
& =-90 \times \frac{-100-0}{100 \times 45000}+120 \times \frac{40-(-165)}{100 \times 45000} \\
& =0.0075(\mathrm{~mm})=7.5(\mu \mathrm{~m})
\end{aligned} \\
& \text { Similarly, } \delta_{y 1}=-0.0082(\mathrm{~mm})=-8.2(\mu \mathrm{~m}) \\
& \delta_{\mathrm{z} 1}=0.0123(\mathrm{~mm})=12.3(\mu \mathrm{~m})
\end{aligned}
$$

## No work mounted:

$$
\begin{aligned}
\delta_{x 2} & =Y_{\mathrm{d}} \cdot \frac{F_{\mathrm{s} 2}-F_{\mathrm{s} 1}}{L_{\mathrm{b}} \cdot K_{\mathrm{s}}}+Z_{\mathrm{d}} \cdot \frac{F_{\mathrm{r} 1}-F_{\mathrm{r} 2}}{L_{\mathrm{b}} \cdot K_{\mathrm{r}}} \\
& =-90 \times \frac{-100-0}{100 \times 45000}+120 \times \frac{10-(-35)}{100 \times 45000} \\
& =0.0032(\mathrm{~mm})=3.2(\mu \mathrm{~m})
\end{aligned}
$$

Similarly, $\delta_{y 2}=-0.0023(\mathrm{~mm})=-2.3(\mu \mathrm{~m})$

$$
\delta_{\mathrm{z2}}=0.0039(\mathrm{~mm})=3.9(\mu \mathrm{~m})
$$

Therefore, the difference in deformation by whether there is a mounted work or not is as follows:

$$
\begin{aligned}
& \delta_{x}=\delta_{x 1}-\delta_{x 2}=7.5-3.2=4.3(\mu \mathrm{~m}) \\
& \delta_{y}=\delta_{y 1}-\delta_{y 2}=-8.2-(2.3)=-5.9(\mu \mathrm{~m}) \\
& \delta_{z}=\delta_{z 1}-\delta_{z 2}=12.3-3.9=8.4(\mu \mathrm{~m})
\end{aligned}
$$

## A-II-10.2 Machining Center

The following is a case calculation for a horizontal type machining center. Arrangements of each axis are shown in Fig. II- $10 \cdot 2$ andl Fig. II-10*:.

## Operating conditions

Dimensions and load conditions are:
$X$ axis column's weight $\quad W x: 7500(N)$
Y axis spindle head's weight Wy: 2500 (N)
Z axis table's weight Wz:5500(N)
$X$ axis rail span
$X L_{r}$ : 450 (mm)
$X$ axis ball slide span $\quad X L_{\mathrm{b}}: 310(\mathrm{~mm})$
$Y$ axis rail span
$Y L_{r}: 410(\mathrm{~mm})$
$Y$ axis ball slide span $\quad Y L_{b}: 308(\mathrm{~mm})$
$Z$ axis rail span $\quad Z L_{r}: 660(\mathrm{~mm})$
$Z$ axis ball slide span $\quad Z L_{b}: 420(m m)$

X axis stroke : 400 (mm)
Y axis stroke: 350 (mm)
Z axis stroke : 500 (mm)

Average rapid traverse speed: $15(\mathrm{~m} / \mathrm{min})$
(Max. 30(m/min))
Starting accelerating speed $: 1(\mathrm{G})$
Milling speed $\quad: 2.5(\mathrm{~m} / \mathrm{min})$
Drilling speed $\quad: 0.8(\mathrm{~m} / \mathrm{min})$


Fig. II-10•2 Machining center (front view)


Fig. II-10॰3 Machining center (side view)

## (1) Selection of linear guide model

From the operating conditions, the linear guide should be LY Series which is suitable for the machining center.

## (2) Selection of linear guide size (model number)

Start selection from $Y$ axis which has fewer acting loads.
Coordinates of load points are as follows.
$W y\left(X_{w y}, Y_{w y}, Z_{w y}\right)=(-25,76,-30)(\mathrm{mm})$
$F X \quad\left(X_{F X}, Y_{F X}, Z_{F X}\right)=(-35,90,-323)(m m)$
Fy $\left(X_{F Y}, Y_{F Y}, Z_{F Y}\right)=(-35,90,-323)(\mathrm{mm})$
$F z\left(X_{F Z}, Y_{F Z}, Z_{F Z}\right)=(-35,90,-323)(\mathrm{mm})$
Ball slide span $: Y L_{b}=308 \mathrm{~mm}$
Rail span : $Y L_{r}=410 \mathbf{~ m m}$
First, find out the load volume $\boldsymbol{P}$ per ball slide in milling process (Pyf) and drilling process (Pyd). Refer to "A-I-3.2 Selection of linear guide size (model code)."

Position coefficients at time of milling process (Wy, Fx and Fy must be considered.)
Regarding Wy: From load application coordinates
$K p y 1=\left|\frac{Z_{W Y}}{Y L_{b}}\right|+\left|\frac{X_{W Y}}{Y L_{b}}\right|=\frac{30}{308}+\frac{25}{308}=0.10+0.08=0.18$
Regarding Fx: From load point coordinates
$K p y 2=\left|\frac{Y_{F X}}{Y L_{b}}\right|+\left|\frac{Z_{F Y}}{Y L_{\mathrm{D}}}\right|=\frac{90}{308}+\frac{323}{410}=0.29+0.79=1.08$
Regarding Fy: From load point coordinates
$K p y 3=\left|\frac{Z_{F Y}}{Y L_{\mathrm{D}}}\right|+\left|\frac{X_{F Y}}{Y L_{\mathrm{D}}}\right|=\frac{323}{308}+\frac{35}{308}=1.05+0.11=1.16$
Therefore, load volume Pfy is:

$$
\begin{aligned}
\text { Pyf }= & \sum \frac{F}{4}+\sum \frac{K p \cdot F}{2} \\
= & \frac{W y+F x+F y}{4}+\frac{K p y 1 \cdot W y+K p y 2 \cdot F x+K p y 3 \cdot F y}{2} \\
= & \frac{2500+1000+1000}{4} \\
& +\frac{0.18 \times 2500+1.08 \times 1000+1.16 \times 1000}{2} \\
= & 2470(N)
\end{aligned}
$$

Position coefficients at time of drilling processing (Wy and Fz must be considered.)
Regarding Wy, as in the case for milling process,
Kpy1 $=0.18$

## Regarding Fz: From load point coefficient

$K p y 4=\left|\frac{Y_{F Z}}{Y L_{b}}\right|+\left|\frac{X_{F Z}}{Y L_{r}}\right|=\frac{90}{308}+\frac{35}{410}=0.29+0.09=0.38$
Therefore, load volume Pyd is:

$$
\begin{aligned}
P y d & =\sum \frac{F}{4}+\sum \frac{K p \cdot F}{2} \\
& =\frac{W y+F z}{4}+\frac{K p x 1 \cdot W y+K p y 4 \cdot F z}{2} \\
& =\frac{2500+3000}{4}+\frac{0.18 \times 2500+0.38 \times 3000}{2} \\
& =2170(\mathrm{~N})
\end{aligned}
$$

From the above results, for milling process with large values, select a model LY 35 from Fig. I-3^4. for $Y$ axis.

Next, determine the linear guide size for $X$ axis. As with $Y$ axis, the distance from the center of the table to the loads and their load points are shown. The stroke position on $Y$ axis is the summit point which imposes strict condition.
$W x\left(X_{w x}, Y_{w x}, Z_{w x}\right)=(0,510,-65)(m m)$ $W y\left(X_{w y}, Y_{w y}, Z_{w y}\right)=(-25,916,-325)(\mathrm{mm})$
$F X \quad\left(X_{F X}, Y_{F X}, Z_{F X}\right)=(-35,930,-618)(\mathrm{mm})$
Fy $\left(X_{F Y}, Y_{F Y}, Z_{F Y}\right)=(-35,930,-618)(\mathrm{mm})$
Fz $\quad\left(X_{F Z}, Y_{f Z}, Z_{f z}\right)=(-35,930,-618)(\mathrm{mm})$
Ball slide span : $Y L_{b}=310$ (mm)
Rail span $\quad: Y L_{r}=0450(\mathrm{~mm})$
Also, determine per-ball slide load volume Pxf and Pxd.
Position coefficients at time of milling process (Wx, Wy, Fx and Fy must be considered)
Regarding Wx: From load point coordinates

$$
K p x 1=\left|\frac{X_{w x}}{X L_{b}}\right|+\left|\frac{Z_{w x}}{X L_{r}}\right|=\frac{0}{310}+\frac{65}{450}=0+0.14=0.14
$$

Regarding Wy: From load point coordinates

$$
K p \times 2=\left|\frac{X_{W Y}}{X L_{\mathrm{b}}}\right|+\left|\frac{Z_{W Y}}{X L_{r}}\right|=\frac{25}{310}+\frac{325}{450}=0.08+0.72=0.8
$$

Regarding Fx: From load point coordinates
$K p x 3=\left|\frac{Y_{F X}}{X L_{b}}\right|+\left|\frac{Z_{F X}}{X L_{b}}\right|=\frac{930}{310}+\frac{618}{310}=3.00+1.99=4.99$
Regarding Fy: From load point coordinates
$K p \times 4=\left|\frac{X_{F Y}}{X L_{b}}\right|+\left|\frac{Z_{F Y}}{X L_{r}}\right|=\frac{35}{310}+\frac{618}{450}=0.11+1.37=1.48$
Therefore,

$$
\begin{aligned}
P x f & =\sum \frac{F}{4}+\sum \frac{K p \cdot F}{2} \\
& =\frac{W x+W y+F x+F y}{4} \\
& +\frac{K p x 1 \cdot W x+K p x 2 \cdot W y+K p x 3 \cdot F x+K p x 4 \cdot F y}{2} \\
& =\frac{7500+2500+1000+1000}{4} \\
& +\frac{0.14 \times 7500+0.8 \times 2500+4.99 \times 1000+1.48 \times 1000}{2} \\
& =7760(\mathrm{~N})
\end{aligned}
$$

Position coefficients at time of drilling process (Wx, Wy and Fz must be considered)
Regarding Wx: Kpx1=0.14
(same as milling process)
Regarding Wy: Kpx2=0.80
(same as milling process)
Regarding Fz: From the load point coordinates
$K p x 5=\left|\frac{X_{F Z}}{X L_{b}}\right|+\left|\frac{Y_{F Z}}{X L_{r}}\right|=\frac{35}{310}+\frac{930}{450}=0.11+2.07=2.18$

## Therefore,

$$
\begin{aligned}
P x d= & \sum \frac{F}{4}+\sum \frac{K p \cdot F}{2} \\
= & \frac{W x+W y+F z}{4} \\
& +\frac{K p x 1 \cdot W x+K p x 2 \cdot W y+K p x 5 \cdot F z}{2} \\
= & \frac{7500+2500+3000}{4} \\
& +\frac{0.14 \times 7500+0.8 \times 2500+2.18 \times 3000}{2} \\
= & 8045(\mathrm{~N})
\end{aligned}
$$

From the above results, for drilling process with large values, select a model from Fig. I-3•4. and LY55 is chosen for $X$ axis.

Finally, determine $Z$ axis. Similarly, the distance from the center of the table to the loads and their loading points are shown. The stroke positions on $Y$ and $X$ axes are at stroke end which imposes strict condition.


Ball slide span : $Z L_{b}=420(\mathrm{~mm})$
Rail span $: Z L_{r}=660(\mathrm{~mm})$
Position coefficients at time of milling process (Wx, Wy, Wz, Fx and Fy must be considered) Regarding Wx: From load point coordinates
$K p z 1=\left|\frac{Z_{w x}}{Z L_{b}}\right|+\left|\frac{X_{w X}}{Z L_{r}}\right|=\frac{65}{420}+\frac{200}{660}=0.15+0.30=0.45$
Regarding $\mathbf{W y}$ : From load point coordinates

$$
K p z 2=\left|\frac{Z_{w r}}{Z L_{b}}\right|+\left|\frac{X_{w r}}{Z L_{r}}\right|=\frac{325}{420}+\frac{225}{660}=0.77+0.34=1.11
$$

Regarding $\mathbf{W z}$ : From load point coordinates

$$
K p z 3=\left|\frac{Z_{W z}}{Z L_{b}}\right|+\left|\frac{X_{w z}}{Z L_{r}}\right|=\frac{0}{420}+\frac{0}{660}=0+0=0
$$

## Regarding Fx: From load point coordinates

$$
K p z 4=\left|\frac{Z_{F X}}{Z L_{b}}\right|+\left|\frac{Y_{F X}}{Z L_{r}}\right|=\frac{618}{420}+\frac{1150}{660}=1.47+1.74=3.21
$$

## Regarding Fy: From load point coordinates

$K p x 4=\left|\frac{Z_{F Y}}{Z L_{b}}\right|+\left|\frac{X_{F Y}}{Z L_{r}}\right|=\frac{618}{420}+\frac{235}{660}=1.47+0.36=1.83$
Therefore,

$$
\begin{aligned}
P z f & =\sum \frac{F}{4}+\sum \frac{K p \cdot F}{2} \\
& =\frac{W x+W y+W z+F x+F y}{4} \\
& +\frac{K p z 1 \cdot W x+K p z 2 \cdot W y+K p z 3 \cdot W z+K p z 4 \cdot F x+K p z 5 \cdot F y}{2} \\
& =\frac{7500+2500+5500+1000+1000}{4} \\
& +\frac{0.45 \times 7500+1.11 \times 2500+0 \times 5500+3.21 \times 1000+1.83 \times 1000}{2} \\
& =9970(\mathrm{~N})
\end{aligned}
$$

Position coefficients at time of drilling process (Wx, Wy, Wz and Fz must be considered)
Regarding $\boldsymbol{W} \mathbf{x}$ : $K p z 1=0.45$
Regarding $\mathbf{W y}$ : Kpz2=1.11
Regarding Wz: $K p z 3=0$
Regarding Fz: From the load point coordinates

$$
K p 6=\left|\frac{Y_{F Z}}{Z Z_{b}}\right|+\left|\frac{X_{F Z}}{Z L_{b}}\right|=\frac{1150}{420}+\frac{235}{420}=2.74+0.56=3.30
$$

Therefore,

$$
\begin{aligned}
\text { Pzd } & =\sum \frac{F}{4}+\sum \frac{K p \cdot F}{2} \\
& =\frac{W x+W y+W z+F z}{4} \\
& +\frac{K p z 1 \cdot W x+K p z 2 \cdot W y+K p z 3 \cdot W z+K p z 6 \cdot F z}{2} \\
& =\frac{7500+2500+5500+3000}{4} \\
& +\frac{0.45 \times 7500+1.11 \times 2500+0 \times 5500+3.30 \times 3000}{2} \\
& =12650(\mathrm{~N})
\end{aligned}
$$

From the above results, for drilling process with large values, select a model LY 65 from Fig. I-3•4. for $Z$ axis.
The selected linear guides are:

$$
\begin{array}{ll}
X \text { axis } & L Y 55 \\
Y \text { axis } & L Y 35 \\
Z \text { axis } & L Y 65
\end{array}
$$

## (3) Calculation of life expectation

Examination shall be done in three cases, no cutting load; milling process; and drilling process.
Inertial force associated with the starting acceleration is not considered in this case. But it must be calculated for more accurate figures.

## Calculation of the loads that apply to the ball slide

In case of no cutting load: $F \mathrm{x}=F \mathrm{y}=\mathrm{Fz}=\mathbf{0}$
Calculate load on $X, Y, Z$ axes using "Table $I I-3 \cdot 1$ " in "A-II-3.2 (3) Calculating load to a ball slide."
$X$ axis: Loads to consider $W x$, and $W y$
Y axis: Loads to consider Wy
Z axis: Loads to consider $W x, W y$, and $W z$
The table below shows calculation of each load coordinates as stroke end which imposes most strict condition.

Unit: N

| Axis | Load direction | Brg1 | Brg2 | Brg3 | Brg4 |
| :---: | :---: | ---: | ---: | ---: | ---: |
|  | Vertical direction $F_{\mathrm{r}}$ | 1156 | 955 | 4045 | 3844 |
|  | Lateral direction $F_{\mathrm{s}}$ | 0 | 0 | 0 | 0 |
| Y Y axis | Vertical direction $F_{\mathrm{r}}$ | 122 | -122 | 122 | -122 |
|  | Lateral direction $F_{\mathrm{s}}$ | 102 | -102 | 102 | -102 |
| Z axis | Vertical direction $F_{\mathrm{r}}$ | 765 | 3860 | 3890 | 6985 |
|  | Lateral direction $F_{\mathrm{s}}$ | 0 | 0 | 0 | 0 |

In case of milling process: $\mathbf{F x}=\boldsymbol{F y}=1000$ ( N )
Similarly,
$X$ axis: Loads to consider $W x, W y, F x$, and $F y$
Y axis: Loads to consider $W \mathrm{y}, \mathrm{Fx}$, and Fy
$Z$ axis: Loads to consider $W x, W y, W z, F x$, and Fy

The table below shows calculation of each load coordinates as stroke end which imposes most strict condition.

Unit: N

| Axis | Load direction | Brg1 | Brg2 | Brg3 | Brg4 |
| :---: | :---: | ---: | ---: | ---: | ---: |
|  | Vertical direction $F_{\mathrm{r}}$ | 2277 | -1039 | 6539 | 3224 |
|  | Lateral direction $F_{\mathrm{s}}$ | 997 | -997 | 997 | -997 |
| Y Y axis | Vertical direction $F_{\mathrm{r}}$ | 252 | -1040 | 1040 | -252 |
|  | Lateral direction $F_{\mathrm{s}}$ | 54 | -554 | 54 | -554 |
| Z axis | Vertical direction $F_{\mathrm{r}}$ | -771 | 3796 | 4453 | 9020 |
|  | Lateral direction $F_{\mathrm{s}}$ | 486 | -986 | 486 | -986 |

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## In case of drilling process: $\mathbf{F z}=\mathbf{3 0 0 0}(\mathbf{N})$

X axis: Loads to consider $W \mathrm{x}, \mathrm{Wy}$, and $F z$
Y axis: Loads to consider $W y$, and $F z$
$Z$ axis: Loads to consider $W x, W y, W z$, and $F z$

The table below shows calculation of each load coordinates as a stroke end which imposes most strict condition.

Unit: N

| Axis | Load direction | Brg1 | Brg2 | Brg3 | Brg4 |
| :---: | :---: | ---: | ---: | ---: | ---: |
| X axis | Vertical direction $F_{\mathrm{r}}$ | 4256 | 4055 | 945 | 744 |
|  | Lateral direction $F_{\mathrm{s}}$ | 919 | 581 | 919 | 581 |
| Y Y axis | Vertical direction $F_{\mathrm{r}}$ | 305 | 938 | 561 | 1195 |
|  | Lateral direction $F_{\mathrm{s}}$ | 102 | -102 | 102 | -102 |
| Z axis | Vertical direction $F_{\mathrm{r}}$ | 4872 | -247 | 7997 | 2878 |
|  | Lateral direction $F_{\mathrm{s}}$ | 839 | -839 | 839 | -839 |

## Calculation of dynamic equivalent load

Next, find dynamic equivalent load under each cutting condition. From "Table II-3•2" in
"A-II-3.2 (4) Calculation of dynamic equivalent load," necessary load Fr, Fse are, as the linear guide model is LY Series, obtained as follows.

## Vertical dynamic equivalent load

$\mathrm{Fr}=\mathrm{Fr}$
Lateral dynamic equivalent load

$$
F s e=F s \cdot \tan \alpha=F s
$$

From above, calculate Fe using formulas for full dynamic equivalent loads shown in Page A136. From calculation, the largest full dynamic equivalent loads are as follows.

|  | Largest full dynamic equivalent load Fe (N) |  |  |
| :---: | :---: | :---: | :---: |
|  | No cutting load | For milling process | For drilling process |
| X axis | 4045 | 7038 | 4716 |
| Y axis | 173 | 1317 | 1246 |
| Z axis | 6985 | 9513 | 8417 |

## Calculation of mean effective load

Calculate the mean effective loads from full dynamic equivalent loads. If duty cycle in the cutting process is not clear, set at $70 \%$ of the largest full dynamic equivalent load in all
processes.Therefore,
X axis: $7038 \times 0.7=4927(\mathrm{~N})$
Y axis: $1317 \times 0.7=922(\mathrm{~N})$
Z axis: $9513 \times 0.7=6659$ ( N )

## Determine various coefficients

Determine based on "A-II-3.2 (6) Various coefficients."
In this occasion,
Load coefficient $\quad f_{\mathrm{w}}: 1.5$
Hardness coefficient $f_{H}: 1$

## Calculation of rating life

Based on the calculated loads and various coefficients, calculate life from "A-II-3.2 (7)
Calculation of rating life."
Basic dynamic load rating C
(X axis linear guide LY 55): 79500 ( N )
Basic dynamic load rating $C$
(Y axis linear guide LY 35): 35000 ( N )
Basic dynamic load rating C (Z axis linear guide LY 65): 168000 (N)
Load coefficient $\quad f_{w}$ : 1.5
Hardness coefficient $f_{H}: 1$
Rating fatigue life $L=50 \times\left(\frac{f_{\mathrm{H}} \cdot C}{f_{\mathrm{W}} \cdot F_{\mathrm{M}}}\right)^{3}$
From this,
In case of $X$ axis $L x=62235(\mathrm{~km})$
In case of $Y$ axis $\quad L y=810415(k m)$
In case of $Z$ axis $\quad L \mathbf{Z} \mathbf{2 3 7 9 0 0}(\mathrm{~km})$

Examination of static loads based on "A-II-3.2 (8)" Basic static load rating $C_{0}$
( X axis linear guide LY 55): 113000
Basic static load rating $C_{0}$
(Y axis linear guide LY 35): 51000 ( N )
Basic static load rating $C_{0}$
(Z axis linear guide LY 65): 226000 ( N )
Examine for milling process with large load.
X axis $f_{\mathrm{s}}=\frac{C_{0}}{P_{0}}=\frac{C_{0}}{\left(F_{\mathrm{r}}+F_{\mathrm{s}}\right)}=\frac{113000}{(6539+997)}=15.0$
Similarly,
$Y$ axis $f_{s}=32.0$
$Z$ axis $f_{s}=22.6$
Therefore, there is no problem.

## (4) Selection of accuracy grade and preload

For machining center, select accurate grade P5, and Preload Z3.

## (5) Calculation of deformation

Calculate deformation at processing points (stroke position is the stroke end positions on Y axis and X axis)
Rigidity of $X$ axis linear guide LY55Z3: $880(\mathrm{~N} / \mu \mathrm{m})$ Rigidity of Y axis linear guide LY35Z3: $580(\mathrm{~N} / \mu \mathrm{m})$ Rigidity of $Z$ axis linear guide LY65Z3: $1340(\mathrm{~N} / \mu \mathrm{m})$

Calculate using Pattern 4 in Table II-3•1.

| Load conditions | Deformation <br> direction | Deformation of each axis $(\mu \mathrm{m})$ |  |  | Total deformation <br> $(\mu \mathrm{m})$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Y axis | Z axis | -4.9 |  |
| Table weight <br> alone | $\delta \mathrm{x}$ | -0.7 | -0.1 | -4.1 | -15.0 |
|  | $\delta \mathrm{y}$ | -7.4 | -0.5 | -7.1 | -13.2 |
|  | $\delta \mathrm{z}$ | -6.8 | -0.1 | -6.3 | -26.2 |
| Milling process | $\delta \mathrm{x}$ | -15.8 | -1.8 | -8.6 | -22.2 |
|  | $\delta \mathrm{y}$ | -10.2 | -2.5 | -9.5 | -19.0 |
|  | $\delta \mathrm{z}$ | -9.8 | -0.5 | -8.7 | -7.8 |

Therefore, deformation at processing points at time of milling is:
$\delta \mathrm{x}=-26.2-(-4.9)=-21.3(\mu \mathrm{~m})$
$\delta y=-22.2-(-15.0)=-7.2(\mu \mathrm{~m})$
$\delta z=-19.0-(-13.2)=-5.8(\mu \mathrm{~m})$

Deformation at processing points at time of milling:
$\delta \mathrm{x}=-7.8-(-4.9)=-2.9 \quad(\mu \mathrm{~m})$
$\delta y=5.3-(-15.0)=-20.3(\mu \mathrm{~m})$
$\delta z=-21.5-(-13.2)=34.7(\mu \mathrm{~m})$

If a life of this long period is not required, select a smaller linear guide model, and calculate life again.
To reduce deformation at processing point, select a linear guide model with higher rigidity. Then $\mathbf{A}$ calculate life again.

## A-II-11 References

The articles in "Motion \& Control (NSK Technical J ournals)" which refer to NSK linear guides are listed in the table below for user convenience.
"Motion \& Control" is compiled to introduce NSK products and its technologies.
For inquiries and orders of "Motion \& Controls," please contact your local NSK sales offices, or representatives.

Table II-11•1 Motion \& Control (NSK Technical J oumal): Articles relating to linear guides (1997 ~)

| Issue No. | Date of Publication | Articles related to linear guides |
| :---: | :---: | :--- |
| No.1 | Sep/96 | The Current State of Precision Machinery Parts and Product |
| No.2 | Mar/97 | Development of "M olded Oil" and Its Application to NSK Linear Guide |
| No. 3 | Dec/97 | NSK Linear Guide Interchangeable Miniature Series (Product introduction) |
| No.4 | May/98 | New LA Series Linear Guide (Product intriduction) |
| No.5 | Nov/98 | Recent Technical Trends in Linear Guides |

# A- III Other Linear Rolling 

 Guide Products
## A-III-1 Linear Rolling Bushing

## A-III-1.1 Features

## (1) Low friction

Low friction owes to its design: Balls come into point contacts with raceway surface: the balls smoothly re-circulate. There is very little stick slip.

## (2) Low noise

Noise level is low due to the ball retainer which is made of a synthetic resin.

## (3) High precision

Due to NSK's superb quality control, precision is guaranteed.

## (4) Dust prevention

Series with seal is available. The seal has small friction, and is highly durable. Highly dustpreventive double-lip system has been adopted.

## (5) Superb durability

The material of outer sleeve is vacuum degassed, highly pure, and is heat-treated with good expertise.

## A-II-1.2 Models

There are three models

## (1) Standard type LB (Fig. III-1•1)

This model is the most commonly used, and is the only model that comes with a seal and in super precision grade.


Fig. III-1•1 Standard type LB

## (2) Adjustable clearance type LB-T (Fig. III-1•2)

A part of the outer sleeve is cut open toward the axial direction. Used with a housing which can adjust inside diameter, it makes minute adjustment of the clearance between the linear shaft and the inscribed circle (an imaginary circle that connects the summit of the ball) of linear rolling bushing.


Fig. III-102 Adjustable Clearance type LB-T

## (3) Open type LB-K (Fig. III-1•3)

A cut is made in the outer sleeve and retainer, to a width equivalent to one row of the retainer, to the axial direction. The opening is used to hold this linear rolling bushing by a support or base to prevent a long linear shaft from bending.


Fig. III-1॰3 Open type LB-K

## A-II-1.3 Accuracy

## (1) Accuracy grades

- Standard type LB High precision grade S, and super precision grade SP are available
- Space adjustment type LB-T \}High precision grade $S$ is available


## (2) Tolerance of rolling linear bushing, linear shaft and housing

Table III-1•1 Tolerance for inscribed circle of the linear rolling bushing and shaft diameter

| Nominal dimension/ inscribed circle diameter / shaft diameter (mm) |  | Tolerance / inscribed circle diameter ${ }^{(1)}$ |  |  |  | Tolerance / width BHigh precision grade SSuper high precision grade SP |  | Tolerance//slot distance <br> of retaining rings Bn$\|$High receision grade S <br> Super high precision grade SP |  | Recommended tolerance / shaft diameter |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | High precision grade S |  | Super high precision grade SP |  |  |  | High grā | $\begin{aligned} & \text { cision } \\ & \text { S } \end{aligned}$ | Super high grad | $\begin{aligned} & \text { precision } \\ & \text { eSP } \end{aligned}$ |
| over | or less | upper | lower | upper | lower | upper | lower |  |  | upper | lower | upper | lower | upper | lower |
| 2.5 | 6 |  |  |  |  |  |  |  |  | -6 | -14 | -4 | -9 |
| 6 | 10 | 0 | -8 | 0 | -5 |  |  |  |  | -6 | -15 | -4 | -10 |
| 10 | 18 |  |  |  |  | 0 | -120 | +240 | -240 | -6 | -17 | -4 | -12 |
| 18 | 30 | 0 | -10 | 0 | -6 |  |  |  |  | -6 | -19 | -4 | -13 |
| 30 | 50 | 0 | -12 | 0 | -8 |  |  |  |  | -7 | -23 | -5 | -16 |

Table III-1•2 Tolerance of linear rolling bush outside diameter, and housing inside diameter
Unit: $\mu \mathrm{m}$

| Nominal dimension / outside diameter / housing inside diameter (mm) |  | Tolerance / outside diameter $\mathrm{D}^{(1)}$ |  |  |  | ccentricity ${ }^{(2)}$ | Tolerance / housing inside diameter |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | High precision grade S |  | Super high precision grade SP |  | Super high precision grade SP | High precision grade S |  | Super high precision grade SP |  |
| over | or less | upper | lower | upper | lower | Maximum | upper | lower | upper | lower |
| 2.5 | 6 |  |  |  |  |  | +12 | 0 | +8 | 0 |
| 6 | 10 | 0 | -10 | 0 | -7 | 8 | +15 | 0 | +9 | 0 |
| 10 | 18 |  |  |  |  |  | +18 | 0 | +11 | 0 |
| 18 | 30 | 0 | -12 | 0 | -8 | 9 | +21 | 0 | +13 | 0 |
| 30 | 50 | 0 | -14 | 0 | -9 | 10 | +25 | 0 | +16 | 0 |

Notes: (1) For adjustable clearance type and open type, figures indicate tolerances before the cut is made.
(2) Eccentricity means the run-out of offset between the centers of outer sleeve diameter and inscribed circle diameter.

## A-II-1.4 Composition of Reference Number



## A-III-1.5 Lubrication and Friction

## (1) Grease lubrication

## (1) Supply in initial stage

At time of delivery, the linear rolling bushing has a coat of rust preventive agent. Wipe it off with clean kerosene or organic solvent. Dry with an air blower, etc., then apply grease.
Lithium soap based greases with consistency level of 2 are generally used (e.g. NSK Grease No. 1, No. 2, Albania No. 2).

## Replenishment

- Sealed linear rolling bushing is designed to be a disposal item. Therefore, a replenishing grease is considered to be not required. However, if replenishment becomes necessary due to dirty environment or wear of the seal, remove the linear bushing from the shaft and replenish lubricant in the same manner as the initial lubricating.
- For items without seal, wipe off old grease from the linear shaft, and apply new grease.
- Intervals of replenishments is every 100 km in an dirty environment, 500 km in a slightly dirty environment, $1,000 \mathrm{~km}$ or no replenishing for a normal environment.


## (2) Oil lubricantion

It is not necessary to wash off the rust preventive agent applied before delivery.
Use an oil of ISO viscosity grade VG15-100. Drip the oil on the linear shaft by an oil supply system.

Temperature to use
$-30^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$ Viscosity VG15-46
$50^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$ Viscosity VG46-100
Lubricant is removed by the seal if the linear ball bearing has a seal. Therefore, the drip method cannot be used except for single-seal types.

## (3) Friction coefficient

The linear rolling bushing has a small dynamic friction coefficient. This contributes to low power loss and temperature rise.
Fig. III- $4 \bullet 1$ indicates dynamic friction coefficient is merely $0.001-0.004$. Also, at the speed of under 60 $\mathrm{m} / \mathrm{min}$, there is no danger for the temperature rise. Friction force can be obtained by the following formula.

$$
\begin{equation*}
F=\mu \bullet P \tag{1}
\end{equation*}
$$

In this formula:
$F$ : Friction force ( N )
$P$ : Load (vertical load to the shaft center line) ( N )
$\mu$ : Friction coefficient (dynamic or static)
For a seal type, a seal resistance of $0.3 \sim 2.40 \mathrm{~N}$ is added to the above.


Fig. III-14 Dynamic friction coefficient of linear rolling bushing

## A-III-16 Range of Conditions to Use

Generally, use under the following conditions.
Please consult NSK when values below exceed these ranges.
Temperature $\cdots$. Minus $30^{\circ} \mathrm{C}$ to plus $80^{\circ} \mathrm{C}$
Speed .......... Up to $120 \mathrm{~m} / \mathrm{min}$
(excluding oscillation and short strokes)

## A-III-107 Preload and Rigidity

The linear rolling bushing is normally used without applying preload. If high positioning accuracy is required, set the clearance between the linear rolling bush and the shaft at the range of $0 \sim 5 \mu \mathrm{~m}$. Slight preload is a general rule ( $1 \%$ of basic dynamic load rating $C$-- see the dimension table).
The dimension table shows theoretical rigidity $K$ when clearance with the shaft is zero, and a load of 0.1 C is applied to the summit of the ball.

Rigidity $K_{\mathrm{N}}$, when load is not 0.1C, is obtained by the following formula.

$$
\begin{equation*}
K_{N}=K(P / 0.1 \mathrm{C})^{1 / 3} \tag{2}
\end{equation*}
$$

In this formula:
$K$ : Rigidity value in the dimension table ( $\mathrm{N} / \mu \mathrm{m}$ )
$P$ : Radial load ( N )
When the load is applied between the ball raws, the load becomes 1.122 times for 4 ball rows; 0.959 times for 5 ball rows; 0.98 times for 6 ball rows.

## A-III-1.8 Basic Load Rating and Rated Life

## (1) Basic dynamic load rating

Basic dynamic load rating C is: A radial load which allows $90 \%$ of a group of linear rolling bush to run a distance of 50 km without suffering damage when they are moved individually.
There is a relationship as below between C and the life

$$
\begin{equation*}
L=50 f L^{3} \tag{3}
\end{equation*}
$$

$f_{\mathrm{L}}=C / P$
In this formula:
$L$ : Rated life (km)
$P$ : Radial load (kgf)
$f_{\mathrm{L}}$ : Life factor (Refer to Fig. III-1•5)
This formula is used provided that the shaft rigidity is HRC58 or higher. Rated life is shorter if the shaft is softer. In this case, find the hardness factor $f_{\mathrm{H}}$ from Fig. III-1•6, and multiply the value.

$$
\begin{equation*}
f_{\mathrm{L}}=C \cdot H / P \tag{5}
\end{equation*}
$$

Or

$$
\begin{equation*}
C=P \cdot f_{\mathrm{L}} / f_{\mathrm{H}} \tag{6}
\end{equation*}
$$

Life in time can be obtained by the following formula, substituting for given stroke length, cycle numbers, and running distance:

$$
\begin{equation*}
L_{n}=(L / 1.2 \cdot S \cdot n) \times 10^{4} \tag{7}
\end{equation*}
$$

In this formula:
$L_{n}$ : Life hours (h)
$L$ : Rated life (km)
$S$ : Stroke (mm)
$n$ : Cycles per minute (cpm)


Fig. III-15 Relationship between life factor and running distance


Fig. III-16 Hardness factor

## (2) Basic static load rating

It is a load that the total permanent deformation of outer sleeve, ball and shaft, at the contact point, becomes $0.01 \%$ of the ball diameter when this load is applied to the rolling bushing. It is understood in general that this is the applicable load limit which causes this much permanent deformation, nevertheless not hampering operation.

## (3) Calculation example

What is the appropriate rolling bushing size if required life is 5,000 hours?
Conditions are:

- Three linear rolling bushings are installed in two parallel shafts, and support a reciprocating table.
- Load 450 N is equally distributed to the three bushings.
- The table is required to reciprocate on the shafts at 200 times per minute, at a stroke of 70 mm .
- Hardness of the shaft: HRC 55

$$
450 / 3=150(\mathrm{~N})
$$

- Load per linear rolling bushing is:

From Formula (7), the required life, when indicated in distance, is:

From Fig. 5 and Fig. 6,
Life factor $f_{\mathrm{L}}=5.6$
Hardness factor $f_{H}=0.65$
Therefore, from Formula (6),

$$
\begin{aligned}
C & =P \times f_{\mathrm{L}} / f_{\mathrm{H}} \\
& =150 \times 5.6 / 0.65=1292(\mathrm{~N})
\end{aligned}
$$

Based on the above, select linear rolling bushing LB30NY with shaft diameter of 30 mm , basic dynamic load rating of 1400 N .

## (4) Compensating load rating by ball raw (circuit) position

Load rating of the linear rolling bushing changes by the position of the ball circuit rows.
Permissible load is larger when it is applied to the middle of the ball circuit rows than when it is applied directly above the ball row (Fig. III-1•7).
(Radial clearance set at zero in this case.)
Load ratings in the dimension table are in case "A" when it is applied directly above the ball circuit row. If used as in case "B," the load rating becomes larger (Refer to Fig. III-1•7).
$L=5 \times 10^{3} \times 1.2 \times 70 \times 200 / 10^{4}=8.4 \times 10^{3}(\mathrm{~km})$


Fig. III-1.7 Increasing rate of load rating by position of ball row (B/A)

## A-III-1.9 Shaft Specification

Harden the shaft surface, where the balls run, with heat treatment to provide the following values.
-Surface hardness .................... HRC58 or over

- Depth of core hardness at HRC50 or higher

Depth for LB3; 0.3 mm or deeper
Depth for LB50; 1.2 mm or deeper
Roughness of the surface should be:

- For SP grade, and "the clearance for fit" with the ball bushing less than $5 \mu \mathrm{~m}$ -

Less than 0.8 S

- For SP grade with "the clearance" of more than $5 \mu \mathrm{~m}$, and for S grade -

Less than 1.2 S
Bending should be:

- LB3 -- $15 \mu \mathrm{~m} / 100 \mathrm{~mm}$
-LB50 -- $100 \mu \mathrm{~m} / 1000 \mathrm{~mm}$
An appropriate clearance for normal use conditions can be obtained when the tolerance in shaft diameter remains within the recommended range (refer to Table III-1•1 in Page A186). For operations which require particular accuracy, select the shaft diameter which creates a clearance in the range of $0 \sim 0.005$ ( mm ) for example, when assembled with the rolling bushing.


## A-II-1.10 Dust Proof

Select a linear rolling bushing with seals to prevent moisture or foreign matters, which are floating in the air, from entering.

## A-II-1.11 Installation

## (1) Combination of shaft and linear rolling bushing

When the linear rolling bushing is installed in a linear motion table for its reciprocating movement, it is necessary to prevent the table from rotating.
In general, for this reason, two shafts, installed with two linear rolling bushings on each, are used.
Fig. III- $1 \cdot 8$ is an installation example.


Fig. III-188 Installation example

## (2) Installation of linear rolling bushing

(1) Standard type installation

Fig. III $-1 \cdot 9$ shows a method using a retainer ring. Linear rolling bushing can also be secured to the housing using a stop plate and/or screw.


Retaining ring method (1)


Retaining ring method (2)
Fig. III-149 Installation using retaining rings
(a) Housing inside diameter should be of a recommended value ITable III-1•2, Page A186I. The entire rolling bushing contracts and gives excessive preload if: the inside diameter is small ; the roundness or cylindricity is excessive. This may result in an unexpected failure.
(b) To install linear rolling bushing, use a tool (Fig. III$1 \cdot 10$ ) and squeeze it in, or use a holder and lightly pound it.


Fig. III-1-10 Tool to install a linear rolling bushing

## (2) Installation of adjustable clearance type

Use a housing which can adjust the inside diameter of the rolling bushing. This way, the clearance between the rolling bushing and the linear shaft can be easily adjusted. Arrange the cut-open section of the rolling bushing at a 90 -degree angle to the housing's cut-open section. This is the most effective way to evenly distribute deformation toward circumferential direction.
The tolerance of shaft diameter of the adjustable clearance type should be within the recommended range (Refer to Table III-1.1 in Page A186). As a general rule, set the preload at slight or light volume. (Do not provide excessive preload.) Use a dial gauge to measure and adjust clearance. However, here is an easy method to adjust .
First, loosen the housing until shaft turns freely. Then narrow the clearance gradually. Stop at the point when the shaft rotation becomes heavy. This creates a clearance zero or light preload.

## (3) Installation of open type

Use with clearance or with light preload.
Keep the tolerance in shaft diameter within the recommended range (Refer to Table III-1.1 in Page A186I, so the preload shall not become excessive.
(Unlike the adjustable clearance type, clearance cannot be narrowed by rotating the shaft because the state of shaft rotation does not indicate how narrow the space has become. Narrowing clearance requires caution for open type.)


Fig. III-1•11 Installation example of an open type

## (3) Precaution for installing a shaft in the linear rolling bushing

(a) To install two shafts parallel to each other, first install one shaft accurately. Use this as a reference, and install the other parallel to the first shaft. This makes installation easy.
(b) Do not incline the shaft when inserting it into the linear rolling bushing. Do not force it to enter by twisting it. This deforms the retainer, and causes the balls to fall out.
(c) Do not use the shaft for rotating movement after the shaft is in the linear rolling bushing. The balls slip and damage the shaft.
(d) Do not twist the shaft after it is in the linear rolling bushing. The pressure scars the shaft.

## A-III-1.12

Model LB (standard type), no seal


Section $A-A$

Unit: mm

| Model No. | Inscribed circle diameter $F_{\mathrm{w}}$ | Outside diameter$D$ | LengthB | Retaining ring groove |  |  | Stiffness ${ }^{(1)}$ <br> $\mathrm{N} / \mu \mathrm{m}$ [Kgf $/ \mu \mathrm{m}$ ] | Number of ball circuit | Weight (kg) (Reference only) | Basic dynamic load rating C N[kgf] | Basic static load rating Co $\mathrm{N}[\mathrm{kgf}]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Distance <br> $B_{n}$ | With $m$ | Bottom diameter $D_{n}$ |  |  |  |  |  |
| LB3Y | 3 | 7 | 10 | - | - | - | 3 [0.32] | 4 | 0.0016 | 20 [2] | 39 [4] |
| LB4Y | 4 | 8 | 12 | - | - | - | 4.5 [0.47] | 4 | 0.0022 | 29 [3] | 59 [6] |
| LB6NY | 6 | 12 | 19 | 11 | 1.15 | 11.5 | 7 [0.72] | 4 | 0.0074 | 74 [7.5] | 147 [15] |
| (2)LB8ANY | 8 | 15 | 17 | 9 | 1.15 | 14.3 | 5.5 [0.56] | 4 | 0.0094 | 78 [8] | 118 [12] |
| LB8NY | 8 | 15 | 24 | 15 | 1.15 | 14.3 | 9.5 [0.99] | 4 | 0.014 | 118 [12] | 226 [23] |
| LB10NY | 10 | 19 | 29 | 19 | 1.35 | 18 | 12 [1.2] | 4 | 0.025 | 206 [21] | 355 [36] |
| LB12NY | 12 | 21 | 30 | 20 | 1.35 | 20 | 13 [1.3] | 4 | 0.028 | 265 [27] | 500 [51] |
| LB13NY | 13 | 23 | 32 | 20 | 1.35 | 22 | 13 [1.3] | 4 | 0.040 | 294 [30] | 510 [52] |
| LB16NY | 16 | 28 | 37 | 23 | 1.65 | 26.6 | 14 [1.4] | 4 | 0.063 | 440 [45] | 635 [65] |
| LB20NY | 20 | 32 | 42 | 27 | 1.65 | 30.3 | 19 [1.9] | 5 | 0.088 | 610 [62] | 1010[103] |
| LB25NY | 25 | 40 | 59 | 37 | 1.9 | 38 | 35 [3.6] | 6 | 0.267 | 1000 [102] | 1960[200] |
| LB30NY | 30 | 45 | 64 | 40 | 1.9 | 42.5 | 41 [4.2] | 6 | 0.305 | 1400 [143] | 2500[255] |
| LB35NY | 35 | 52 | 70 | 45 | 2.2 | 49 | 48 [4.9] | 6 | 0.440 | 1510 [154] | 2800 [286] |
| LB40NY | 40 | 60 | 80 | 56 | 2.2 | 57 | 54 [5.5] | 6 | 0.520 | 2230 [227] | 4000[410] |
| LB50NY | 50 | 80 | 100 | 68 | 2.7 | 76.5 | 69 [7.0] | 6 | 1.770 | 4100 [420] | 7100[725] |

Note (1): Refer to Section III-1•7.
(2): Semi-standard item of which length $B$ is shorter than standard.

## Model LB (standard type), with seal



Section $A-A$

Unit: mm

| ${ }^{(1)}$ Model No. | Inscribed circle diameter $F_{w}$ | Outside diameter <br> D | Length <br> B | Retaining ring groove |  |  | Number of ball circuit | Weight (kg) (Reference only) | Basic dynamic load rating C $\mathrm{N}[\mathrm{kgf}]$ | Basic static load rating Co N[kgf] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Distance <br> $B_{n}$ | With m | Bottom diameter $D_{n}$ |  |  |  |  |
| LB6NYDD | 6 | 12 | 19 | 11 | 1.15 | 11.5 | 4 | 0.0074 | 74 [7.5] | 147 [15] |
| LB8ANYDD | 8 | 15 | 17 | 9 | 1.15 | 14.3 | 4 | 0.0094 | 78 [8] | 118 [12] |
| LB8NYDD | 8 | 15 | 24 | 15 | 1.15 | 14.3 | 4 | 0.014 | 118 [12] | 226 [23] |
| LB10NYDD | 10 | 19 | 29 | 19 | 1.35 | 18 | 4 | 0.025 | 206 [21] | 355 [36] |
| LB12NYDD | 12 | 21 | 30 | 20 | 1.35 | 20 | 4 | 0.028 | 265 [27] | 500 [51] |
| LB13NYDD | 13 | 23 | 32 | 20 | 1.35 | 22 | 4 | 0.040 | 294 [30] | 510 [52] |
| LB16NYDD | 16 | 28 | 37 | 23 | 1.65 | 26.6 | 4 | 0.063 | 440 [45] | 635 [65] |
| LB20NYDD | 20 | 32 | 42 | 27 | 1.65 | 30.3 | 5 | 0.088 | 610 [62] | 1010 [103] |
| LB25NYDD | 25 | 40 | 59 | 37 | 1.9 | 38 | 6 | 0.267 | 1000[102] | 1960 [200] |
| LB30NYDD | 30 | 45 | 64 | 40 | 1.9 | 42.5 | 6 | 0.305 | 1400[143] | 2500 [255] |
| LB35NYDD | 35 | 52 | 70 | 45 | 2.2 | 49 | 6 | 0.440 | 1510[154] | 2800 [286] |
| LB40NYDD | 40 | 60 | 80 | 56 | 2.2 | 57 | 6 | 0.520 | 2230[227] | 4000 [410] |
| LB50NYDD | 50 | 80 | 100 | 68 | 2.7 | 76.5 | 6 | 1.770 | 4100[420] | 7100 [725] |

Note (1) Single-seal type is indicated as LB-D.

## Model LB-T (Adjustable clearance type)



Section $A-A$

Unit: mm

| Model No. | Inscribed circle diameter $F_{\text {w }}$ | Outside diameter$D$ | Length$B$ | Opening width E | Retaining ring groove |  |  | Number of ball circuit | Weight (kg) <br> (Reference only) | Basic dynamic load rating C N[kgf] | Basic static load rating Co N[kgf] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Distance <br> $B_{n}$ | With <br> m | Bottom diameter $D_{n}$ |  |  |  |  |
| LB6NTY | 6 | 12 | 19 | 0.8 | 11 | 1.15 | 11.5 | 4 | 0.0073 | 74 [7.5] | 147 [15] |
| LB8ANTY | 8 | 15 | 17 | 1 | 9 | 1.15 | 14.3 | 4 | 0.0093 | 78 [8] | 118 [12] |
| LB8NTY | 8 | 15 | 24 | 1 | 15 | 1.15 | 14.3 | 4 | 0.014 | 118 [12] | 226 [23] |
| LB10NTY | 10 | 19 | 29 | 1.5 | 19 | 1.35 | 18 | 4 | 0.025 | 206 [21] | 355 [36] |
| LB12NTY | 12 | 21 | 30 | 1.5 | 20 | 1.35 | 20 | 4 | 0.028 | 265 [27] | 500 [51] |
| LB13NTY | 13 | 23 | 32 | 1.5 | 20 | 1.35 | 22 | 4 | 0.040 | 294 [30] | 510 [52] |
| LB16NTY | 16 | 28 | 37 | 1.5 | 23 | 1.65 | 26.6 | 4 | 0.062 | 440 [45] | 635 [65] |
| LB20NTY | 20 | 32 | 42 | 2 | 27 | 1.65 | 30.3 | 5 | 0.087 | 610 [62] | 1010[103] |
| LB25NTY | 25 | 40 | 59 | 2 | 37 | 1.9 | 38 | 6 | 0.265 | 1000[102] | 1960[200] |
| LB30NTY | 30 | 45 | 64 | 2 | 40 | 1.9 | 42.5 | 6 | 0.302 | 1400[143] | 2500[255] |
| LB35NTY | 35 | 52 | 70 | 3 | 45 | 2.2 | 49 | 6 | 0.44 | 1510[154] | 2800[286] |
| LB40NTY | 40 | 60 | 80 | 3 | 56 | 2.2 | 57 | 6 | 0.52 | 2230[227] | 4000[410] |
| LB50NTY | 50 | 80 | 100 | 3 | 68 | 2.7 | 76.5 | 6 | 1.75 | 4100[420] | 7100[725] |

## Model LB-K (Open type)



Section $A-A$

Unit: mm

| Model No. | Inscribed circle diameter $F_{\mathrm{w}}$ | Outside diameter <br> D | Length$B$ | Opening width $E_{1}$ | Opening angle $\theta$ | Retaining ring groove |  |  | Number of ball circuit | Weight (kg) (Reference only) | Basic dynamic load rating C N[kgf] | Basic static load rating Co N[kgf] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Distance <br> $B_{n}$ | Width <br> m | Bottom diameter $D_{n}$ |  |  |  |  |
| LB20NKY | 20 | 32 | 42 | 11 | 60 | 27 | 1.65 | 30.3 | 4 | 0.072 | 610 [62] | 1010[103] |
| LB25NKY | 25 | 40 | 59 | 13 | 50 | 37 | 1.9 | 38 | 5 | 0.220 | 1000[102] | 1960[200] |
| LB30NKY | 30 | 45 | 64 | 15 | 50 | 40 | 1.9 | 42.5 | 5 | 0.260 | 1400[143] | 2500[255] |
| LB35NKY | 35 | 52 | 70 | 17 | 50 | 45 | 2.2 | 49 | 5 | 0.370 | 1510[154] | 2800[286] |
| LB40NKY | 40 | 60 | 80 | 20 | 50 | 56 | 2.2 | 57 | 5 | 0.440 | 2230[227] | 4000[410] |
| LB50NKY | 50 | 80 | 100 | 25 | 50 | 68 | 2.7 | 76.5 | 5 | 1.480 | 4100[420] | 7100[725] |

## A-III-2 Crossed Roller Guide

## A-III-2.1 Structure

Rollers with a retainer (hereinafter refer to as "retainer") are assembled in a pair of rails which have a V-shape groove. ( the grooves form a 90-degree angle. Refer to Fig. III-2•1, III-2•2). Rollers are placed crisscrossed, and are able to support load in all directions, including moment loads.


Fig. III-2• Structure of crossed roller guide


Fig. III-2.2 Cross section of a crossed roller guide

## A-III-2.2 Features

## (1) High rigidity

This is attributable to the long contact area between the rollers and their accurately ground rolling surface.

## (2) Superbly smooth movement, low noise

The window which directly embraces the roller is made of plastic for smooth and quiet operation, lowering clatter when the retainer and the rollers come into contact.

## (3) Less micro-slip

Occasionally, a minute continuous slippage of the retainer to one one direction, called "micro-slip," is caused due to installation error of the rail. After years of testing and research, NSK has developed technology to minimize this.

## (4) Easy installation

Installation is easy because the rail bending is
minimal, and the bolt hole pitch for installation is precise.

## (5) Long durability

The material is vacuum-degassed and highly pure, and is hardened by carburized heat treatment for superb resistance to wear and fatigue.

## A-III-2.3 Accuracy

Accuracy grade P5 (super precision and high precision grade P6 are available.
Fig. III $-2 \cdot 3$ shows parallelism of the roller's rolling surface to the mounting datum face.


Fig. III -2•3 Parallelism of the roller rolling surface

## A-III-2.4 Rigidity

The number of the load rollers changes by the direction of the load. This is because the rollers are positioned criss-cross.
That is, in case of Fig. III-2•4:
The number of load rollers $=1 / 2 x$ total roller number
$\qquad$
In case of Fig. III- $2 \cdot 5$ :
The number of load rollers =Total roller number

Fig. III $-2 \cdot 6$ shows changes in elastic deformation when there are 20 load rollers. If the total number of rollers is other than 20, use the graph in Fig. III- $2 \cdot 7$. Obtain the compensation factor which converts the elastic deformation value at time of 20 load rollers into the value when a specific number of rollers are loaded. That is, obtain a compensation factor on ordinates that correspond to the number of load rollers on the abscissa. Then, multiply this factor by the elastic deformation value (on ordinates) which corresponds to the load (on abscissa) shown in Fig. III- $2 \cdot 6$.


Fig. III-24


Fig. III-2 -5

## [ Calculation example: Elastic deformation]

A retainer which contains 30 rollers (roller diameter 6 mm ) is installed on both right and left side (Fig. III-2.8). How large is the elastic deformation of the crossed roller guide when a load of 4 kN is applied to the table center?

## [Answer]

A load of 2 kN is applied to each side of the crossed roller guide. The elastic deformation value on the ordinates which corresponds to the load 2 kN on the abscissa (in Fig. III-26) is:

$$
4.5 \mu \mathrm{~m}
$$

This application of load is the same as in Fig. III$2 \cdot 4$. Therefore, the number of load rollers is onehalf of 30 , or 15 . From Fig. III- $2 \cdot 7$, the compensation factor on the ordinate which corresponds to 15 rollers on abscissa is:
1.3

Multiply 1.3 by $4.5 \mu \mathrm{~m}$ obtained above. The answer is:
$4.5 \times 1.3 \div 6 \mu \mathrm{~m}$


Fig. III-26 Elastic deformation with $\mathbf{2 0}$ rollers


Fig. III-2.7 Compensation factor to obtain elastic deformation


Fig. III-2.8 Example calculation of elastic deformation (illustration)

## A-III-2.5 Friction Force

If installation and lubrication are appropriate, the starting friction coefficient is markedly small as shown below:

$$
\mu=0.005
$$

## A-II-2.6 Lengths of Rail and Retainer

The relationship of rail length $L$ with stroke $S$ is as follows:

$$
\begin{align*}
& \text { When } S \leqq 400 \mathrm{~mm}, L \geqq 1.5 S  \tag{3}\\
& \text { When } S>400 \mathrm{~mm}, L \geqq S \ldots \tag{4}
\end{align*}
$$

Since the retainer travels a distance of half of the stroke, the retainer length K is:

$$
\begin{equation*}
K<L-\frac{S}{2} \tag{5}
\end{equation*}
$$

The retainer does not detach from the rail when condition in Formula (5) is satisfied (Refer to Fig. III-2.9).


Fig. III-2.9 Relationship of rail and retainer

## A-III-2.7 Lubrication and Dust Proof

For grease lubrication, lithium soap based greases of consistency 1 or 2 are used.

For example; NSK Grease No.1, NSK Grease No.2, Albania No. 2 (Shell Petroleum) For oil lubrication, JIS viscosity 32 to 150 is recommended.
When necessary, install a bellows on the rail, or install a seal on the side of the rail to arrest foreign matters and dust as shown in Fig. III-2•10.


Fig. III-2•10 Dust prevention (example)

## A-III-2.8 Installation

Fig. III-2•11 shows the standard installation procedures.
(a) Secure Rail 1 and 2 to the bed using the fixing bolts. . Secure Rail 3 to the table with the bolts. Temporarily secure Rail 4 and loosen the side bolt.
(b) Match the bed and the table. Insert the retainer in the roller space. At this time, measure the distance from the rail end to the retainer end with a depth gauge to determine its position.
If the roller space is too narrow and the retainer does not go inside, slide Rail 4 toward the side bolt, then insert the retainer.
(c) Follow the reading of dial gauge which is previously set, and squeeze in all side bolts until they stop rattling. Do not apply excessive force. When the side bolts are tightened, the rollers should be in the vicinity of the bolt position. Then, secure Rail 4 with the fixing bolts. Finally, install a stopper to the rail end.
(a)

(b)


Fig. III-2•11 Standard installation procedures

## [Regarding preload]

As crossed roller guide has higher rigidity than other linear rolling guides, it does not need preload. It is also difficult to apply preload accurately. Crossed roller guide is usually used without clearance. For highly accurate applications, it is desirable to press the crossed roller guide by means of a bolt over the gib as shown in Fig. III2•12.


Fig. III -2•12 Tightening using a gib

## A-III-2.9 Basic Static Load Rating

Basic static load rating becomes larger in proportion to the number of the load rollers "n." Obtain basic static load rating per roller $C_{010}$. Then the basic static load rating Con when the numbers of rollers is n can be obtained as follows.

$$
\begin{equation*}
C_{0 n}=n \times C_{01} \tag{6}
\end{equation*}
$$

Values of $C_{01}$ are shown in the dimension table.

## A-II-2.10 Basic Dynamic Load Rating and Rated Life

Basic static load rating is based on a rated traveled distance of 50 km . The dimension table shows the value with 20 load rollers. When the number of load rollers is other than 20, a basic dynamic load rating $C_{n}$ can be obtained by multiplying a compensation factor (obtained from Fig. III-2•13.) by C in the dimension table.
(Suffix ' $n$ ' is to refer the number of load rollers.)
As an example; Number of load rollers: $\mathrm{n}=15$.
The compensation factor from Fig. III-2•13 is 0.8 .

$$
C_{15}=0.8 \times C
$$

Therefore, $C_{15}$ is obtained from the following formula. Rated life (km) is shown in the formula below. In this formula:

$$
\begin{equation*}
L=50\left(\frac{C_{n}}{f_{\mathrm{w}} \cdot F_{\mathrm{c}}}\right)^{\frac{10}{3}} . \tag{7}
\end{equation*}
$$

$f_{\mathrm{w}}$ : Load factor. $1.0 \sim 1.2$ under smooth operation
$F_{c}$ : Computed load which applies to the guide (kN) Please refer to NSK Linear Guide Technical Description for details.


Fig. III -2•13 Compensation factor for basic dynamic load rating

## A-III-2.11 Reference Number and Standard Set for "One-Axis"

Specifications are indicated as a reference number as shown below.


Note (1) : Semi-standard T, a shape of rail cross section, is available only for CRG04. It is lower in H dimension, and wider in W dimension compared with A .
Remarks : Standard set for "one axis" of the guide refers to 4 rails and 2 retainers which usually comprise the guide way for a one axis.

## A-III-2.12 Dimension Table

## Crossed roller guide: Model CRG




When mounting bolt hole code is $N$


When mounting bolt hole code is D


Unit: mm

| Model No. | $D_{w}$ | W | H | w | C | $E$ | $d$ | $h$ | $d_{1}$ | $d_{2}$ | M | G | F | $t$ | P | $P_{1}$ | $\begin{array}{\|c\|} \hline \text { Dynamic } \\ \text { load rating } \\ \text { Chen } \\ \text { rollers are } \\ 20 \\ N[k g f] \end{array}$ | Static load rating Cor when roller is one N[kgf] |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CRG04...A | 4 | 24 | 12 | 11.3 | 0.5 | 5 | 8 | 4.2 | 4.3 | 5 | M 5x0.8 | 20 | 40 | 2.3 | 6.5 | 3.8 | $\begin{gathered} 9800 \\ {[1000]} \end{gathered}$ | $\begin{aligned} & \hline 665 \\ & \text { [68] } \end{aligned}$ |  | 200300 |
| CRG04...T | 4 | 26 | 10 | 12.3 | 0.5 | 5 | 8 | 4.2 | 4.3 | 5 | M 5x0.8 | 12/15 | 38/40 | 2.3 | 6.5 | 3.8 | $\begin{gathered} 9800 \\ {[1000]} \end{gathered}$ | $\begin{aligned} & \hline 665 \\ & {[68]} \end{aligned}$ |  | 200300 |
| CRG06...A | 6 | 31 | 15 | 14.5 | 0.8 | 6 | 9.5 | 5.2 | 5.2 | 5.5 | M 6x1 | 25 | 50 | 3.2 | 9.5 | 5.8 | $\begin{aligned} & 26700 \\ & {[2720]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 1510 \\ \text { [154 } \\ \hline \end{array}$ |  | 00600 |
| CRG09...A | 9 | 44 | 22 | 20.7 | 1 | 9 | 11 | 6.2 | 6.8 | 7 | M 8x1.25 | 50 | 100 | 4 | 14 | 8 | $\begin{aligned} & 72500 \\ & {[7420]} \\ & \hline \end{aligned}$ | $\begin{array}{r} 3400 \\ {[347]} \\ \hline \end{array}$ |  | 600900 |
| CRG12...A | 12 | 58 | 28 | 27.6 | 1.5 | 12 | 14 | 8.2 | 8.5 | 9 | M10x1.5 | 50 | 100 | 5 | 20 | 12 | $\begin{aligned} & 130000 \\ & {[13300]} \end{aligned}$ | $\begin{aligned} & \hline 6050 \\ & {[616]} \end{aligned}$ |  | 001200 |

Remarks: The area which embraces the roller is plastic for the standard retainer. A solid type made of steel plate is available for high temperature resistance.

## A-III-3 Roller Pack

## A-II-3.1 Structure

A roller pack comprises a main body which supports load from the guide way block via two rows of rollers; an end cap which change the direction of the recirculation of rollers at the end of the main body; a side plate which guides the rollers. (Fig. III-3•1). Roller pack is one of linear rolling guide of which rollers are allowed to re-circulate infinitely for free from restriction of running range (stroke).
There is a plate spring attached to a side of roller pack to prevent roller pack from falling out when it is turned upside down after assembly.
Other component of the roller pack is spring pin. Spring pin is on the top surface of the roller pack, and makes installation of wedge block and fitting plate easier.
Wedge block is a unit to provide preload (Fig. III-3•3) to roller pack; a fitting plate (Fig.III-3•2), functioning like a pivot, adjusts misalignment of roller pack automatically. Wedge of wedge block moves up and


Fig. III-31 Roller pack
down, to apply preload, by turning the adjust screw.


Photo 2 Wedge block


Fig. III-3•2 Fitting plate


Fig. III-3॰3 Wedge block

## A-III-3.2 Features

Roller pack has two remarkable characteristics other linear roller guide bearings do not have.

## (1) No roller skewing

If the roller is long relative to its diameter, the roller inclines during operation. This phenomenon is called skewing. Skewing causes problems such as sudden rise in friction force. However, a short roller lacks large load carrying capacity. The roller introduced here solved the skewing problem, yet has a large load carrying capacity: short rollers are combined into double rows.Load is applied equally.
This is due to a "fitting plate," a result of "changed way of conceiving." Installation is quite easy: Merely place the fitting plate through the two holes to spring pins. The stop pins are inserted to holes on the top surface of the roller pack. The contact area between the fitting plate and the main body is made small. This way, the self-alignment is automatically accomplished by elastic contact of both parts.
This distributes an equal load to the rollers, far extending the life, compared to conventional roller linear guides.
Other characteristics include: Easy to provide preload by the wedge block; can be installed to vertical shaft; and reduction in noise level.

## A-III-3.3 Accuracy

The height tolerance of roller pack is $10 \mu \mathrm{~m}$. Roller packs are grouped into a size difference of every $2 \mu \mathrm{~m}$ (corded by A $\sim$ E) before delivery (Table III-3•1).

Table III-3॰1 Height Classification
Unit: $\mu \mathrm{m}$

| Category | Code |
| :---: | :---: |
| over or less |  |
| $+3 \sim+5$ | A |
| $+1 \sim+3$ | B |
| $-1 \sim+1$ | C |
| $-3 \sim-1$ | D |
| $-5 \sim-3$ | E |

## A-III-3.4 Rigidity

Fig. III-3•4 shows the relationship between load and deformation. This includes deformation caused by contact between: the rollers and main body; the rollers and guide way surface; the main body and fitting plate.


Fig. III-34 Elastic deformation of the roller pack

## A-III-35 Preload

Fig. II- 3.5 shows conversions of tightening torque of the wedge block adjust screw into preload volume. Use a dial gauge for accurate measurement.


Fig. III-35 Tightening torque of the adjust screw, and preload volume

## A-III-3.6 Friction and Lubrication

## (1) Lubricants and volume

Mineral oils are commonly used. Since roller pack is used under a relatively heavy load, the oil should, ideally, have high viscosity and provide a strong film. Select from J IS viscosity 32-150.
Criteria of oil supply per roller pack $Q$ (cc/h) can be calculated by the following formula.

$$
\begin{equation*}
Q \geqq S \times 1 / 4 . \tag{1}
\end{equation*}
$$

In this formula, $S$ (stroke) is shown in meters. The oil volume, when the stroke is 1 m , per roller pack is more than 0.25 (cc/h). It is more desirable to supply a small amount of oil at short intervals than supplying a large amount at one time. In case of grease lubrication, use a grease of consistency 2. Albania EP2 is widely used.

## (2) Friction coefficient

Starting friction coefficient is significantly small at under 0.005 .

## (3) Seal

It is necessary to install a wiper seal to the guide way surface to prevent foreign matters (swarf from cutting, and other dust) from entering to roller pack to enjoy the full benefit of the designed life of it. The material of the seal should have strong resistance to oil and wear. Felt and synthetic rubber (acrylonitril butadiene rubber) are some of the suitable materials.
Fig. III $-3 \bullet 6$ shows a general method to install the seals.


Fig. III-36 Installation of seal

## A-II-3.7 Installation

## (1) Installation and applying preload

As shown in Fig. III-3•7, it is basic that a fitting plate is installed on the roller pack which receives load, and a wedge block is installed on the roller pack which receives no load, but only for preload. All components should be secured with a stop pin, facing toward the direction of movement. To cut costs for processing, it is recommended to divide the pocket (which contains roller pack) into some blocks and secure them with bolts (Fig. III-3•7). Preload is provided by the wedge block. Estimate the actual load beforehand, so the preload shall not be lost when a load is applied. A load variation equivalent to up to two times of the preload volume can be absorbed in this case.
(Take into consideration the life in A-III-3•8 in determining preload volume.)

## (2) Accuracy of way block

The following is the ideal accuracy specification and installation accuracy of way block as a guide face.

Hardness by heat treatment
: More than HRC58 hardened depth 2 mm or more
Surface roughness
: Less than 1.6 S
Parallelism as a single unit: Less than 0.010 mm per meter
Parallelism after installation
: Less than 0.020 mm per meter
Please consult NSK when using cast iron or cast steel guide face.

## (3) Pocket accuracy

Accuracy of the pocket in which the roller pack is mounted should satisfy the following conditions.

Pocket width
: Roller pack width $+0.10 \mathrm{~mm} \sim 0.20 \mathrm{~mm}$ Parallelism of the pocket side faces to the guide way face
: Less than 0.010 mm per 100 mm .
Parallelism of the fitting plate (pocket bottom) mounting face to the guide way face and parallelism of the wedge block mounting face to the guide way face :
: Less than 0.040 mm per 100 mm .


Fig. III-3•7 Design of the roller pack pocket (example)

## A-III-3.8 Rated life

Rated life $\mathrm{L}(\mathrm{km})$ is shown in the following formula. In this formula:

$$
\begin{equation*}
L=50\left(\frac{C}{f_{\mathrm{w}} \cdot F_{\mathrm{c}}}\right)^{\frac{10}{3}} . \tag{2}
\end{equation*}
$$

C : Basic dynamic load rating (kN)
$f_{w}$ : Load factors. 1.0-~1.2 at time of smooth operation
$F_{c}$ : Calculated load (kN) applied to the roller pack

## A-III-3.9 Disassembly

For the roller pack preloaded by the wedge block, remove it in the following manner.

- Loosen the adjust screw of the wedge block. Lightly tap the wedge. In case of light preload, the wedge loosens, and the roller pack can be pulled out.
-When pulling, put the bolt in the tap hole at the end of the end cap, and tug the bolt.
- In case of heavy load, the roller pack could not be pulled out by the above method. Hook a tool to the pull-out hole (Fig. III-3.1) on the side plate of the roller pack, and pull out the roller pack.


## A-III-3.10 Dimension Table

Roller pack: Model WRP


Section A-A
Unit: mm
$\left.\begin{array}{c|c|c|c|c|c|c|c|c|c}\hline \text { Model No. } & \text { Width } & \begin{array}{c}\text { Height } \\ \pm 0.005 \\ H\end{array} & L & \text { Length } & \begin{array}{c}\text { Applicable } \\ \text { fitting plate } \\ \text { reference No. }\end{array} & \begin{array}{c}\text { Assembled } \\ \text { height } \\ H_{1}\end{array} & \begin{array}{c}\text { Applicable } \\ \text { wedge } \\ \text { reference No. }\end{array} & \begin{array}{c}\text { Assembled } \\ \text { height } \\ H_{2}\end{array} & \begin{array}{c}\text { Basic dynamic } \\ \text { load rating } \\ \text { C } \\ \text { N[kgf] }\end{array}\end{array} \begin{array}{c}\text { Basic static } \\ \text { load rating } \\ \text { Co } \\ \mathrm{N}[\mathrm{kgf}]\end{array}\right]$

Remarks : Numbers in the parentheses in column $\mathrm{H}_{2}$ show the adjustable height range of the wedge block.

Fitting plate: Model WFT


Unit: mm

| Model No. | Width <br> $W$ | Height <br> $( \pm 0.01)$ <br> $H$ | Length <br> $L$ | Applicable Roller pack |
| :---: | :---: | :---: | :---: | :---: |

Wedge block: Model WED


Unit: mm

| Model No. | Width <br> $W$ | Height <br> $H$ | Length <br> $L$ | Applicable Roller pack |
| :---: | :---: | :---: | :---: | :---: |
| WED 25 | 23 | $12(11.5 \sim 12.5)$ | 47 | WRP 251907 |
| WED 31 | 28 | $14(13.5 \sim 14.5)$ | 63 | WRP 312609 |
| WED 38 | 35 | $17.47(16.9 \sim 18.1)$ | 76 | WRP 383310 |
| WED 45 | 40 | $20(19.2 \sim 20.8)$ | 95 | WRP 454014 |

Remarks : Numbers in the parentheses in column $\mathrm{H}_{2}$ show adjustable height range of the wedge block.

## A-III-4 Linear Roller Bearings

## A-II-4.1 Structure

Linear roller bearing comprises: A single row of rollers; the main body which supports load via rollers; the end cap which turns the roller recirculating direction at the end of the main body from the loaded zone to the unloaded zone; a retaining wire which prevents rollers from falling out (Fig. III-4•1). The main body, as the cylindrical roller bearing, has a rib at both sides. The rib guides the rollers to travel correctly, and assist the rollers to circulate infinitely in the bearing in a stable manner. This contributes to the bearing's linear movement without the restriction of travel range.
NSK also developed a highly functional preload pad
(Photo 2) to provide a slight preload to the bearing. Basically, the preload pad comprises parallel plates and bellevile springs, which are installed between a parallel plates, and are adjusted its spring rate.
Preloaded pad can be used in a machine tool in the following manner.
When two bearings are installed with one on the top and the other under the way block (the bearings comprise a set), a preloaded pad is used at the bottom bearing. This provides an equal preload to the top and bottom bearings. This way, to a certain extent, the variation in the load and the uneven thickness of the way block can be absorbed.


Fig. III-4•1 Linear roller bearing


Photo 1 Linear roller bearing


Photo 2 Preload pad

## A-III-4.2 Features

In addition to the general features of a roller bearing guide such as no-stick slip, small friction resistance, and easy maintenance, the linear roller bearing has several more advantages.

## (1) No trouble by roller skewing

Skewing is the inclination of the rollers during operation. It causes friction force to suddenly soar. Skewing is apt to occur when the roller is long relative to its diameter. The proportion of the length and diameter is $1: 2$ for the products in this series. This is superior to the commonly used 1:3 ratio.

## (2) Highly reliable

Retaining the rollers without allowing them to fall out bearing is a crucial function of the linear guide bearing. The simple and highly effective retaining wire has solved such problem for this product series.

## (3) Compact design

Despite the load carrying capacity, this series is smaller in size than any other models. This contributes to the application which requires compact design.

## (4) High rigidity

The contact area between the bearing and the mounting surface is large to increase rigidity.

## A-III-4.3 Accuracy

The nominal height difference between bearings is $10 \mu \mathrm{~m}$. The bearings are grouped into every $2 \mu \mathrm{~m}$, and are coded before delivery (Table III-4•1).

Table III-4•1 Classification of height
Unit: $\mu \mathrm{m}$

| Category |  |  | Code |
| :---: | :---: | :---: | :---: |
| over |  | or less |  |
| 0 | $\sim$ | -2 | A |
| -2 | $\sim$ | -4 | B |
| -4 | $\sim$ | -6 | C |
| -6 | $\sim$ | -8 | D |
| -8 | $\sim$ | -10 | E |

## A-II-4.4 Rigidity

Fig. III-4•2 shows elastic deformation.


Fig. III-4-2 Elastic deformation

## A-III-4.5 Friction and Lubrication

## (1) Lubricants and volume

Mineral oils are used in general. The linear roller bearing is used under relatively heavy load. An oil which has high viscosity and creates a strong oil film is ideal for linear roller guides. Select from J IS viscosity 32-150.
General oil supply for a linear roller bearing $Q$ (cc/h) can be calculated by the following formula.

$$
\begin{equation*}
Q \geqq S \times 1 / 4 \tag{1}
\end{equation*}
$$

In this formula, $S$ (stroke) is shown in meters. Therefore, when the stroke is 1 m , the volume of lubricant per roller bearing is more than 0.25 (cc/h). It is recommended to supply a small amount of oil at short intervals rather than supplying a large amount at one time. In case of grease lubrication, a grease of consistency degree 2 , such as Albania EP2, is generally used.

## (2) Friction coefficient

Starting friction coefficient is significantly small at under 0.005 .

## (3) Seal

Install a wiper seal on the way block surface to prevent foreign matters (swarf from cutting, other dust) to realize a full life of the linear roller bearing. The material of the seal should have strong resistance against oil and wear. Felt and synthetic rubber (acrylonitril-butadien rubber) are some of the suitable materials.

## A-III-4.6 Installation

Secure the linear roller bearing using four bolts. The bearing main body has four holes for mounting.

Accuracy of way block
The ideal accuracy specification and mounting accuracy of a way block as a guide way surface are as follows.

Hardness by heat treatment
:M ore than HRC58 hardened depth
2 mm or more
Surface roughness
: Less than 1.6 S
Parallelism as a single unit
:Less than 0.010 mm per 1 m
Parallelism after installation
:Less than 0.020 mm per 1 m
Please consult NSK when using cast iron or cast steel guide way.

## A-II-4.7 Rated life

Rated life $L(\mathrm{~km})$ is shown in the following formula.
In this formula:
$L=50\left(\frac{@ C}{f_{\mathrm{w}} \cdot F_{\mathrm{c}}}\right)^{\frac{10}{3}}$.
C: Basic dynamic load rating (kN)
$f_{\mathrm{w}}$ : Load factor. $1.0 \sim 1.2$ at time of smooth operation
$F_{c}$ : Calculated load applied on the bearing (kN)

## A-III-4.8 Dimension Table

## Linear roller bearing Model: LRB



Unit: mm

| Model No. | Width W | Height $H^{0.010}$ | Length L | $L_{1}$ | Roller Diameter $x$ length | Mounting bolt hole D | Bolt hole distance |  | Basic dynamic load rating C N[kgf] | Basic static <br> load rating Co $\mathrm{N}[\mathrm{kgf}]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | A | $B$ |  |  |
| LRB 14×53 | 26.5 | 14.29 | 52.8 | 32.8 | $\phi 4 \times 8$ | ¢ 3.4 | 19 | 19.3 | $\begin{aligned} & 15400 \\ & {[1570]} \end{aligned}$ | 21900 $[2230]$ |
| LRB 19×69 | 30.5 | 19.05 | 68.6 | 44.6 | $\phi 5 \times 10$ | ¢ 3.4 | 25.4 | 23.3 | 27000 $[2750]$ | $\begin{aligned} & 39000 \\ & {[3960]} \end{aligned}$ |
| LRB 29×92 | 41.5 | 28.58 | 92.0 | 59 | $\phi 7.5 \times 15$ | $\phi 4.5$ | 38.1 | 32.7 | $\begin{aligned} & 57500 \\ & {[5850]} \end{aligned}$ | $\begin{aligned} & 76500 \\ & {[7810]} \end{aligned}$ |
| LRB 38×132 | 51.4 | 38.10 | 132.0 | 88 | $\phi 10 \times 20$ | $\phi 5.5$ | 50.8 | 41.5 | 119000 [12100] | 159000 [16200] |

Remarks: Bearings are grouped into heights of every $2 \mu \mathrm{~m}$ before delivery.

## Preload pad Model: PRP



Unit: mm

| Model No. | Applicable linear <br> roller bearing | Height <br> $($ no-load <br> $h$ max | Compress <br> ed height <br> $h$ min | Load when <br> fully <br> compressed <br> $(N)$ | $W$ | $L$ | $d$ | $a$ | $S$ <br> $b$ <br> Hex. <br> Socket <br> cap screw |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PRP 14 $\times \mathbf{5 3}$ | LRB $14 \times 53$ | 10.23 | 9.53 | 1570 | 26 | 72 | $\phi 4.5$ | 62 | 14 | $\mathrm{M} 3 \times 16$ |
| PRP 19 $\times \mathbf{6 9}$ | LRB $19 \times 69$ | 11.53 | 11.10 | 2650 | 30 | 96 | $\phi 4.5$ | 86 | 18 | $\mathrm{M} 3 \times 19$ |
| PRP 29 $\times \mathbf{9 2}$ | LRB $29 \times 92$ | 13.13 | 12.70 | 6450 | 41 | 120 | $\phi 4.5$ | 110 | 27 | $\mathrm{M} 3 \times 25$ |
| PRP $\mathbf{3 8} \times \mathbf{1 3 2}$ | LRB $38 \times 132$ | 16.28 | 15.88 | 12000 | 51 | 157 | $\phi 4.5$ | 147 | 35 | $\mathrm{M} 5 \times 38$ |

## A-III-5 Cam Follower

## A-III-5.1 Structure and Characteristics

The outer ring of the bearing functions as a rolling ring (Fig. III-5•1). This rolling ring is thick and tough. The rollers are crowned needle rollers, and have a large load carrying capacity. This provides high impact load resistance. The surface of the stud is core-hardened to provide durability against wear, and toughness.


Fig. III-5.1 Structure of Cam follower

## A-III-5.2 Types

## (1) Bearing models

There are four models: With/ without a retainer and oil/grease lubricant (Table III-51).

Table III-5.1. Bearing models

| Bearing model | Description |
| :---: | :--- |
| FCR | Full complement of rollers, no seal <br> (oil is supplied later) |
| FCRS | Full complement of rollers, with seal <br> (grease is sealed in) |
| FCJ S | With retainer, no seal (oil is supplied later) <br> With retainer, with seal (grease is sealed in) |

## (2) Appearances

Specifications of the exterior appearance include: Shape of the slot for the "screw driver" on the end of the stud; With/without an eccentric bush to be secured to the stud; Oil hole; Shape of outer surface of the rolling ring.


Fig. III-5•2 Cam follower with sphere shaped outer surface

Table III-5•2 Exterior appearances

| Deference in appearance | Code for <br> appearance | Description |
| :---: | :---: | :---: |
| Screw driver slot at <br> the end of stud | (no code) | Hole for Philip's screwdriver |
|  | B | Hole for hexagonal socket screw keys |
| secured to the stud | (no code) | No eccentric bush |
| Oil hole | E | With eccentric bush |
|  | (no code) | Simple round hole |
| Rolling ring outer surface | P | Pipe tap for oil hole |
|  | (no code) | Cylindrical shaped outer surface |

## (3) Accessories

A blind plug comes with order. Nut, spring washer, and grease fitting are available on request. Table III$5 \cdot 3$ shows accessory codes.

Table III-53 Accessory codes

|  | Nut | Spring washer | Grease nipple |
| :---: | :---: | :---: | :---: |
| Code | I | N | Z |

## (4) Special products

Please consult NSK for the following items manufactured by NSK.

- Items in inch sizes
- Items with black film coating on exposed surface.
- Items in special shape.


## A-III-5.3 Reference Number for Ordering

Codes for (1) Bearing models, (2) Appearances, (3) Accessories constitute a reference number to be
used in ordering. If accessory is not required, omit codes after the "+" sign.

Reference number composition

Bearing model (Table III-5•1) Appearance (Table III-5•2)
B Bearing $\qquad$
FCR : Full complement rollers, no seal (oil is supplied later)
FCRS : Full complement of rollers, with seal (grease is sealed in)
FCJ : With retainer, no seal (oil is supplied later)
FCJ S : With retainer, with seal (grease is sealed in)

(omitted): Cylindrical outer surface
R: Sphere shaped surface
(sphere radius 500 mm )
Out side diameter (unit: mm)
(omitted): Oil hole (round)
—P: Pipe tap for oil hole
(omitted): No eccentric bush
E: With eccentric bush
(omitted): Hole for Philip's screwdriver
—B: Hexagonal hole for socket head keys
(Example) FCJ SP-16RZ: With retainer and seal (grease is sealed in); Pipe tap for oil hole; Outer diameter 16 mm , its face forms an arc; With grease nipple
FCRS-16-N: Full complement of rollers; With a hole for screwdriver; With eccentric bush; Outer diameter 16 mm ; With spring washer

## A-III-5.4 Accuracy

Table III- 5.4 shows the dimensional tolerances of cam follower.
Running accuracy grade is the same as JIS 0 Grade.
Table III-54 Dimensional tolerance of cam follower
Unit: $\mu \mathrm{m}$

| Model code | Tolerance of stud diameter $\Delta d \mathrm{mp}$ Fit tolerance grade | Variation of single plane mean outside diameter $\Delta D \mathrm{mp}$ |  |  | Variation of outer ring width $\Delta$ Cs |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Cylindrical outer sufface Upper Lower | Sphere-shaped outer sufface |  |  |  |
|  |  |  | Upper | Lower | Upper | Lower |
| FCR, FCRS FCJ, FCJ S | h7 | Same as J IS 0 Grade |  | -50 | Same | Grade |

## A-III-5.5 Permissible Load

## (1) Permissible load of cam follower

Maximum radial load the cam follower can support is determined by the stud strength to bending or shearing force. Maximum values are shown in the dimension table.

## (2) Permissible load of the rail track

Permissible load of the rail track where the bearing ring rolls are determined by the surface hardness, roughness, and state of lubrication of the rail surface. Table III-3.5 shows load factors that correspond to the hardness of the track surface when the surface of the track is lubricated. Multiply the track's permissible load value shown in the dimension table by the coefficient that corresponds to the hardness. Hardness of HRC40 is the standard for these values.

Table III-5.5 Permissible load factor of the track

| Hardness <br> (HRC) | Load factor |
| :---: | :---: |
| 20 | 0.4 |
| 25 | 0.5 |
| 30 | 0.6 |
| 35 | 0.8 |
| 40 (Standard) | 1.0 |
| 45 | 1.4 |
| 50 | 1.9 |
| 55 | 2.6 |
| 58 | 3.2 |

## A-III-5.6 Lubrication

A lithium soap based grease is sealed inside the cam follower which has seals. The range of temperature to use this grease is -10 to $110^{\circ} \mathrm{C}$. (Cam follower without seal uses oil lubrication, and does not have grease inside.)
Keep the lubricated track surface free of foreign mattersa.

## A-III-5.7 Permissible Rotational Speed

Cam followers with seal are suitable for high rotational operation. Table III $-5 \bullet 6$ shows their permissible rotational speed. Permissible rotational speed of full complement roller bearings are $1 / 3$ of those with retainer. For grease lubrication, permissible rotational speed is $60 \%$ of the values shown in the Table.
Table III-56 Permissible rotational speed of the bearing with retainer

| Reference No. | Permissible rotational <br> speed (rpm) |
| :---: | :---: |
| FCJ B-10 | 34000 |
| FCJ -12 | 26000 |
| FCJ -16 | 16000 |
| FCJ -19 | 12000 |
| FCJ -22 | 10000 |
| FCJ -26 | 10000 |
| FCJ -30 | 7500 |
| FCJ -32 | 7500 |
| FCJ -35 | 6000 |
| FCJ -40 | 5300 |
| FCJ -47 | 4800 |
| FCJ -52 | 4800 |
| FCJ -62 | 3800 |
| FCJ -72 | 3800 |
| FCJ -80 | 3000 |
| FCJ -85 | 3000 |
| FCJ -90 | 3000 |

## A-III-5.8 Precautions for Installation

## (1) Fits

The stud of cam follower is held on one side fixed. Fit between the stud and the bore where the stud enters must be in close tolerance.
Table III $-5 \cdot 7$ shows a recommended fit value.
The chamfer of the bore where the stud enters should be as small as possible, and the surface should be free of burrs.
When the fit is to be interference, press the stud into the hole, pushing the center of the end face.
To make the support face sufficiently large for the side plate, the surface diameter of the support end should be larger than $F$ shown in the dimension table.

## (2) Maximum tightening torque of the stud

Stud receives bending and tensile stress from the load to the bearing. Therefore, a screw tightening torque must not exceed values in the dimension table. (These values are when oil is applied to the screw section. Double the value when dry.)

Table III-5.7 Recommended fitt for stud installation

| Model code | Fit tolerance, class and <br> grade of installation hole |
| :---: | :---: |
| FCR, FCJ, FCRS, FCJ S | $\mathrm{J} 57(\mathrm{7})$ |

## Cam follower

FCR : Full complement of rollers
FCRS : Full complement of rollers, with seal and thrust washer

## FCJ : With retainer

FCJ S : With retainer, seal, and

## thrust washer



FCR


FCRS


FRE
FCRSP


| Model No. |  | Main dimension |  |  | Detail dimension |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { FCR } \\ & \text { FC } \end{aligned}$ | $\begin{aligned} & \text { FCRS } \\ & \text { FCJ S } \end{aligned}$ | D | C | d | $\begin{gathered} \text { Thread } \\ G \end{gathered}$ | $G_{1}$ | $B_{1}$ | $B_{2}$ | $B_{3}$ | M2 | M ${ }_{1}$ | $\begin{gathered} Y_{(2)} \\ (\mathrm{Min} .) \end{gathered}$ |
| FCJ B-10 | - | 10 | 7 | 3 | M $3 \times 0.5$ | 5 | 17 | 9 | - | - | - | 0.3 |
| $\begin{gathered} \text { FCJ -12 } \\ \text { FCJ B-12 } \end{gathered}$ | - | 12 | $8$ | $\begin{aligned} & 4 \\ & 4 \\ & 4 \end{aligned}$ | M4×0.7 <br> M4×0.7 | $\begin{aligned} & 6 \\ & 6 \\ & 6 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 11 \\ & 11 \end{aligned}$ | - |  | - | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ |
| $\begin{aligned} & \text { FCR-16 } \\ & \text { FCJ -16 } \end{aligned}$ | FCRS-16 <br> FCJ S-16 | 16 | $\begin{aligned} & \hline 11 \\ & 11 \end{aligned}$ | $\begin{aligned} & 1 \\ & \hline 6 \\ & 6 \end{aligned}$ | $\begin{aligned} & \hline \text { M } 6 \times 1.0 \\ & \text { M } 6 \times 1.0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 28 \\ & 28 \\ & 28 \end{aligned}$ | $\begin{aligned} & 16 \\ & 16 \\ & 16 \end{aligned}$ | - | - | $\begin{aligned} & \text { 4(1) } \\ & 4(1) \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FCR-19 } \\ & \text { FCJ -19 } \end{aligned}$ | $\begin{aligned} & \text { FCRS-19 } \\ & \text { FCJ S-19 } \end{aligned}$ | 19 | $\begin{aligned} & 11 \\ & 11 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & \text { M } 8 \times 1.25 \\ & \text { M } 8 \times 1.25 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | - | - | 4(1) 4(1) | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ |
| $\begin{aligned} & \text { FCR-22 } \\ & \text { FCJ }-22 \end{aligned}$ | FCRS-22 <br> FCJ S-22 | 22 | $\begin{aligned} & 12 \\ & 12 \\ & \hline \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { M10×1.25 } \\ & \text { M } 10 \times 1.25 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \\ & \hline \end{aligned}$ | $\begin{aligned} & 36 \\ & 36 \end{aligned}$ | $\begin{array}{r} 23 \\ 23 \\ \hline \end{array}$ | - | - | $\begin{aligned} & 4(1) \\ & 4(1) \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FCR-26 } \\ & \text { FCJ -26 } \end{aligned}$ | FCRS-26 <br> FCJ S-26 | 26 | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { M } 10 \times 1.25 \\ & \text { M } 10 \times 1.25 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & 36 \\ & 36 \\ & \hline \end{aligned}$ | $\begin{aligned} & 23 \\ & 23 \end{aligned}$ | - | - | $\begin{aligned} & 4(1) \\ & 4(1) \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ |
| $\begin{aligned} & \text { FCR-30 } \\ & \text { FCJ }-30 \end{aligned}$ | FCRS-30 FCJ S-30 | 30 | $\begin{aligned} & 14 \\ & 14 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & \text { M } 12 \times 1.5 \\ & \text { M } 12 \times 1.5 \end{aligned}$ | $\begin{aligned} & 13 \\ & 13 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | 6 | $\begin{aligned} & 3 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6 \\ & \hline 6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.6 \end{aligned}$ |
| $\begin{aligned} & \text { FCR-32 } \\ & \text { FCJ }-32 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { FCRS-32 } \\ & \text { FCJ S-32 } \\ & \hline \end{aligned}$ | 32 | $\begin{array}{r} 14 \\ 14 \\ \hline \end{array}$ | $\begin{aligned} & 12 \\ & 12 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{M} 12 \times 1.5 \\ & \mathrm{M} 12 \times 1.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 13 \\ & 13 \\ & \hline \end{aligned}$ | $\begin{array}{r} 40 \\ 40 \\ \hline \end{array}$ | $\begin{array}{r} 25 \\ 25 \\ \hline \end{array}$ | 6 | $\begin{aligned} & 3 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6 \\ & 6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.6 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FCR-35 } \\ & \text { FCJ }-35 \end{aligned}$ | FCRS-35 FCJ S-35 | 35 | $\begin{aligned} & 18 \\ & 18 \end{aligned}$ | $\begin{aligned} & 16 \\ & 16 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { M16×1.5 } \\ & \text { M } 16 \times 1.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 17 \\ & 17 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 52 \\ & 52 \\ & \hline \end{aligned}$ | $\begin{aligned} & 32.5 \\ & 32.5 \end{aligned}$ | $\begin{aligned} & \hline 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6 \\ & 6 \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.6 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FCR-40 } \\ & \text { FCJ }-40 \end{aligned}$ | $\begin{gathered} \hline \text { FCRS-40 } \\ \text { FCJ S-40 } \end{gathered}$ | 40 | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 18 \\ & 18 \end{aligned}$ | $\begin{aligned} & \text { M } 18 \times 1.5 \\ & \text { M } 18 \times 1.5 \end{aligned}$ | $\begin{aligned} & 19 \\ & 19 \\ & \hline \end{aligned}$ | $\begin{aligned} & 58 \\ & 58 \\ & \hline \end{aligned}$ | $\begin{aligned} & 36.5 \\ & 36.5 \end{aligned}$ | 8 | 3 3 | $\begin{aligned} & 6 \\ & 6 \end{aligned}$ | 1 |
| $\begin{aligned} & \text { FCR-47 } \\ & \text { FCJ }-47 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { FCRS-47 } \\ & \text { FCJ S-47 } \\ & \hline \end{aligned}$ | 47 | $\begin{array}{r} 24 \\ 24 \\ \hline \end{array}$ | $\begin{array}{r} 20 \\ 20 \\ \hline \end{array}$ | $\begin{aligned} & \text { M20 } 21.5 \\ & \text { M } 20 \times 1.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 21 \\ & 21 \\ & \hline \end{aligned}$ | $\begin{aligned} & 66 \\ & 66 \\ & \hline \end{aligned}$ | $\begin{array}{r} 40.5 \\ 40.5 \\ \hline \end{array}$ | 9 9 | $\begin{aligned} & 4 \\ & 4 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FCR-52 } \\ & \text { FCJ }-52 \end{aligned}$ | FCRS-52 <br> FCJ S-52 | 52 | $\begin{aligned} & 24 \\ & 24 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { M20×1.5 } \\ & \text { M } 20 \times 1.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 21 \\ & 21 \end{aligned}$ | $\begin{aligned} & \hline 66 \\ & 66 \end{aligned}$ | $\begin{aligned} & 40.5 \\ & 40.5 \end{aligned}$ | 9 9 | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \end{aligned}$ | 1 |
| $\begin{aligned} & \text { FCR-62 } \\ & \text { FCJ }-62 \end{aligned}$ | FCRS-62 FCJ S-62 | 62 | $\begin{aligned} & 29 \\ & 29 \end{aligned}$ | $\begin{aligned} & 24 \\ & 24 \end{aligned}$ | $\begin{aligned} & \text { M } 24 \times 1.5 \\ & \text { M } 24 \times 1.5 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \\ & \hline \end{aligned}$ | $\begin{aligned} & 80 \\ & 80 \end{aligned}$ | $\begin{aligned} & 49.5 \\ & 49.5 \end{aligned}$ | 11 | 4 | $\begin{aligned} & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |
| $\begin{aligned} & \text { FCR-72 } \\ & \text { FCJ }-72 \end{aligned}$ | FCRS-72 <br> FCJ S-72 | 72 | $\begin{aligned} & 29 \\ & 29 \end{aligned}$ | $\begin{aligned} & 24 \\ & 24 \end{aligned}$ | $\begin{aligned} & \text { M } 24 \times 1.5 \\ & \text { M } 24 \times 1.5 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 80 \\ & 80 \end{aligned}$ | $\begin{aligned} & 49.5 \\ & 49.5 \end{aligned}$ | 11 11 | 4 4 | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FCR-80 } \\ & \text { FCJ }-80 \\ & \hline \end{aligned}$ | FCRS-80 FCJ S-80 | 80 | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { M } 30 \times 1.5 \\ & \text { M } 30 \times 1.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 100 \\ & 100 \\ & \hline \end{aligned}$ | $\begin{aligned} & 63 \\ & 63 \end{aligned}$ | 15 15 | 4 4 | $\begin{aligned} & \hline 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |
| $\begin{aligned} & \text { FCR-85 } \\ & \text { FCJ }-85 \end{aligned}$ | FCRS-85 FCJ S-85 | 85 | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & \text { M } 30 \times 1.5 \\ & \text { M } 30 \times 1.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \end{aligned}$ | 100 100 | $\begin{aligned} & 63 \\ & 63 \end{aligned}$ | 15 15 | 4 4 | 8 | 1 |
| $\begin{aligned} & \text { FCR-90 } \\ & \text { FCJ -90 } \end{aligned}$ | FCRS-90 <br> FCJ S-90 | 90 | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & \text { M } 30 \times 1.5 \\ & \text { M } 30 \times 1.5 \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 63 \\ & 63 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & \hline 8 \\ & 8 \end{aligned}$ | 1 1 |


|  |  |  |  |  |  |  |  |  |  |  |  |  | Unit: mm |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Basic dynamic load ratiing $C_{r}$ |  | Permissible maximum load Pmax |  | Permissible track load |  | $\begin{array}{\|c\|} \begin{array}{c} \text { Weight } \\ \text { (kg) } \end{array} \\ \left\lvert\, \begin{array}{c} \text { (Reference } \\ \text { only) } \end{array}\right. \\ \hline \text { s. } \end{array}$ | Hexagon <br> sockethole <br> (wioth <br> accoss flat <br> x | Eccentric bush |  |  | $\begin{gathered} \begin{array}{c} \text { Tap hole for } \\ \text { lubrication pipe } \end{array} \\ P_{\mathrm{T}} \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { Diameter, } \\ \text { supportin } \\ \text { gusface } \end{array}\left\|\begin{array}{c} \text { g } \\ \hline \text { (M in.) } \end{array}\right\|$ | Thread tightening <br> torque(4) <br> $\mathbb{N} \cdot \mathrm{cm}\} \mathrm{kgf} \cdot \mathrm{cm}\}$ <br> (Max.) (Min.) |  |
| (N) | kgf\} |  | \{kgf\} | (N) | kgf\} |  |  | $B_{4}$ | $c_{1}$ | $E$ |  |  |  |  |
| 1390 | 142 | 590 | 60 | 1320 | 135 | 0.005 | 2.5 | - | - | - | - | 7.5 | 28 | 2.9 |
| 1970 | 201 | 1050 | 107 | 1860 | 190 | 0.008 |  | - | - | - |  | 9 | 64 | 6.5 |
| 1970 | 201 | 1050 | 107 | 1860 | 190 | 0.008 | 2.5 | - | - | - | - | 9 | 64 | 6.5 |
| 5800 | 590 | 2360 | 240 | 3350 | 340 | 0.020 | 4 | 8 | 9 | 0.5 | M6×0.75(3) | 11 | 226 | 23 |
| 2830 | 288 | 2360 | 240 | 3350 | 340 | 0.018 | 4 | 8 | 9 | 0.5 | M 6x0.75(3) | 11 | 226 | 23 |
| 6600 | 670 | 4200 | 425 | 4150 | 425 | 0.031 | 4 | 10 | 11 | 0.5 | M6x0.75(3) | 13 | 550 | 56 |
| 3450 | 355 | 4200 | 425 | 4150 | 425 | 0.030 | 4 | 10 | 11 | 0.5 | M 6x0.75(3) | 13 | 550 | 56 |
| 8550 | 875 | 6550 | 665 | 5300 | 540 | 0.047 | 5 | 11 | 13 | 0.5 | M6x0.75(3) | 15 | 1060 | 108 |
| 4350 | 445 | 6550 | 665 | 5300 | 540 | 0.045 | 5 | 11 | 13 | 0.5 | M $6 \times 0.75$ (3) | 15 | 1060 | 108 |
| 8550 | 875 | 6550 | 665 | 6000 | 610 | 0.060 | 5 | 11 | 13 | 0.5 | M6x0.75(3) | 15 | 1060 | 108 |
| 4350 | 445 | 6550 | 665 | 6000 | 610 | 0.058 | 5 | 11 | 13 | 0.5 | M $6 \times 0.75$ (3) | 15 | 1060 | 108 |
| 12500 | 1280 | 9250 | 945 | 7800 | 795 | 0.088 | 6 | 12 | 17 | 1 | M6x0.75(3) | 20 | 1450 | 148 |
| 7200 | 735 | 9250 | 945 | 7800 | 795 | 0.086 | 6 | 12 | 17 | 1 | M 6x0.75(3) | 20 | 1450 | 148 |
| 12500 | 1280 | 9250 | 945 | 8050 | 820 | 0.099 |  | 12 | 17 | 1 | M6x0.75(3) | 20 | 1450 | 148 |
| 7200 | 735 | 9250 | 945 | 8050 | 820 | 0.096 | 6 | 12 | 17 | 1 | M 6x0.75(3) | 20 | 1450 | 148 |
| 18600 | 1900 | 17000 | 1740 | 11800 | 1200 | 0.17 | 10 | 15.5 | 22 | 1 | RC 1/8 | 24 | 4000 | 410 |
| 9700 | 990 | 17000 | 1740 | 11800 | 1200 | 0.165 | 10 | 15.5 | 22 | 1 | RC 1/8 | 24 | 4000 | 410 |
| 20500 | 2090 | 21700 | 2220 | 14300 | 1460 | 0.25 | 10 | 17.5 | 24 | 1 | RC 1/8 | 26 | 5950 | 605 |
| 10300 | 1050 | 21700 | 2220 | 14300 | 1460 | 0.24 | 10 | 17.5 | 24 | 1 | RC 1/8 | 26 | 5950 | 605 |
| 28200 | 2880 | 26400 | 2690 | 20800 | 2120 | 0.39 | 12 | 19.5 | 27 | 1 | RC 1/8 | 31 | 8450 | 860 |
| 19200 | 1950 | 26400 | 2690 | 20800 | 2120 | 0.38 | 12 | 19.5 | 27 | 1 | RC 1/8 | 31 | 8450 | 860 |
| 28200 | 2880 | 26400 | 2690 | 22900 | 2340 | 0.47 | 12 | 19.5 | 27 | 1 | RC 1/8 | 31 | 8450 | 860 |
| 19200 | 1950 | 26400 | 2690 | 22900 | 2340 | 0.455 | 12 | 19.5 | 27 | 1 | RC 1/8 | 31 | 8450 | 860 |
| 40000 | 4100 | 38500 | 3950 | 34000 | 3450 | 0.80 | 14 | 24.5 | 34 | 1 | RC 1/8 | 45 | 15200 | 1550 |
| 24900 | 2540 | 38500 | 3950 | 34000 | 3450 | 0.79 | 14 | 24.5 | 34 | 1 | RC 1/8 | 45 | 15200 | 1550 |
| 40000 | 4100 | 38500 | 3950 | 38000 | 3860 | 1.05 | 14 | 24.5 | 34 | 1 | RC 1/8 | 45 | 15200 | 1550 |
| 24900 | 2540 | 38500 | 3950 | 38000 | 3860 | 1.05 | 14 | 24.5 | 34 | 1 | RC 1/8 | 45 | 15200 | 1550 |
| 60500 | 6200 | 61000 | 6200 | 52000 | 5300 | 1.55 | 17 | 31 | 40 | 1.5 | RC 1/8 | 52 | 30500 | 3120 |
| 39000 | 4000 | 61000 | 6200 | 52000 | 5300 | 1.55 | 17 | 31 | 40 | 1.5 | RC 1/8 | 52 | 30500 | 3120 |
| 60500 | 6200 | 61000 | 6200 | 55500 | 5650 | 1.75 | 17 | 31 | 40 | 1.5 | RC 1/8 | 52 | 30500 | 3120 |
| 39000 | 4000 | 61000 | 6200 | 55500 | 5650 | 1.75 | 17 | 31 | 40 | 1.5 | RC 1/8 | 52 | 30500 | 3120 |
| 60500 | 6200 | 61000 | 6200 | 59000 | 6000 | 1.95 | 17 | 31 | 40 | 1.5 | RC 1/8 | 52 | 30500 | 3120 |
| 39000 | 4000 | 61000 | 6200 | 59000 | 6000 | 1.95 | 17 | 31 | 40 | 1.5 | RC 1/8 | 52 | 30500 | 3120 |

(2) Use a value larger than $\gamma$ (minimum)
(3) Pipe tap screw for oil supply is only on the front face of the head.
(4) Values are when oil is applied to the screw section. Double (approx.) the value when dry.

Remarks : Grease is sealed in for the cam follower with seals. Cam follower without seal does not have grease

## A-III-6 Roller Follower

## A-II-6.1 Structure and Characteristics

The outer ring of the bearing functions as a rolling ring (Fig. III- $-\cdot 1$ ). This rolling ring is thick and tough. The rollers are crowned needle rollers, and have a large load carrying capacity. This provides high impact resistance.


Needle roller bearing
Fig. III-6•1 Structure of Roller Follower
A-III-6.2 Types

## (1) Bearing models

There are four models: With/ without a retainer and oil/grease lubricant (Table III-6•1).

Table III-6•1 Bearing models

| Bearing model | Description |
| :---: | :--- |
| FYCR | Full complement of rollers, no seal <br> (oil is supplied later) |
| FYCRS | Full complement of rollers, with seal <br> (grease is sealed in) |
| FYCJ | With retainer, no seal (oil is supplied later) |
| FYCJ S | With retainer, with seal (grease is sealed in) |



Fig. III-6॰2 Sphere shaped rolling ring

## (2) Exterior appearances

There are two types as shown in Table III-6•2.

Table III-6•2 Types of exterior appearance

| Code for <br> appearance | Description |
| :---: | :--- |
| (no code) | Cylindrical shaped outer surface <br> RSphere shaped: Outer surface forms a <br> part of sphere with arc of radius 500 mm. <br> (Fig. III-6.2) |

## (3) Special products

NSK manufactures the following items. Please consult NSK.

- Items in inch sizes
- Black film coating on exposed surface
- Special-shaped items.


## A-III-6.3 Reference Number for Ordering

Codes shown in (1) Bearing models, (2) Exterior Appearances constitute a reference number for ordering.

## Reference number composition



FYCR : Full complement of rollers, no seal (oil is supplied later)
FYCRS : Full complement of rollers, with seal (grease is sealed in)
FYCJ : With retainer, no seal (oil is supplied later)
FYCJ S : With retainer, with seal (grease is sealed in)

- G : Spherical outer surface, radius of 500 mm (R) Internal diameter (unit: mm)

Note: Different from cam follower which uses outer diameter .
(Example) FYCR-5 : Full complement of rollers; with seal (grease is sealed in); internal diameter 5 mm FYCJ -5R : With retainer, no seal (oil is supplied later), internal diameter 5 mm ; Spherical outer surface rolling ring

## A-III-6.4 Accuracy

Dimension tolerance and running accuracy are the same as JIS 0 grade. However, the admissible difference in single plane mean outside diameter of spherical outer surface is 0.0 to -(minus) 0.05 mm .

## A-III-6.5 Permissible Load

## (1) Permissible load of roller follower

As a bearing, allowable load is determined by basic load rating. Refer to load rating values in the dimension table.

## (2) Permissible load of rail track

The concept is the same as for cam follower. Refer to Page A217 for permissible load values.

## A-III-6.6 Lubrication

A lithium soap based grease is sealed inside the Roller Follower which has seals. The range of temperature to use this grease is -10 to $110{ }^{\circ} \mathrm{C}$. Supply oil to the Roller Follower which does not have a seal.
The track surface for lubrication should be nearly free of foreign matters.

## A-III-6.7 Permissible Rotational Speed

Roller Follower models with retainer are suitable for high rotational operations. Table III- $6 \cdot 3$ shows their permissible rotational speed. Permissible rotational speed of a roller follower with full complement of roller is $1 / 3$ of those with retainer. In case of grease lubrication, permissible speed is $60 \%$ of the values shown in the Table.

Table III-6.3 Permissible rotational speed of the bearing with retainer

| Reference No. | Permissible rotational <br> speed (rpm) |
| :---: | :---: |
| FYCJ -5 | 16000 |
| FYCJ -6 | 12000 |
| FYCJ -8 | 10000 |
| FYCJ -10 | 8000 |
| FYCJ -12 | 7100 |
| FYCJ -15 | 6300 |
| FYCJ -17 | 5600 |
| FYCJ -20 | 5000 |
| FYCJ -25 | 4000 |
| FYCJ -30 | 3200 |
| FYCJ -35 | 2800 |
| FYCJ -40 | 2400 |
| FYCJ -45 | 2000 |
| FYCJ -50 | 1900 |

## A-III-6.8 Precautions for Installation

Roller Follower is generally operated by outer ring rotation. The shaft is used by "medium fit" or "clearance fit." For heavy load, the shaft is hardened by heat-treatment, and is used by "interference fit." Table III-6•4 shows recommended fit values.
Secure both sides of the inner ring to a flat surface which is at right angle to the center axis.
To make the support face sufficiently large for the side plate, the end face of the support should be larger than F shown in the dimension table. (anion

Table III-64 Recommended fit for shaft

| Load | Tolerance grade of shaft (class) |
| :---: | :---: |
| Light load, medium load | g6 or h6 |
| Heavy load | k6 |

## Roller Follower

FYCR : Full complement of rollers

## FYCRS : Full complement of rollers, with

 seal, thrust washer FYCJ : With retainerFYCJ S : With retainer, seal, thrust washer

FYCR
FYCRS

| Model No. |  | Main dimension |  |  |  |  | Basic load <br> (N) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { FYCR } \\ & \text { FYCJ } \end{aligned}$ | $\begin{aligned} & \hline \text { FYCRS } \\ & \text { FYCJ S } \end{aligned}$ | d | D | C | $\begin{gathered} B \\ -0.38 \\ -0.38 \end{gathered}$ | $\begin{gathered} r \\ \text { (Min.) } \end{gathered}$ | $\underset{C_{r}}{\substack{\text { Dynamic }}}$ | Static Cor |
| FYCR-5 <br> FYCJ -5 | FYCRS-5 <br> FYCJ S-5 | 5 | $\begin{aligned} & 16 \\ & 16 \end{aligned}$ | $\begin{aligned} & 11 \\ & 11 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 5800 \\ & 2830 \end{aligned}$ | $\begin{aligned} & 8000 \\ & 2620 \end{aligned}$ |
| FYCR-6 FYCJ -6 | $\begin{aligned} & \text { FYCRS-6 } \\ & \text { FYCJ S-6 } \end{aligned}$ | 6 | $\begin{aligned} & 19 \\ & 19 \end{aligned}$ | $\begin{aligned} & 11 \\ & 11 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 6550 \\ & 3450 \end{aligned}$ | $\begin{aligned} & 9900 \\ & 3600 \end{aligned}$ |
| FYCR-8 FYCJ -8 | FYCRS-8 FYCJ S-8 | 8 | $\begin{aligned} & 24 \\ & 24 \end{aligned}$ | $\begin{aligned} & 14 \\ & 14 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{gathered} 10100 \\ 5700 \\ \hline \end{gathered}$ | $\begin{aligned} & 15000 \\ & 6000 \end{aligned}$ |
| $\begin{aligned} & \text { FYCR-10 } \\ & \text { FYCJ -10 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-10 } \\ & \text { FYCJ S-10 } \end{aligned}$ | 10 | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 14 \\ & 14 \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.6 \\ & \hline \end{aligned}$ | $\begin{gathered} 11700 \\ 6950 \\ \hline \end{gathered}$ | $\begin{gathered} 18500 \\ 8200 \\ \hline \end{gathered}$ |
| $\begin{aligned} & \text { FYCR-12 } \\ & \text { FYCJ -12 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { FYCRS-12 } \\ & \text { FYCJ S-12 } \\ & \hline \end{aligned}$ | 12 | $\begin{aligned} & 32 \\ & 32 \\ & \hline \end{aligned}$ | $\begin{aligned} & 14 \\ & 14 \\ & \hline \end{aligned}$ | $\begin{aligned} & 15 \\ & 15 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.6 \\ & \hline \end{aligned}$ | $\begin{gathered} 12600 \\ 7650 \\ \hline \end{gathered}$ | $\begin{gathered} 21000 \\ 9650 \\ \hline \end{gathered}$ |
| $\begin{aligned} & \text { FYCR-15 } \\ & \text { FYCJ-15 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-15 } \\ & \text { FYCJ S-15 } \end{aligned}$ | 15 | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & 18 \\ & 18 \\ & \hline \end{aligned}$ | $\begin{aligned} & 19 \\ & 19 \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 18700 \\ & 12200 \end{aligned}$ | $\begin{aligned} & 29300 \\ & 14100 \end{aligned}$ |
| FYCR-17 FYCJ - 17 | $\begin{aligned} & \text { FYCRS-17 } \\ & \text { FYCJ S-17 } \end{aligned}$ | 17 | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & 21 \\ & 21 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 21100 \\ & 13700 \\ & \hline \end{aligned}$ | $\begin{aligned} & 35000 \\ & 16700 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \hline \text { FYCR-20 } \\ & \text { FYCJ-20 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-20 } \\ & \text { FYCJ S-20 } \end{aligned}$ | 20 | $\begin{array}{r} 47 \\ 47 \\ \hline \end{array}$ | $\begin{array}{r} 24 \\ 24 \\ \hline \end{array}$ | 25 25 | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 28900 \\ & 18200 \\ & \hline \end{aligned}$ | $\begin{aligned} & 50000 \\ & 22600 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { FYCR-25 } \\ & \text { FYCJ }-25 \\ & \hline \end{aligned}$ | FYCRS-25 FYCJ S-25 | 25 | $\begin{aligned} & 52 \\ & 52 \end{aligned}$ | $\begin{aligned} & 24 \\ & 24 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 32500 \\ & 22200 \\ & \hline \end{aligned}$ | $\begin{aligned} & 60000 \\ & 31000 \end{aligned}$ |
| $\begin{aligned} & \text { FYCR-30 } \\ & \text { FYCJ }-30 \end{aligned}$ | $\begin{aligned} & \text { FYCRS-30 } \\ & \text { FYCJ S-30 } \end{aligned}$ | 30 | $\begin{aligned} & 62 \\ & 62 \end{aligned}$ | $\begin{aligned} & 28 \\ & 28 \end{aligned}$ | $\begin{aligned} & 29 \\ & 29 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 47500 \\ & 31500 \end{aligned}$ | $\begin{aligned} & 96000 \\ & 47000 \end{aligned}$ |
| $\begin{aligned} & \hline \text { FYCR-35 } \\ & \text { FYCJ }-35 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { FYCRS-35 } \\ & \text { FYCJ S-35 } \\ & \hline \end{aligned}$ | 35 | $\begin{aligned} & \hline 72 \\ & 72 \\ & \hline \end{aligned}$ | $\begin{aligned} & 28 \\ & 28 \\ & \hline \end{aligned}$ | $\begin{array}{r} 29 \\ 29 \\ \hline \end{array}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 49000 \\ & 33000 \\ & \hline \end{aligned}$ | $\begin{gathered} 106500 \\ 52500 \\ \hline \end{gathered}$ |
| $\begin{aligned} & \text { FYCR-40 } \\ & \text { FYCJ }-40 \end{aligned}$ | $\begin{aligned} & \text { FYCRS-40 } \\ & \text { FYCJ S-40 } \end{aligned}$ | 40 | $\begin{aligned} & 80 \\ & 80 \\ & 80 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 54500 \\ & 38500 \end{aligned}$ | $\begin{gathered} 126000 \\ 67500 \end{gathered}$ |
| $\begin{aligned} & \text { FYCR-45 } \\ & \text { FYCJ -45 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-45 } \\ & \text { FYCJ S-45 } \end{aligned}$ | 45 | $\begin{aligned} & 85 \\ & 85 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 57500 \\ & 40000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 139000 \\ & 73000 \end{aligned}$ |
| $\begin{aligned} & \text { FYCR-50 } \\ & \text { FYCJ -50 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-50 } \\ & \text { FYCJ S-50 } \end{aligned}$ | 50 | $\begin{aligned} & 90 \\ & 90 \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 60500 \\ & 41500 \end{aligned}$ | $\begin{gathered} 152000 \\ 78000 \end{gathered}$ |

Remarks: Grease is sealed in for the Roller follower with seals. Roller follower without seal does not have grease.


| rating kgf\} |  | Track permissible load |  | Weight <br> (kg) <br> (Reference only) | Diameter, <br> supporting surface <br> $F$ <br> (Min.) | Model No. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Dynamic } \\ C_{T} \end{gathered}$ | $\begin{gathered} \text { Static } \\ \text { Cor } \end{gathered}$ | (N) | kgf $\}$ |  |  | $\begin{aligned} & \hline \text { FYCR } \\ & \text { FYCJ } \end{aligned}$ | $\begin{aligned} & \hline \text { FYCRS } \\ & \text { FYCJ S } \end{aligned}$ |
| $\begin{aligned} & 590 \\ & 288 \end{aligned}$ | $\begin{aligned} & 815 \\ & 267 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3350 \\ & 3350 \end{aligned}$ | $\begin{aligned} & 340 \\ & 340 \end{aligned}$ | $\begin{aligned} & 0.016 \\ & 0.014 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | FYCR-5 FYCJ -5 | FYCRS-5 FYCJ S-5 |
| $\begin{aligned} & 665 \\ & 355 \end{aligned}$ | $\begin{gathered} 1010 \\ 365 \end{gathered}$ | $\begin{aligned} & 4150 \\ & 4150 \end{aligned}$ | $\begin{aligned} & 425 \\ & 425 \end{aligned}$ | $\begin{aligned} & 0.022 \\ & 0.020 \\ & \hline \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ | FYCR-6 FYCJ -6 | $\begin{aligned} & \text { FYCRS-6 } \\ & \text { FYCJ S-6 } \end{aligned}$ |
| $\begin{gathered} 1030 \\ 580 \\ \hline \end{gathered}$ | $\begin{gathered} 1530 \\ 610 \end{gathered}$ | $\begin{aligned} & 6500 \\ & 6500 \end{aligned}$ | $\begin{aligned} & 665 \\ & 665 \end{aligned}$ | $\begin{aligned} & \hline 0.044 \\ & 0.042 \\ & \hline \end{aligned}$ | $\begin{aligned} & 14 \\ & 14 \end{aligned}$ | $\begin{aligned} & \text { FYCR-8 } \\ & \text { FYCJ }-8 \end{aligned}$ | $\begin{aligned} & \hline \text { FYCRS-8 } \\ & \text { FYCJ S-8 } \end{aligned}$ |
| $\begin{gathered} 1190 \\ 705 \end{gathered}$ | 1890 835 | 7800 7800 | $\begin{aligned} & \hline 795 \\ & 795 \end{aligned}$ | $\begin{aligned} & 0.069 \\ & 0.067 \end{aligned}$ | $\begin{aligned} & 17 \\ & 17 \\ & \hline \end{aligned}$ | FYCR-10 <br> FYCJ - 10 | $\begin{aligned} & \hline \text { FYCRS-10 } \\ & \text { FYCJ S-10 } \end{aligned}$ |
| $\begin{aligned} & 1280 \\ & 780 \\ & \hline \end{aligned}$ | $\begin{gathered} 2140 \\ 985 \\ \hline \end{gathered}$ | $\begin{aligned} & 8050 \\ & 8050 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 820 \\ & 820 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.076 \\ & 0.074 \\ & \hline \end{aligned}$ | $\begin{array}{r} 19 \\ 19 \\ \hline \end{array}$ | $\begin{aligned} & \hline \text { FYCR-12 } \\ & \text { FYCJ-12 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-12 } \\ & \text { FYCJ S-12 } \\ & \hline \end{aligned}$ |
| 1910 | 2990 | 11800 | 1200 | 0.105 | 23 | FYCR-15 | FYCRS-15 |
| 1250 | 1440 | 11800 | 1200 | 0.097 | 23 | FYCJ -15 | FYCJ S-15 |
| 2160 1390 | 3600 1700 | 14300 | $\begin{aligned} & \hline 1460 \\ & 1460 \\ & \hline \end{aligned}$ | $\begin{gathered} 0.145 \\ 0.14 \\ \hline \end{gathered}$ | $\begin{aligned} & 25 \\ & 25 \\ & \hline \end{aligned}$ | FYCR-17 <br> FYCJ - 17 | $\begin{aligned} & \hline \text { FYCRS-17 } \\ & \text { FYCJ S-17 } \end{aligned}$ |
| $\begin{array}{r} 2940 \\ 1850 \\ \hline \end{array}$ | $\begin{aligned} & 5100 \\ & 2310 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20800 \\ & 20800 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2120 \\ & 2120 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.255 \\ & 0.245 \\ & \hline \end{aligned}$ | $\begin{array}{r} 29 \\ 29 \\ \hline \end{array}$ | $\begin{aligned} & \text { FYCR-20 } \\ & \text { FYCJ -20 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { FYCRS-20 } \\ & \text { FYCJ S-20 } \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 3300 \\ & 2270 \end{aligned}$ | $\begin{aligned} & 6100 \\ & 3150 \end{aligned}$ | $\begin{aligned} & 22900 \\ & 22900 \end{aligned}$ | $\begin{aligned} & 2340 \\ & 2340 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.285 \\ & 0.275 \end{aligned}$ | $\begin{aligned} & 34 \\ & 34 \end{aligned}$ | $\begin{aligned} & \text { FYCR-25 } \\ & \text { FYCJ }-25 \end{aligned}$ | FYCRS-25 FYCJ S-25 |
| $\begin{aligned} & 4800 \\ & 3200 \end{aligned}$ | $\begin{aligned} & 9800 \\ & 4800 \end{aligned}$ | $\begin{aligned} & 33000 \\ & 33000 \end{aligned}$ | $\begin{aligned} & 3350 \\ & 3350 \end{aligned}$ | $\begin{aligned} & 0.48 \\ & 0.47 \end{aligned}$ | $\begin{aligned} & 51 \\ & 51 \end{aligned}$ | $\begin{aligned} & \text { FYCR-30 } \\ & \text { FYCJ }-30 \end{aligned}$ | $\begin{aligned} & \text { FYCRS-30 } \\ & \text { FYCJ S-30 } \end{aligned}$ |
| $\begin{array}{r} 5050 \\ 3400 \\ \hline \end{array}$ | $\begin{gathered} 10800 \\ 5350 \\ \hline \end{gathered}$ | $\begin{aligned} & 36500 \\ & 36500 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3700 \\ & 3700 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.64 \\ 0.635 \\ \hline \end{array}$ | $\begin{aligned} & 58 \\ & 58 \end{aligned}$ | $\begin{aligned} & \text { FYCR-35 } \\ & \text { FYCJ -35 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-35 } \\ & \text { FYCJ S-35 } \end{aligned}$ |
| $\begin{aligned} & 5600 \\ & 3950 \end{aligned}$ | $\begin{gathered} 12800 \\ 6900 \end{gathered}$ | $\begin{aligned} & 43500 \\ & 43500 \end{aligned}$ | $\begin{aligned} & 4450 \\ & 4450 \end{aligned}$ | $\begin{aligned} & 0.88 \\ & 0.865 \end{aligned}$ | $\begin{aligned} & 66 \\ & 66 \end{aligned}$ | $\begin{aligned} & \text { FYCR-40 } \\ & \text { FYCJ -40 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-40 } \\ & \text { FYCJ S-40 } \end{aligned}$ |
| $\begin{aligned} & 5850 \\ & 4100 \end{aligned}$ | $\begin{aligned} & 14100 \\ & 7450 \end{aligned}$ | $\begin{aligned} & 46500 \\ & 46500 \end{aligned}$ | $\begin{aligned} & 4750 \\ & 4750 \end{aligned}$ | $\begin{aligned} & 0.93 \\ & 0.91 \end{aligned}$ | $\begin{aligned} & 72 \\ & 72 \\ & \hline \end{aligned}$ | FYCR-45 <br> FYCJ - 45 | FYCRS-45 FYCJ S-45 |
| $\begin{aligned} & 6150 \\ & 4200 \end{aligned}$ | $\begin{gathered} 15500 \\ 7950 \end{gathered}$ | $\begin{aligned} & 49500 \\ & 49500 \end{aligned}$ | $\begin{aligned} & 5050 \\ & 5050 \end{aligned}$ | $\begin{aligned} & 0.995 \\ & 0.965 \end{aligned}$ | $\begin{aligned} & 76 \\ & 76 \end{aligned}$ | $\begin{aligned} & \text { FYCR-50 } \\ & \text { FYCJ -50 } \end{aligned}$ | $\begin{aligned} & \text { FYCRS-50 } \\ & \text { FYCJ S-50 } \end{aligned}$ | . . 


[^0]:    * Refer to the dimension tables for the rail dimension G.

[^1]:    * Refer to the dimension tables for the rail dimension $\mathbf{G}$.
    **A rail, of which reference number has a letter T, is a standard rail with bolt holes for M4. Reference number without letter T indicates that a rail is a standard with bolt holes for M3. Both items are stocked as the standard rail.

[^2]:    * Refer to the dimension tables for the rail dimension G.

[^3]:    * Refer to the dimension tables for the rail dimension $\mathbf{G}$.

[^4]:    * Refer to the dimension tables for the rail dimension $\mathbf{G}$.

[^5]:    * Refer to the dimension tables for the rail dimension $\mathbf{G}$.

[^6]:    * Refer to the dimension tables for the rail dimension $\mathbf{G}$.

[^7]:    * Refer to the dimension tables for the rail dimension G.

[^8]:    LA Series does not have a ball retainer. Be aware that balls fall out when the ball slider is withdrawn from the rail.

[^9]:    LA Series does not have a ball retainer. Be aware that balls fall out when the ball slider is withdrawn from the rail.

[^10]:    LY15 has a single row of balls on each right and left side.

[^11]:    AU09 and 12 are available only in stainless stee.

